



forestry, fisheries & the environment

Department:
Forestry, Fisheries and the Environment
REPUBLIC OF SOUTH AFRICA

Private Bag X447, Pretoria, 0001, Environment House, 473 Steve Biko Road, Pretoria, 0002 Tel: +27 12 399 9000, Fax: +27 86 625 1042

SPECIALIST DECLARATION FORM – AUGUST 2023

Specialist Declaration form for assessments undertaken for application for authorisation in terms of the National Environmental Management Act, Act No. 107 of 1998, as amended and the Environmental Impact Assessment (EIA) Regulations, 2014, as amended (the Regulations)

REPORT TITLE

Geotechnical Assessment Study for the proposed construction and maintenance of New System 1 and associated infrastructure at Rand Water Vereeniging Treatment Works. *Note the report was compiled in 2019 but is still applicable for this project.*

Kindly note the following:

1. This form must always be used for assessment that are in support of applications that must be subjected to Basic Assessment or Scoping & Environmental Impact Reporting, where this Department is the Competent Authority.
2. This form is current as of August 2023. It is the responsibility of the Applicant / Environmental Assessment Practitioner (EAP) to ascertain whether subsequent versions of the form have been published or produced by the Competent Authority. The latest available Departmental templates are available at <https://www.dffe.gov.za/documents/forms>.
3. An electronic copy of the signed declaration form must be appended to all Draft and Final Reports submitted to the department for consideration.
4. The specialist must be aware of and comply with 'the Procedures for the assessment and minimum criteria for reporting on identified environmental themes in terms of sections 24(5)(a) and (h) and 44 of the act, when applying for environmental authorisation - GN 320/2020', where applicable.

1. SPECIALIST INFORMATION

Title of Specialist Assessment	Geotechnical Assessment Study for the proposed construction and maintenance of New System 1 and associated infrastructure at Rand Water Vereeniging Treatment Works
Specialist Company Name	Knight Piesold
Specialist Name	Michael Plichta
Specialist Identity Number	7508075219084
Specialist Qualifications:	BSc (Eng) Civil, GDE (Civil)
Professional affiliation/registration:	ECSA 20060014
Physical address:	Boardwalk Office Park, Eros Street, Faerie Glen
Postal address:	Atterbury PostNet Suite #057, Private Bag X20009
Postal address	Garsfontein 0042
Telephone	012 991 0557
Cell phone	083 609 9919
E-mail	mplichta@knightpiesold.com

SPECIALIST DECLARATION FORM – AUGUST 2023

2. DECLARATION BY THE SPECIALIST

I, Michael Plichta declare that –

- I act as the independent specialist in this application;
- I am aware of the procedures and requirements for the assessment and minimum criteria for reporting on identified environmental themes in terms of sections 24(5)(a) and (h) and 44 of the National Environmental Management Act (NEMA), 1998, as amended, when applying for environmental authorisation which were promulgated in Government Notice No. 320 of 20 March 2020 (i.e. “the Protocols”) and in Government Notice No. 1150 of 30 October 2020.
- I will perform the work relating to the application in an objective manner, even if this results in views and findings that are not favourable to the applicant;
- I declare that there are no circumstances that may compromise my objectivity in performing such work;
- I have expertise in conducting the specialist report relevant to this application, including knowledge of the Act, Regulations and any guidelines that have relevance to the proposed activity;
- I will comply with the Act, Regulations and all other applicable legislation;
- I have no, and will not engage in, conflicting interests in the undertaking of the activity;
- I undertake to disclose to the applicant and the competent authority all material information in my possession that reasonably has or may have the potential of influencing –
 - any decision to be taken with respect to the application by the competent authority; and;
 - the objectivity of any report, plan or document to be prepared by myself for submission to the competent authority;
- All the particulars furnished by me in this form are true and correct; and
- I realise that a false declaration is an offence in terms of Regulation 48 and is punishable in terms of section 24F of the NEMA Act.

M Plichta

Signature of the Specialist

Knights Piesold

Name of Company:

16 Sept 2025

Date

SPECIALIST DECLARATION FORM – AUGUST 2023

3. UNDERTAKING UNDER OATH/ AFFIRMATION

I, Michael Plichta, swear under oath / affirm that all the information submitted or to be submitted for the purposes of this application is true and correct.

M. Plichta
Signature of the Specialist

Knight Piesold
Name of Company

16 September 2025
Date

[Signature]
Signature of the Commissioner of Oaths

16 September 2025
Date

CERTIFIED TRUE COPY OF THE ORIGINAL DOCUMENT
THERE ARE NO INDICATION THAT THE ORIGINAL
DOCUMENT HAS BEEN ALTERED BY UNAUTHORISED
PERSONS.

Neeva Anne Matthyssen: Tender Lead
Reference Number: 31/04/2016
Commissioner of Oaths (RSA)
Signature: [Signature]
Date: 16/09/2025
Business Address: 1 Discovery Place, The Ridge, Sandton
Tel: +27 11 8067111 email: tenders@knightpiesold.com
Place: Sandton

VEREENIGING PUMPING STATION 225ML SEDIMENTATION TANK, FLOCCULATOR AND ASSOCIATED SYSTEM 1 PIPELINES

GEOTECHNICAL INVESTIGATION



PREPARED FOR:



RAND WATER

PO Box 1127
Johannesburg
2000
Tel: Tel: +27 11 682 0089

PREPARED BY



PO Box 72292
Lynnwood Ridge
0040

Tel: +27 12 991 0557

MAY 2019

Project No: 30300496/03

Report No: KHH2488

Rev: 2

Reference Code: OGP-DB/KHH2488/Rev.2

FINAL REPORT



Prepared for
RAND WATER
PO Box 1127
JOHANNESBURG
2000

Prepared by
Knight Piésold Ltd.
The Boardwalk Office Park
Block 5
Eros Road
Faerie Glen, Pretoria
South Africa

Project Number
30300496/03

VEREENIGING PUMPING STATION: GEOTECHNICAL INVESTIGATION 225ML SEDIMENTATION TANK, FLOCCULATOR AND ASSOCIATED SYSTEM 1 PIPELINES

Rev	Description	Date
2	Issued as Final	10 May 2019

TABLE OF CONTENTS

	PAGE
Table of Contents	i
1. INTRODUCTION	1
2. SITE DESCRIPTION	1
3. AVAILABLE INFORMATION	2
4. REGIONAL GEOLOGY	2
5. GEOHYDROLOGY	3
6. CLIMATE	3
7. SEISMICITY	3
8. METHOD OF INVESTIGATION	4
8.1 Fieldwork.....	4
8.2 Pipeline General Soil Profile	4
8.3 Old System 1A Soil Profile (TP12 to TP16 and TP16A)	6
9. LABORATORY TESTING	7
9.1 Pipeline Results	7
9.2 Old System 1A Excavation Results	8
10. GEOTECHNICAL EVALUATION	9
10.1 General.....	9
10.2 Earthworks Recommendations	10
10.3 Excavation Dewatering	11
10.4 Construction Recommendations.....	12
10.5 Pipeline Recommendations	12
11. CONCLUSION	13
12. REFERENCES	14
13. CERTIFICATION	15

TABLE OF CONTENTS (continued)

TABLES

TABLE 1	: SUMMARY OF TEST PIT PROFILES
TABLE 2	: SUMMARY OF LABORATORY TEST RESULTS
TABLE 3	: MINIMUM FLOCCULATOR AND SEDIMENTATION TANK EXCAVATION LEVELS
TABLE 4	: RECOMMENDED FLOCCULATOR AND SEDIMENTATION TANK EXCAVATION LEVELS

FIGURES

FIGURE 1	: LOCALITY PLAN
FIGURE 2	: GEOLOGY
FIGURE 3	: GEOTECHNICAL PLAN
FIGURE 4	: PROPOSED EXCAVATION PLAN (SCHEMATIC)
FIGURE 5	: SIMPLIFIED SECTION AND PLAN OF SLUDGE PIPELINE

APPENDICES

APPENDIX A	: TEST PIT PROFILES
APPENDIX B	: SITE PHOTOGRAPHS
APPENDIX C	: LABORATORY TEST RESULTS
APPENDIX D	: JG AFRIKA TEST PIT AND BOREHOLE LOGS

1. INTRODUCTION

Rand Water (RW) appointed Knight Piésold (KP) to conduct a geotechnical investigation for a 225 ML sedimentation tank and flocculator referred to as System 1 at Vereeniging Pumping Station. The appointment also included the geotechnical investigation for the associated raw water, wash water, recovered water and sludge pipelines.

The old System 1A structures should have been demolished to allow construction of the new sedimentation tank and flocculator. A contractor was appointed for the demolition works but the work was not completed as the contractor was removed from site.

The objectives of the geotechnical investigation were to:

- Confirm the site stratigraphy and the geotechnical properties thereof,
- Determine the nature of the shallow soils,
- Establish the potential for in situ materials to be used in pavement layers, and
- Provide foundation recommendations.

This report presents the findings from the recent fieldwork that supplements the previous geotechnical investigation information from other consultants. This report details the KP findings and provides recommendations for the proposed System 1 development.

2. SITE DESCRIPTION

The Vereeniging Pump Station is located approximately 2km south-west of the Vereeniging Central Business District (CBD), and 1,5km north-west of the Vaal River. The pump station is bounded by the R42 road to the south, a railway line to the east, and by Colenso and Taaibos Streets to the west and north respectively. The location of the site is shown in Figure 1, included at the end of this report.

The site topography is generally flat but the natural ground has been significantly disturbed when the large tank and water treatment structures were constructed. The elevations across the pump station vary between 1446 masl and 1441 masl according to Google Earth imagery. Access is generally from Taaibos street to the north, or from the main gate off the R42 Barrage road to the south.

Surface vegetation typically comprises veld grasses for most of the site. Scattered pine trees occur at the south-western portion of the site together with other indigenous trees.

The Vaal river lies approximately 1,8 km south of the site and a concrete lined tributary canal lies approximately 200 m to the west. Apart from these water courses, no other regional surface drainage features of significance are close to the site.

Reinforced concrete rubble from the old System 1A demolition is stockpiled north of the System 4 sedimentation tanks.

3. AVAILABLE INFORMATION

RW previously provided KP with the following information:

- System 1 geotechnical report dated November 2016, prepared by JG Afrika.
- System 5 geotechnical report dated February 1984, prepared by SRK, Report No. PT3583.
- Pre-wetting of sedimentation tanks at Vereeniging Pump Station, dated February 1986, Report No. PT3583/2.
- Proposed System 1 Drawings, prepared by Bosch Projects.
- Old System 1A drawings.
- System 5 tank drawings.

A geotechnical investigation was conducted at the proposed System 1 sedimentation tank and flocculator by JG Africa in 2016. The investigation comprised the following:

- Six electrical resistivity traverses
- Drilling of 8 rotary core boreholes to depths from 12,5m to 20,4m.
- The excavation of 3 test pits using a TLB.
- The driving of 3 Dynamic Cone Penetrometer (DCP) tests, one at each test pit position.

The borehole information is quite comprehensive although no boreholes were drilled at the north-western portion of the investigation footprint. This is probably due to the presence of ponding water that made this area inaccessible.

4. REGIONAL GEOLOGY

According to the published 1:250 000 scale regional geological map of the West Rand 2626 [1], the site is underlain by residual soils and rocks of Vryheid Formation, in the Eccu Group, Karoo Supergroup. This comprises predominantly of sandstone, gritstone and arkose as well as mudrock and shale interbedded with coal seams. The regional geology is shown in Figure 2, included at the end of this report.

Weathering has produced soil profiles of variable thickness, the upper reaches of which are typically moderately to highly expansive, as decomposition of the feldspar minerals within these rocks form clays from the smectite group, which are present to considerable depth. The assumption that founding conditions typically improve with depth are not necessarily valid for heavy structures as weak strata may underly competent strata [2].

A more detailed overview of the regional geology is presented in the report by JG Afrika (2016).

5. GEOHYDROLOGY

A geohydrological investigation was conducted by GCS Water & Environmental Consultants near the proposed sedimentation tank and flocculator during the same period as the geotechnical investigation. This included a hydro census and the drilling of additional groundwater monitoring boreholes. It was found from the study that a shallow water table was present at approximately 1m below the old System 1A excavation floor level i.e. at the 1435.00 level. Dewatering will therefore be required during construction as the excavation for the sedimentation tank will be below the water table.

Modelling was done by GCS for an assumed 12-month earthworks construction period to determine the water table draw down cone. The modelling showed that the existing sedimentation tanks to the north (System 5 Tanks U and V) will be affected by the dewatering. These tanks are constructed on expansive clay soils which should be kept at a high moisture content to prevent drying out and shrinkage of the clay. This may result in settlement of Tanks U and V taking place. The soil moisture content will increase once the dewatering stops which will result in the clay swelling and may result in upward tank movement. It should be noted that the tank movement due to the drying out and re-wetting of the clay may not be uniform. This will have to be monitored during construction by installing survey points on Tanks U and V and conducting weekly surveys. Movement which is above the values specified by Rand Water and the Engineer may require dewatering to be temporarily stopped until it has stabilised.

A herringbone drain system is proposed by GCS which will drain the water into a sump which will be located at the north-west corner of the excavation. The sump will be pumped to keep the water table at the 1433.00 level which will be the deepest section of the excavation for the new sedimentation tank.

6. CLIMATE

As per JG Afrika's report, regional rainfall for Vereeniging is approximately 560 mm per annum with temperatures varying between 0° C and 28° C. Summers are usually dry and hot with winters typically cold and wet. The site is located within a humid area where Weinert's N-value is less than 5, which indicates that chemical decomposition is the dominant weathering mode [3].

7. SEISMICITY

According to the report by JG Afrika, the site has a peak ground acceleration of 0,15g (gravitational acceleration) with a 10% probability of exceedance within a 50-year period, which may result from either natural or mining induced seismicity and classifies the site as "Ground Type 4" in terms of SANS 10160-4 [4].

8. METHOD OF INVESTIGATION

The geotechnical investigation was sub-divided into two components: pipeline investigations by means of TLB test pit excavation and excavator test pits for the sedimentation tank and flocculator. This is discussed below.

8.1 FIELDWORK

TLB test pits for the pipelines were excavated between 19 and 21 November 2018 using a CAT 422E TLB. Excavator test pits were excavated within the old System 1A area on 22 and 23 November 2018 using a CAT 320D (20-ton) excavator. Both the TLB and excavator were provided by V&S Cat Hire.

Underground service detection information was provided by RW to KP to assist with the planning of the test pit positions. The test pit positions are shown in Figure 3 and the test pit profile logs are given in Appendix A.

Soil profiling was undertaken by an engineering geologist according to standard practice [5]. The test pit positions were recorded with a hand held GPS (accuracy $\pm 5\text{m}$). Test pit and site photographs are given in Appendix B. The test pits and borehole logs from the work by JG Afrika have been included for reference purposes in Appendix D.

8.1.1 PIPELINE INVESTIGATION

Test pits TP1 to TP11 were excavated for the pipeline investigation. There were services that were encountered during the test pit excavation that were not indicated on the service detection drawing. It was then decided to use hand excavation for most of the test pits to avoid damaging services.

Thandi Projects is a contractor who was on site since May 2018 and was busy with a large number of trench excavations, which is understood to be mostly for a new fire hydrant pipeline. The trench excavations had prevented access for the TLB at some of the planned test pit positions and in general made access difficult. Only two test pits (TP1 and TP2) could therefore be excavated by the TLB.

Thandi Projects provided labourers to assist KP with the hand excavation. Some of the existing trenches were excavated deeper to provide additional soil profile information. The soils in the open trenches were also profiled.

8.1.2 SEDIMENTATION TANK AND FLOCCULATOR

Excavator test pits TP12 to TP16 and TP16A were excavated by KP for the new System 1 sedimentation tank and flocculator to supplement the JG Africa test pit and borehole information.

8.2 PIPELINE GENERAL SOIL PROFILE

The soil profile along the pipelines is summarized below.

8.2.1 EAST OF FILTER HOUSE NO. 2

The soil profile at TP1 to TP4 is as follows from top to bottom:

- 0,9m to 1,95m thick fill at TP1 to TP3 generally comprising loose to medium dense clayey silty sand with slag and ash. There is thicker fill at TP4, which is at least 2,1m thick and has a higher clay content.
- The fill is underlain by transported soils, interpreted to be alluvial in origin, and comprising soft to firm silty clay to a depth of at least 3,7m, which was the maximum reach of the TLB.

Slight water seepage was encountered in TP4 at a depth of 1,6m below the ground surface.

8.2.2 SYSTEM 3 AND SYSTEM 5 SEDIMENTATION TANKS

The soil profile at TP5 to TP7 comprises highly variable fill, which extends to a depth of at least 2,2m (at TP5) comprising very loose to medium dense sandy silty gravel with building rubble, ash and slag. The fill also contains soft to stiff clayey sand with ash and slag.

Side wall collapse occurred at TP7, which limited the test pit depth to 1,1m due to safety reasons.

A geological section for the proposed sludge pipeline from manhole MH1 to MH16 is shown in Figure 5. All the excavation is expected to be soft according to SANS 1200DB.

8.2.3 EAST OF SYSTEM 5 FLOCCULATOR

The soil profile at TP8 and TP10 is as follows:

- Interlocking paving layer.
- 0,2m to 0,4m thick engineered fill comprising distinct layers of dense to very dense silty sand with gravel.
- Fill extending to depths of between 1m and 1,9m comprising medium dense to dense silty sand with gravel, ash and slag.
- 0,4m to 0,6m thick topsoil layer occurs below the fill material. This means that fill had previously been deposited on top of the topsoil.
- Ferruginous colluvium comprising medium dense silty sand with ferricrete nodules to a depth of at least 2,5m (at TP10).

Highly variable fill comprising of a large variety of materials extends to a depth of 2m at TP9.

At TP11 the topsoil was covered by a 0,2m thick layer of fill. The topsoil was underlain by ferruginous colluvium with nodular ferricrete, which extends to a depth of at least 1,4m.

8.3 OLD SYSTEM 1A SOIL PROFILE (TP12 TO TP16 AND TP16A)

The old System 1A excavation is approximately 3m to 4m deep and 310m in length by 45m to 75m in width and has been fenced off. The area is highly disturbed and the old System 1A structures have only been partially demolished. The excavator test pits were excavated at the floor level of the excavation and these have subsequently been surveyed. Historical satellite imagery corroborates the disturbance in this area, and the origin of the upper expansive soils remains uncertain.

The soil profile at TP12 and TP13 is as follows from top to bottom:

- 2,8m to 3,8m thick fill comprising soft clayey sand.
- The upper reaches of the fill are organic-rich, and the lower reaches comprises very soft to firm clayey sand with sandstone and quartzite cobbles.
- Residual mudstone or shale was encountered from depths of 4,8m and 3,8m at TP12 and TP13 respectively. At TP12 the residual mudstone is overlain by a 2m thick layer of residual carbonaceous shale comprising firm clayey sandy silt.
- Excavator refusal occurred on very soft to soft rock shale from a depth of 5m at TP13.

Slow water seepage was observed in TP12 from a depth of 3,5m.

TP15 was the deepest test pit with a depth of 6m but there was no excavator refusal on residual shale, which comprised stiff to very stiff sandy clayey silt.

Fill was encountered in TP14 from the ground surface to the test pit depth of 4,9m. The fill comprises concrete blocks and builders' rubble within a silty clay or sandy soil matrix.

Shallow excavator refusal occurred on concrete slabs at TP16 and TP16A at depths of 0,2m and 1,4m respectively.

The test pits were positioned by the KP geologist in between the partially demolished System 1A structures. It must be noted that there is still a great deal of remaining concrete that needs to be demolished before the earthworks and construction of the new sedimentation tank and flocculator can commence. The concrete rubble could be stockpiled north of the System 4 sedimentation tanks where material has been stockpiled previously. A mobile crusher could be used to crush the concrete to produce suitable backfill material although there is significant reinforcing in the concrete, which will have to be removed and this can complicate the crushing process.

A summary of the test pit profiles is presented in Table 1.

According to the JG Africa report the rock depth varies from 5,1m to 10,74m below the floor level of the old System 1A excavation. The rock is highly variable and comprises interbedded sandstone, siltstone, mudstone, carbonaceous mudstone and tillite.

9. LABORATORY TESTING

Representative disturbed and undisturbed samples were taken from the test pits, both along the pipeline route and within the proposed sedimentation tank footprint. These were submitted to Civilab in Johannesburg for laboratory testing. The laboratory results are presented in Appendix C and a summary of the results are given in Table 2.

The following tests have been carried out:

- 20 x Foundation indicator (grading, Atterberg limits and clay content)
- 10 x Moisture content
- 5 x Modified AASHTO compaction and CBR
- 3 x Compactibility to determine the suitability of materials for pipe bedding
- 4 x Basson's Index to assess the potential for soils to corrode concrete and steel
- 2 x Falling head permeability on remoulded samples
- 1 x Consolidation test
- 1 x Free swell test

9.1 PIPELINE RESULTS

The transported soils encountered are considered to range in origin from topsoil to colluvium and alluvium. Due to the highly disturbed nature of the site, even along the pipeline route, some uncertainty regarding the origin of the latter exists. The results are presented with reference to the general profile for each of the proposed structures below.

9.1.1 EAST OF FILTER HOUSE NO.2

The fill is encountered in the upper reaches of the profile and varies significantly in grading, viz. gravel (2% to 51%), sand (24% to 48%), silt (11% to 26%) and clay (14% to 24%). The Plasticity Index (PI) varies between 19% and 26%, which results in a low to medium potential expansiveness [6]. The Unified Soil Classification (USC) of the fill varies from, GC (clayey gravel) to CL (clays of low to medium plasticity). The natural moisture content is 17,3% at 1,6 m in test pit TP04, and the fill is regarded as highly corrosive to steel and mildly aggressive towards concrete.

Alluvium underlies the fill and was encountered in TP01 and TP02, and the interpretation of origin is based on the typical composition, viz. gravel (1% to 6%), sand (31% to 39%), silt (18% to 19%) and clay (42% to 44%), with the latter typical of alluvial soils. High liquid limits (LL) of 51% to 66% in combination with the clay content, result in high to very high potential expansiveness and a USC of CH (clays of high plasticity). The natural moisture content varies from 14,7% to 34,6% at depths between 1m to 3,7m.

9.1.2 SYSTEM 3 AND SYSTEM 5 SEDIMENTATION TANKS

In the area between System 3 and 5, the USC for the fill ranges from GM (poorly graded silty gravel) to SC (clayey sands), with the typical composition viz. gravel (21% to 65%), sand (21% to 39%), silt (12% to 15%) and clay (2% to 25%). The PI of the fill varies from slightly plastic (SP) to 33% and the grading moduli from 1,28 to 2,27. The coarse fill (slag and ash) from test pit TP06, qualifies for use as a subbase (G5), with a low maximum dry density of approximately 1500 kg/m³ and a compactibility factor of 0,316. This indicates that the material is unsuitable for use as pipe bedding or backfill, as per RW specification [8].

9.1.3 EAST OF SYSTEM 5 FLOCCULATOR

The fill encountered near the proposed flocculator, specifically at TP10, is comprised of gravel (34%), sand (34%), silt (15%) and clay (16%), with a PI of 16% and a low potential expansiveness. Compaction tests indicate it has a maximum dry density of 1967 kg/m³ at 10,9% moisture content. The PI and grading requirements as per RW specification classifies this material as unsuitable for use as backfill or bedding.

The topsoil has typically been profiled as a clayey silty sand with a pin-holed structure, often accompanied by organic material. The one sample tested of this horizon indicates that the composition, viz. gravel (2%), sand (50%), silt (21%) and clay (27%), poses a moderate potential for expansiveness and has a USC of CL (clays of low to medium plasticity). The organic content of these soils makes it unlikely to be suitable for layer works.

Ferruginous colluvium, underlying the proposed flocculator, is of a slightly variable composition, viz. gravel (29% to 36%), sand (31% to 38%), silt (10% to 14%) and clay (20% to 22%). The PI for this horizon varies between 16% and 29%, indicating a low potential for expansiveness. Grading moduli range from 1,31 to 1,68 with the USC of SC (clayey sands).

Neither the topsoil or the ferruginous colluvium qualifies for use as backfill or bedding in accordance with the RW specification [8].

9.2 OLD SYSTEM 1A EXCAVATION RESULTS

Fill encountered within the Old system 1A area varies considerably in grading, viz. gravel (5% to 51%), sand (23% to 42%), silt (8% to 19%), clay (18% to 46%). The PI varies from 31% to 41% with the LL from 55% to 66%. This results in low to medium potential expansiveness in the clayey sand soils (SC) and high to very high potential expansiveness in the high plasticity clays (CH). Grading moduli range from 0,57 to 1,95, and natural moisture contents varying between 23,6% and 31,4% at depths of 0,0 m-2,8 m. The drained shear strength parameters for the fill/alluvium from TP13 are shown below.

Effective Internal friction angle (ϕ) : 22,8°

Effective cohesion (c') : 24,9 kPa.

The above strength parameters are in line with typical values expected for a sandy clay. This in combination with the noted sidewall collapse, as well as high degree of potential expansiveness, indicates the necessity for battering of sidewalls in excavations, during all phases of work on the pipeline, sedimentation tank and flocculator, where this material may be encountered..

Reworked residual sandstone underlies the transported soils and comprises gravel (3% to 5%), sand (20% to 83%), silt (9% to 41%) and clay (3% to 36%). The PI for the soils varies from 13% to 25% with LL from 31% to 45%, resulting in a low to medium potential expansiveness. Grading moduli range from 0,42 to 1,58 with the former having a USC of CL (clays of low plasticity) and the latter SC (sandy clay). Natural moisture contents vary from 14% to 19,4% at depths between 1,3m to 6m.

Both carbonaceous and non-carbonaceous soils were encountered with grouped compositions, viz. gravel (0% to 5%), sand (22% to 30%), silt (36% to 57%) and clay (13% to 37%), with the former profiled as a sandy silt and the latter as a sandy silty clay. Similar liquid limits of 36% and 39% combined with PI's of 13% and 18% respectively, result in a low degree of potential expansiveness for both soils. The USC for the residual shales varies from CI to CL (clays of low to intermediate plasticity) respectively. The disparities in the results are likely linked to the degree of reworking in the residual shale from TP13.

The Basson's index for all the fill tested indicates that the soils are highly corrosive towards steel and mildly to highly aggressive towards concrete. The fill is not suitable for backfilling around conventional pipes and therefore corrosion protection of steel pipes, or PVC/HDPE pipe materials should be considered.

In addition to the above, one sample of the stockpiled material from north of System 4 sedimentation tanks was also tested (WBA2). The results indicate that the material mostly likely came from below the old System 1A structure and correlates well with the results obtained for the reworked residual sandstone.

10. GEOTECHNICAL EVALUATION

10.1 GENERAL

Design information for the sedimentation tank and flocculator is shown on the former Bosch Stemele PDF drawings R0 21709 to R0 21712 (dated 2012) that were forwarded to KP for information by Rand Water. According to the drawings the flocculator will be 30m in diameter while the sedimentation tank will be 240m in length by 51m in width with a typical wall height of 4,2m. The sedimentation tank will have a sloping floor from east to west with a 0,8m elevation difference over the length of the tank. The underside (i.e. bottom) of the 0,3m thick concrete floor levels vary from 1436.12 to 1436.86. The drawings show that the foundation wall levels are similar to the bottom of the floor levels. The flocculator depth is variable but the deepest central section has a bottom floor level of 1435.91.

The excavation for the removal of the old System 1A structures that was undertaken by the previous contractor is generally close to the founding level of the sedimentation tank. The excavation floor levels typically vary from 1436.5 to 1437.0 although the central portion of the excavation has a higher elevation of 1439.0 as some of the material had not been removed by the contractor. There are still a large number of old System 1A concrete structures remaining in the excavation as they have only been partially demolished. These structures will need to be demolished down to the recommended KP excavation levels. The demolished material could be stockpiled on site and possibly re-used for backfilling if it is crushed to a suitable size using a mobile crusher.

It may be possible for structures that are below the recommended excavation levels to remain behind but this will need to be verified by a geotechnical engineer during construction. Any voids in the old concrete structures will need to be filled with mass concrete. Alternatively, the structures will need to be demolished and removed.

Reference was made to the KP test pit information together with the JG Afrika test pit and borehole information [9] to obtain an understanding of the soil and rock conditions at the old System 1A excavation. The KP test pits and JG Afrika boreholes were surveyed by Delta Plan Professional Land Surveyors in 2019 to obtain ground level information, which allowed a direct correlation to be done between the test pit and borehole information.

The test pit and borehole information show that the area has been highly disturbed during the previous excavation by the contractor and large parts have been covered by fill. The in situ soils below the fill are also highly variable and vary from clayey sands with a low to medium potential expansiveness to clays with a very high potential expansiveness. The soils are typically described as moist to very moist (wet in places), which is indicative of shallow water table conditions. The soil consistencies are loose or soft to firm to a typical depth of 2m. Poorer soil conditions occur at the west side of the excavation where very soft to soft clays are present to a typical depth of 3m.

10.2 EARTHWORKS RECOMMENDATIONS

The soft expansive clays are unsuitable for the founding of the sedimentation tank due to the expected excessive settlement of the soils that will occur under the applied bearing pressure. Movement of the expansive soils may occur during wetting (swell) and drying (shrinkage) of the soils, which may also result in unacceptable differential movement of the sedimentation tank. It is therefore recommended that the soft clay soils are excavated and removed to spoil. The required excavation depths will vary according to the thickness of unsuitable soils that have to be removed. This is summarised in Tables 3 and 4 at the end of the report.

The recommended earthworks for the sedimentation tank are as follows:

- From the east wall of the sedimentation tank to a distance of 135m away from the wall excavate to the 1434.50 level to reach medium dense clayey silty sand.
- From a distance of 135m to 240m from the east wall excavate to the 1433.00 level to reach firm clayey silt.
- Compact the excavation floor to 90% of Modified AASHTO maximum dry density (MDD) at optimum moisture content (OMC).
- Backfill the excavation with imported rockfill up to 0,5m below the tank founding levels. Place the rockfill in maximum 500mm thick layers and compact with a minimum of 5 passes with a 10-ton pad foot roller. The maximum rock size must not exceed 350mm.
- Place imported G6 quality material on the rockfill and compact in maximum 200mm thick layers to 95% of Modified AASHTO MDD at OMC up to the required levels.
- Construct a 50mm thick blinding layer on the engineered backfill. The maximum allowable bearing pressure should not exceed 150kPa to limit settlement to less than 10mm.

The excavation must extend 2,5m beyond the sedimentation tank footprint. The excavation side wall slopes should not exceed 1V:1H but should be flattened to 1V:2H at the west side of the excavation where thicker soft clays are present.

The recommended earthworks for the flocculator are as follows:

- Excavate to the 1435.00 level to reach medium dense clayey sand and remove all material to spoil.
- Compact the excavation floor to 90% of Modified AASHTO MDD at OMC.
- Backfill the excavation with imported rockfill up to 0,5m below the flocculator founding levels. Place the rockfill in maximum 500mm thick layers and compact with a minimum of 5 passes with a 10-ton pad foot roller. The maximum rock size must not exceed 350mm.
- Place imported G6 quality material on the rockfill and compact in maximum 200mm thick layers to 95% of Modified AASHTO MDD at OMC up to the required flocculator floor levels.
- Construct a 50mm thick blinding layer on the engineered backfill. The maximum allowable bearing pressure should not exceed 150kPa to limit settlement to less than 10mm.

The excavation must extend 2m beyond the flocculator footprint. The excavation side wall slopes should not exceed 1V:1H.

A schematic excavation drawing for the sedimentation tank and flocculator is shown in Figure 4. The required excavation depths will vary from 1,9m to 3,3m below the sedimentation tank.

The old System 1A excavation is approximately 3m deep and has side walls that are close to vertical, but appear to be stable. The deeper excavation that will be required for the sedimentation tank and flocculator will be located relatively close to the toe of the old System 1A excavation walls. This may compromise the stability of some of the vertical slopes, which could result in localised slip failure. It is therefore recommended that all the vertical slopes around the perimeter of the old System 1A excavation are flattened to 1V:1H to increase the short-term stability. This must be done first before commencing with the excavation for the sedimentation tank.

10.3 EXCAVATION DEWATERING

Dewatering of the excavations will be required in accordance with the GCS dewatering plan. A system of herringbone drains draining towards a pumped sump located at the north-west side of the sedimentation tank excavation will be used for dewatering. Dewatering should only be done during the earthworks construction period, which is expected to take 1 year to complete. Permanent dewatering post-construction should not be undertaken as the water draw down cone will affect the adjacent System 5 Sedimentation Tanks U and V. The clayey soils below these structures may start to dry out resulting in soil shrinkage and soil settlement. Differential settlement of the structures may then occur, which could lead to leaking joints and also damage to pipework.

A possible method to safeguard the adjacent System 5 Sedimentation Tanks U and V to the north and the System 3 tanks to the west of the sedimentation tank from differential settlement due to de-watering would be to construct a sheet pile wall. The wall would have an approximate length of 280m at the north side of the sedimentation tank and 90m at the west side of the tank. The wall will need to be installed from the floor of the excavation and extend down to the rock level 6m below. The wall will contain the groundwater at the System 5 and System 3 sides and away from the sedimentation tank excavation.

The estimated cost for the wall installation by a specialist geotechnical contractor is in the region of R8 million.

10.4 CONSTRUCTION RECOMMENDATIONS

The excavations must be inspected by a geotechnical engineer during construction. This will include a visual assessment of the side walls and also whether adequate founding conditions have been reached for the sedimentation tank and flocculator before proceeding with backfilling. Deeper over-excavation may be required by the engineer should localised poorer soil conditions be encountered. At least 5 visits should be allowed for by a geotechnical engineer during construction. Backfilling may not commence until the excavations have been inspected and signed off by a geotechnical engineer.

Laboratory testing of the G6 material will be required to ensure that it meets the required COLTO specification. This will include foundation indicator, Modified AASHTO and CBR tests. The test results must be submitted to the geotechnical engineer for approval. Troxler density tests and sand replacement tests must be conducted on the G6 material to ensure that it meets the required 95% of Modified AASHTO compaction specification.

Survey points should be placed on the structures and weekly surveys should be undertaken during construction to monitor movement. Dewatering may need to be stopped should movement occur at Sedimentation Tanks U and V outside the specified values by Rand Water and the Engineer.

It is recommended that the excavation for the sedimentation tank should proceed from east to west (i.e. shallower excavation done first before proceeding with the deeper excavation) to avoid working below the water table for as long as possible.

A large volume of rockfill will be required for backfilling. One possible source of material could be the Seriti New Vaal Colliery which is located approximately 4km east of the Vereeniging Pump Station. This may be more cost effective than importing material from a commercial source.

Spoil and stockpile areas for material removed from the old System 1A excavation need to be identified. Demolished concrete could possibly be stockpiled north of the System 4 sedimentation tanks at the existing demolished concrete stockpile. A designated spoil area for the clay soils needs to be identified at the Vereeniging Pump Station. Alternatively, the material will have to be removed off site.

10.5 PIPELINE RECOMMENDATIONS

All excavations of a temporary nature for installation of pipelines, must be excavated to a slope not steeper than 1H:0,6V for safety reasons. The excavation slope may have to be further flattened to 1H:1V or appropriate shoring must be installed for the required duration of work, should this be required. It is recommended that most of the excavations are made by hand to the required pipe invert levels so as to minimise damage to existing services.

It is likely that pipe trench dewatering will be required to the east of Filter House No.2 as well as east of the System 5 Flocculator, and provision for dewatering equipment must be made. All materials for pipe bedding and backfilling are to be imported as no suitable materials which meet the RW specification were encountered on site. All imported materials and construction of pipelines are to follow RW specifications [8].

Rand Water requires the elastic modulus (E_s) values of subsoil materials along the pipeline route. The results of plate load bearing or triaxial tests provide the parameters to calculate the E-value. These tests were not carried out and estimated ranges of the E-values are provided in Table 2.

It should be noted that the moisture condition of the test pits influences the modulus of elasticity. A cohesive soil that increases in moisture content will decrease in consistency and thus have a decrease in the modulus of elasticity.

11. CONCLUSION

The current geotechnical investigation by KP and previous drilling investigation by JG Afrika in 2016 shows that the soils at the old System 1A excavation are highly variable and comprise from clayey sands with a low to medium potential expansiveness to clays with a very high potential expansiveness. Thicker soft clays are present at the west side of the excavation and typically extend to depths of 3m. The excavation has been highly disturbed and large areas have been covered by fill. There are a number of remaining old System 1A structures, which have been partially demolished and still need to be removed before construction of the sedimentation tank may proceed.

The excavation must be deepened to remove unsuitable soils below the proposed position of the sedimentation tank to the 1434.50 and 1433.00 levels. The required excavation depths will vary from 1,9m to 3,3m below the tank. The excavation must be backfilled with rockfill in maximum 500mm thick layers with G6 material placed in maximum 200mm thick layers compacted to 95% of Modified AASHTO MDD at OMC on the rockfill.

The required excavation level for the flocculator is 1435.00. Backfilling below the structure must be as for the sedimentation tank.

The excavations will need to be dewatered due to the presence of a shallow water table as per the GCS plan. There is a risk of differential settlement of the adjacent System 5 Sedimentation Tanks U and V and the tanks to the west of the sedimentation tank. A sheet pile wall may be considered as an option to mitigate this at an estimated cost of R8 million. The wall will contain the groundwater at the System 5 and System 3 sides and away from the sedimentation tank excavation.

The excavations must be inspected by a geotechnical engineer during construction. This will include a visual assessment of the side walls and also whether adequate founding conditions have been reached for the sedimentation tank and flocculator before the contractor may be allowed to proceed with backfilling. This is a key holding point during the earthworks construction.

Imported backfill materials for pipelines will be required as no suitable backfill material is available on site. Dewatering of pipe trenches will be required in some places. Hand excavation should be used for most of the pipe trench excavations to avoid damaging existing services.

12. REFERENCES

- [1] Department of Mineral and Energy Affairs and the Geological Survey, *Geological Map of the West Rand*, Sheet No. 2626, 1:250 000 scale, 1986.
- [2] Brink, A.B.A., *Engineering Geology of Southern Africa: The Karoo Sequence* (Vol. 3). Building Publications 1983.
- [3] Weinnert, H.H. *The natural road construction materials of South Africa*. H and R Academica (Pty) Ltd. Pretoria 1980.
- [4] South African Bureau of Standards SANS 10160 Part 4. *Seismic actions and general requirements for buildings*. Pretoria 2016.
- [5] South African Bureau of Standards SANS 633. *Soil profiling and rotary percussion borehole logging on dolomite land in Southern Africa for engineering purposes*. Pretoria 2012.
- [6] Van der Merwe, D.H. *The Prediction of Heave from the Plasticity Index and Percentage Clay Fraction*. Trans. S.A. Ins. Civ. Eng. No. 6, 1964.
- [7] Hunt, R.E. *Geotechnical Engineering Techniques and Practices*, McGraw-Hill, 1986, ISBN 0-07-031310-5.
- [8] Rand Water, *Technical Specification for Pipeline Excavation, Backfilling and Pipe Trenches and Pipe Laying, Special and Testing and Investigations and Returnable Schedules (TS)*, Doc No. SAM DOP 00001 TS, Rev No.1, June 2018.
- [9] Rand Water. *Sedimentation and Flocculation Plant at Vereeniging Pumping Station Geotechnical Report*. JG Afrika (Pty) Ltd 2016.

13. CERTIFICATION

This report was prepared and reviewed by the undersigned.

Prepared:



DEON BESTER Pr.Sci.Nat.
Junior Engineering Geologist

Reviewed:



MICHAEL PLICHTA PrEng
Senior Geotechnical Engineer

This report was prepared by Knight Piésold Ltd. for the account of RAND WATER. Report content reflects Knight Piésold's best judgement based on the information available at the time of preparation. Any use a third party makes of this report, or any reliance on or decisions made based on it is the responsibility of such third parties. Knight Piésold Ltd. accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this report. Any reproductions of this report are uncontrolled and might not be the most recent revision.

RAND WATER
 VEREENIGING PUMPING STATION:
 GEOTECHNICAL INVESTIGATION
 225ML SEDIMENTATION TANK, FLOCCULATOR AND ASSOCIATED SYSTEM 1 PIPELINES

TABLE 1. SUMMARY OF TEST PIT PROFILES

Test Pit No.	Total Depth (m)	Refusal	Thickness of Layers (m) – (m)										Depth to Seepage (m)
			Transported Soil					Residual Soil			Pedogenic Nodular/ *Honeycomb/ **Hardpan Ferricrete	Rock Shale	
			Fill	Topsoil	Colluvium	Hillwash	Alluvium	Reworked Residual Sandstone	Carbonaceous Shale	Reworked Shale/Mudrock			
TP01	3,70	T	0,0-1,0	-	-	-	1,0-3,7	-	-	-	-	-	-
TP02	3,65	T	0,0-1,95	-	-	-	1,95-3,65	-	-	-	-	-	-
TP03	1,40	T	0,3-0,9	0,0-0,3	-	-	0,9-1,4	-	-	-	-	-	-
TP04	2,10	T	0,0-2,1	-	-	-	-	-	-	-	-	-	-
TP05	2,20	T	0,0-2,2	-	-	-	-	-	-	-	-	-	-
TP06	1,90	T	0,0-1,9	-	-	-	-	-	-	-	-	-	-
TP07	1,10	T	0,0-1,1	-	-	-	-	-	-	-	-	-	-
TP08	2,10	T	0,0-1,0	1,0-1,6	1,6-2,1	-	-	-	-	-	-	-	-
TP09	2,00	T	0,2-2,0	0,0-0,2	-	-	-	-	-	-	-	-	-
TP10	2,50	T	0,0-1,9	1,9-2,3	2,3-2,5	-	-	-	-	-	-	-	-
TP11	1,40	T	0,0-0,2	0,2-0,6	-	0,6-1,1	-	-	-	-	1,1-1,4	-	-
TP12	5,20	NR	0,0-2,8	-	-	-	-	-	2,8-4,8	4,8-5,2	-	-	3,5
TP13	5,00	R	0,0-3,8	-	-	-	-	3,8-5,0	-	-	-	5,0+	-
TP14	4,90	T	0,0-4,9	-	-	-	-	-	-	-	-	-	4,0
TP15	6,00	T	0,0-1,3	-	-	-	-	1,3-5,0	-	5,0-6,0	-	-	2,0
TP16	0,15	R	0,0-0,15	-	-	-	-	-	-	-	-	-	-
TP16A	1,40	R	0,0-1,4	-	-	-	-	-	-	-	-	-	-

Notes: NR - Near Refusal
 T - Terminated by Geologist
 R - Refusal

TABLE 2
SUMMARY OF LABORATORY TEST RESULTS

Sample No.	Depth (m-m)	Grading %				Atterberg Limits %			GM	PE	USC	Proctor Compaction		Natural Moisture Content (%)	Relative Density (S.G.)	Free Swell (%)	CBR (Modified AASHTO) TMH1 A7							Maximum Dry Density (kg/m ³) & OMC	Compact-ibility Factor	Falling Head - Remoulded Avg Permeability (100 KPa)	Basson's Index	Material Description	Estimated Range of Modulus of Elasticity E _s (MPa)		
		Gravel	Sand	Silt	Clay	LL	PI	LS				MDD (kg/m ³)	OMC (%)				% Swell	90%	93%	95%	97%	98%	100%								
TP01/1	1.00 - 1.70	1	39	18	42	51	32	15,5	0,55	High	CH	-	-	14,7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	Interpreted as Alluvium	2 – 4
TP01/2	1.70 - 3.70	6	31	19	44	64	42	17	0,55	V.high	CH	-	-	34,6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	Interpreted as Alluvium	2 – 4	
TP02/1	0.90 - 1.40	51	24	11	14	49	26	13,5	1,87	Low	GC	1828	14,3	-	-	-	8,4	2	2	2	2	2	2	1828 @ 14.3	-	-	Highly corrosive and mildly aggressive	Fill	6 – 20		
TP04/1	1.60 - 2.10	2	48	26	24	32	19	9	0,59	Med	CL	-	-	17,3	-	-	-	-	-	-	-	-	-	-	-	-	-	Fill	8 – 12		
TP05/1	1.40 - 2.20	21	39	15	25	55	33	16	1,28	Med	SC	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	Fill	-		
TP06/1	0.20 - 1.20	65	21	12	2	NA	SP	1	2,27	Low	GM	1497	18,7	-	-	-	0,1	24	38	52	71	83	114	1497 @ 18.7%	0,316	-	-	Fill	-		
TP08/1	1.00 - 1.60	2	50	21	27	33	18	9,5	0,64	Med	CL	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	Topsoil	10 – 30		
TP08/2	1.60 - 2.10	39	31	10	20	50	29	13	1,68	Low	SC	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	Ferruginous Colluvium	8 – 20		
TP10/1	0.6 - 1.90	34	34	15	17	32	16	8	1,47	Low	SC	1967	10,9	-	-	-	0,8	8	11	15	19	21	27	1967 @ 10.9%	0,333	-	Highly corrosive and mildly aggressive	Fill	15 – 40		
TP10/2	2.30 - 2.50	26	38	14	22	34	16	7	1,31	Low	SC	-	-	15,9	-	-	-	-	-	-	-	-	-	-	-	-	-	Ferruginous Colluvium	8 – 20		
TP12/1	0.00 - 1.30	10	40	18	32	55	34	16	0,85	High	CH	-	-	23,6	-	-	-	-	-	-	-	-	-	-	-	-	-	Fill	2 – 4		
TP12/2	1.90 - 2.80	15	42	19	24	66	36	18	1,16	Med	SC	-	-	31,4	-	-	-	-	-	-	-	-	-	-	-	-	-	Fill	2 – 4		
TP12/3	2.80 - 4.80	0	30	57	13	36	13	5	0,24	Low	CI	-	-	23,7	-	-	-	-	-	-	-	-	-	-	-	-	-	Residual Carbonaceous Shale	8 – 20		
TP13/1	1.20 - 1.40	5	31	18	46	66	41	17,5	0,57	V.high	CH	-	-	-	2,519	1,91	-	-	-	-	-	-	-	-	-	-	-	Fill	2 – 4		
TP13/2	3.80 - 5.00	5	22	36	37	39	18	9,5	0,5	Low	CL	-	-	-	-	-	-	-	-	-	-	-	-	-	-	Highly corrosive and aggressive	Reworked Residual Shale	8 – 20			
TP15/1	0.50 - 1.30	51	23	8	18	60	31	15,5	1,95	Low	SC	1702	16	-	-	-	3,8	2	2	3	3	3	3	1702 @ 16%	-	4,1E-08	-	Fill	-		
TP15/2	1.30 - 2.40	3	42	20	35	45	25	11,5	0,61	Med	CL	-	-	19,4	-	-	-	-	-	-	-	-	-	-	-	-	-	Reworked Residual Sandstone	2 – 20		
TP15/3	2.40 - 5.00	5	83	9	3	31	13	6,5	1,58	Low	SC	-	-	14	-	-	-	-	-	-	-	-	-	-	-	Highly corrosive and aggressive	Reworked Residual Sandstone	2 – 20			
TP15/4	5.00 - 6.00	3	20	41	36	34	13	7	0,42	Low	CL	-	-	15,3	-	-	-	-	-	-	-	-	-	-	-	-	-	Reworked Residual Sandstone	2 – 20		
WBA2	Stockpile	39	32	14	15	41	23	11,5	1,66	Low	SC	1913	12,3	-	-	-	1,9	5	7	8	11	12	15	1913 @ 12.3%	0,366	3,2E-09	-	Fill	-		

ABBREVIATIONS

LL	: Liquid Limit	OMC	: Optimum Moisture Content
PI	: Plasticity Index	S.G.	: Specific gravity
LS	: Linear Shrinkage	CH	: Clay with high plasticity
GM	: Grading Modulus	GC	: Clayey gravel
PE	: Potential Expansiveness	CL	: Low plasticity clay
USC	: Unified Soil Classification	SC	: Clayey sand
MDD	: Maximum Dry Density	GM	: Silty gravel

RAND WATER
 VEREENIGING PUMPING STATION:
 GEOTECHNICAL INVESTIGATION
 225ML SEDIMENTATION TANK, FLOCCULATOR AND ASSOCIATED SYSTEM 1 PIPELINES

TABLE 3. MINIMUM FLOCCULATOR AND SEDIMENTATION TANK EXCAVATION LEVELS

BOREHOLE / TEST PIT NO.	GROUND LEVEL	REQUIRED EXCAVATION DEPTH FROM GROUND SURFACE (m)	MINIMUM EXCAVATION LEVEL	BOTTOM OF STRUCTURE LEVEL	MINIMUM EXCAVATION DEPTH BELOW BOTTOM OF STRUCTURE (m)
BOREHOLES					
BH1*	1438,712	3,50	1435,210	1435,910	0,700
BH2	1436,476	N/A (no structure)	-	-	-
BH3	1436,505	2,00	1434,505	1436,800	2,295
BH4**	1436,500	2,00	1434,500	1436,800	2,300
BH5	1439,060	4,25	1434,806	1436,650	1,844
BH6	1436,978	2,30	1434,677	1436,400	1,723
BH7	1436,888	3,00	1433,888	1436,300	2,412
BH8	1436,815	2,70	1434,115	1436,250	2,135
TEST PITS					
TP12	1436,535	3,00	1433,535	1436,300	2,765
TP13	1436,722	3,50	1433,222	1436,200	2,978
TP14	1437,306	2,50	1434,806	1436,600	1,794
TP15	1437,077	2,40	1434,677	1436,490	1,813
TP16	1436,759	Unknown: shallow test pit	-	1436,700	-
TP16A	1436,072	Unknown: shallow test pit	-	1436,700	-

Notes:

- * Borehole drilled at proposed flocculator.
- ** No survey data. Estimated ground level.

RAND WATER
 VEREENIGING PUMPING STATION:
 GEOTECHNICAL INVESTIGATION
 225ML SEDIMENTATION TANK, FLOCCULATOR AND ASSOCIATED SYSTEM 1 PIPELINES

TABLE 4. RECOMMENDED FLOCCULATOR AND SEDIMENTATION TANK EXCAVATION LEVELS

BOREHOLE / TEST PIT NO.	GROUND LEVEL	REQUIRED EXCAVATION DEPTH FROM GROUND SURFACE (M)	RECOMMENDED EXCAVATION LEVEL	BOTTOM OF STRUCTURE LEVEL	MINIMUM EXCAVATION DEPTH BELOW BOTTOM OF STRUCTURE (M)
BOREHOLES					
BH1*	1438,712	3,71	1435,00	1435,910	0,910
BH2	1436,476	N/A (no structure)	-	-	-
BH3	1436,505	2,01	1434,50	1436,800	2,300
BH4**	1436,500	2,00	1434,50	1436,800	2,300
BH5	1439,060	4,56	1434,50	1436,650	2,150
BH6	1436,978	2,48	1434,50	1436,400	1,900
BH7	1436,888	3,89	1433,00	1436,300	3,300
BH8	1436,815	3,82	1433,00	1436,250	3,250
TEST PITS					
TP12	1436,535	3,54	1433,00	1436,300	3,300
TP13	1436,722	3,72	1433,00	1436,200	3,200
TP14	1437,306	2,81	1434,50	1436,600	2,100
TP15	1437,077	2,58	1434,50	1436,490	1,990
TP16	1436,759	2,26	1434,50	1436,700	2,200
TP16A	1436,072	1,57	1434,50	1436,700	2,200

Notes:

* Borehole drilled at proposed flocculator.

** No survey data. Estimated ground level.



onville

Powerville

VEREENIGING
PUMP STATION

Vereeniging

Vaal River



COMPANY'S PHOTOGRAPHS AND THE INFORMATION THEREON IS NOT
TO BE USED IN ANY MANNER OR FOR ANY PURPOSES WITHOUT THE WRITTEN
CONSENT OF THE COMPANY.

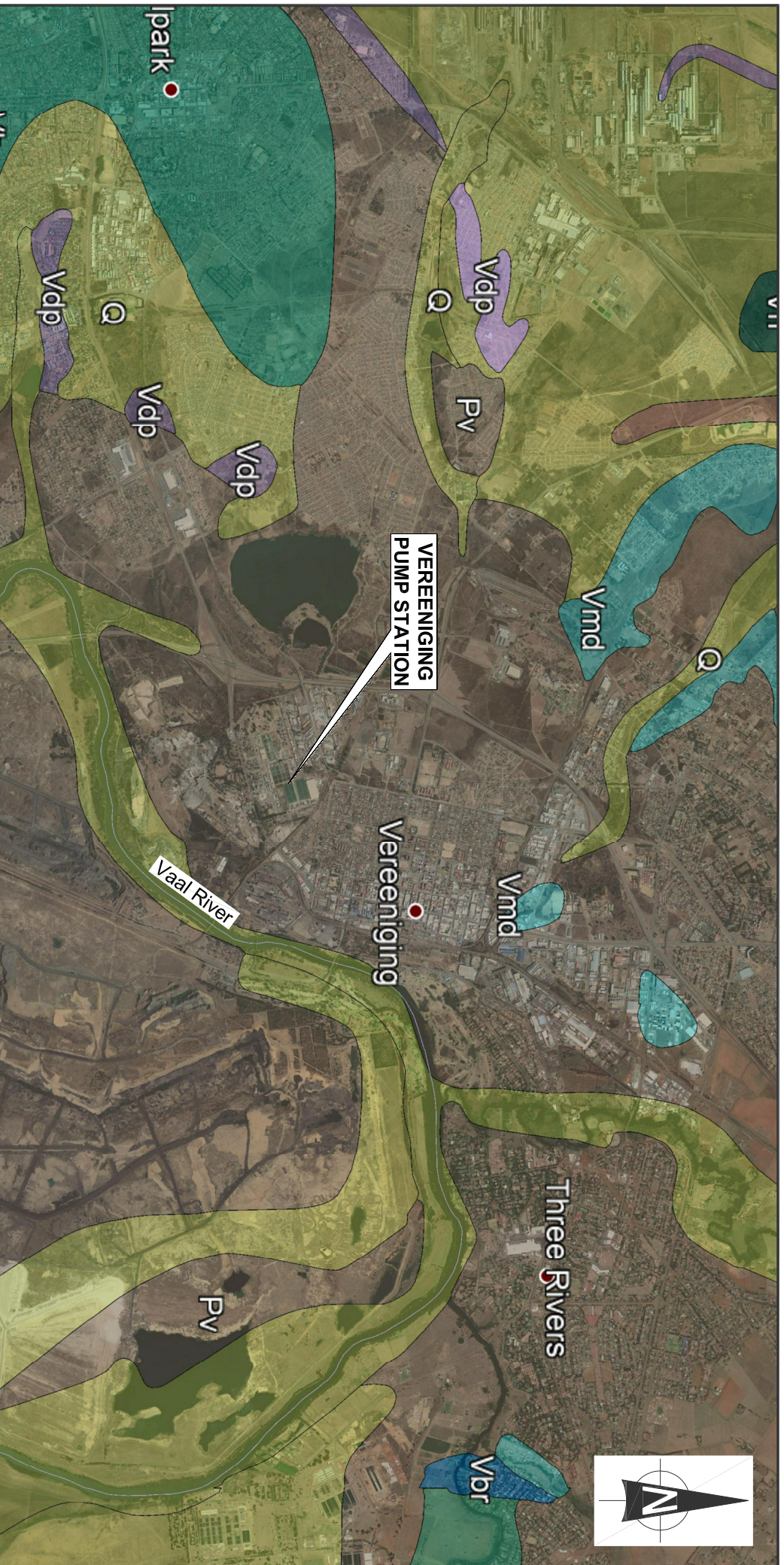
**VEREENIGING PUMP STATION
SYSTEM 1 GEOTECHNICAL INVESTIGATION**

LOCALITY PLAN

PROJECT NO: 30300496/03

FIGURE NO 1

SCALE N.T.S.



GEOLOGICAL LEGEND:

- Q : Soil cover, river sand, diamondiferous gravels
- Qa : Alluvium
- Os : Aeolian sand
- Pv : Shale, sandstone, coal of the Vryheid Formation, Eccca Group, Karoo Supergroup.
- Vdp : Quartzite, shale, ferruginous in places of the Daspoort Formation, Pretoria Group, Transvaal Supergroup.
- Vmd : Dolomite of the Malmani Subgroup, Chuniespoort Group, Transvaal Supergroup.

REFERENCE MAP
GEOLOGICAL SERIES
WEST RAND GEOLOGY
NOT TO ORIGINAL SCALE



KNIGHT PIÉSOLD CONSULTING
REGISTERED PROVIDER OF PROFESSIONAL SERVICES IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL ENGINEERS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL GEOTECHNICAL ENGINEERS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL GEOLOGISTS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL CHEMISTS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL ARCHITECTS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL SURVEYORS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL AGRICULTURAL ENGINEERS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL MECHANICAL ENGINEERS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL ELECTRICAL ENGINEERS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL CIVIL ENGINEERS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL METALLURGICAL ENGINEERS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL CHEMISTS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL ARCHITECTS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL SURVEYORS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL AGRICULTURAL ENGINEERS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL MECHANICAL ENGINEERS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL ELECTRICAL ENGINEERS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL CIVIL ENGINEERS IN THE
REPUBLIC OF SOUTH AFRICA
MEMBER OF THE ASSOCIATION OF PROFESSIONAL METALLURGICAL ENGINEERS IN THE
REPUBLIC OF SOUTH AFRICA

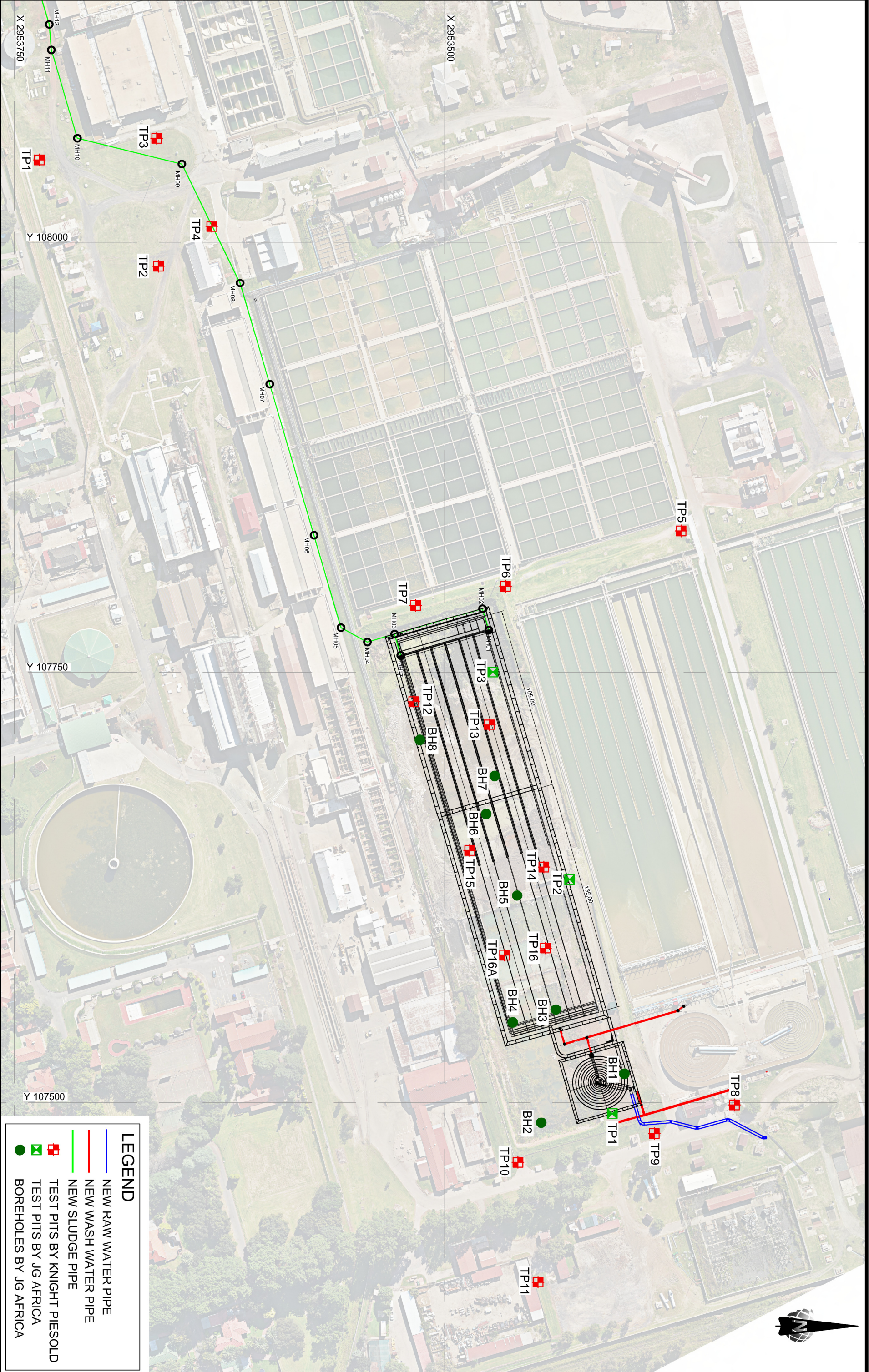
**VEREENIGING PUMP STATION
SYSTEM 1 GEOTECHNICAL INVESTIGATION**

GEOLOGY PLAN

PROJECT NO: 303004966/03

FIGURE NO 2

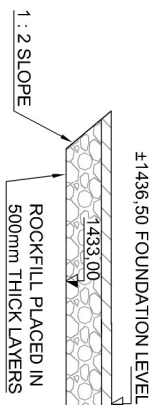
SCALE N.T.S.



LEGEND	
	NEW RAW WATER PIPE
	NEW WASH WATER PIPE
	NEW SLUDGE PIPE
	TEST PITS BY KNIGHT PIESOLD
	TEST PITS BY JG AFRICA
	BOREHOLES BY JG AFRICA

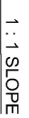
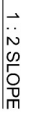
**VEREENIGING PUMP STATION
SYSTEM 1 GEOTECHNICAL INVESTIGATION
GEOTECHNICAL PLAN**

PROJECT NO: 30300496/03
FIGURE NO 3
SCALE 1 : 2000



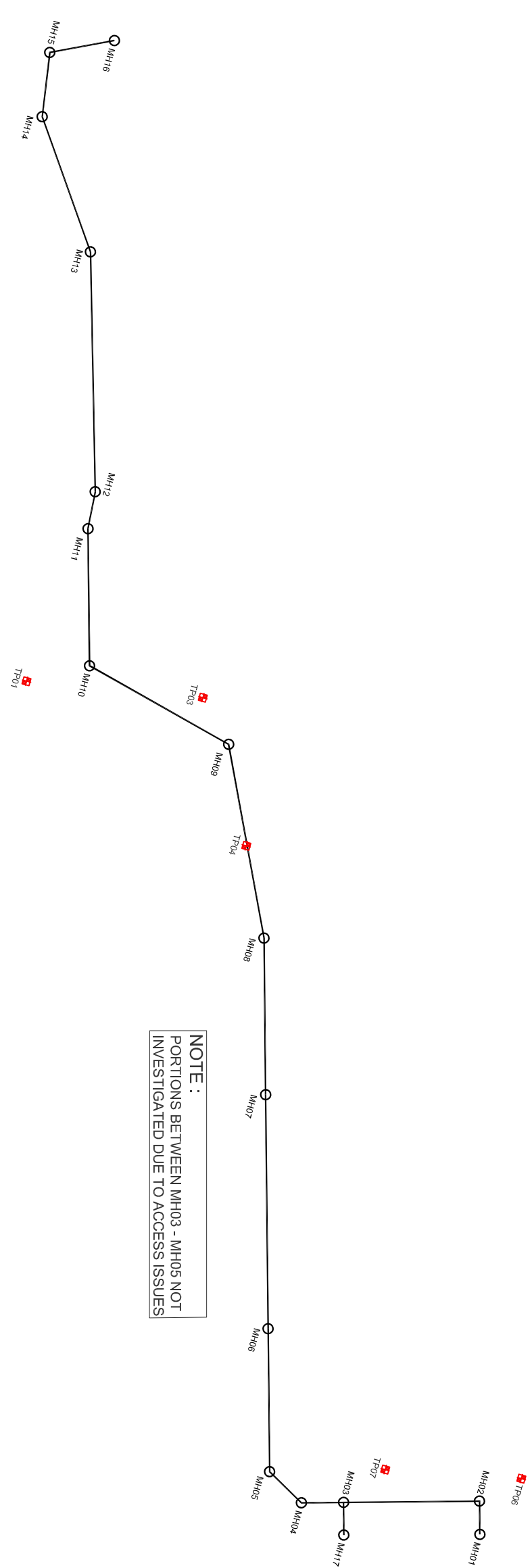
0.5m THICK G6 BACKFILL

SECTION A - A
NTS



VEREENIGING PUMP STATION
SYSTEM 1 GEOTECHNICAL INVESTIGATION

PROPOSED EXCAVATION PLAN (SCHEMATIC)



NOTE :
PORTIONS BETWEEN MH03 - MH05 NOT INVESTIGATED DUE TO ACCESS ISSUES

LEGEND

TEST PIT MATERIAL LEGEND

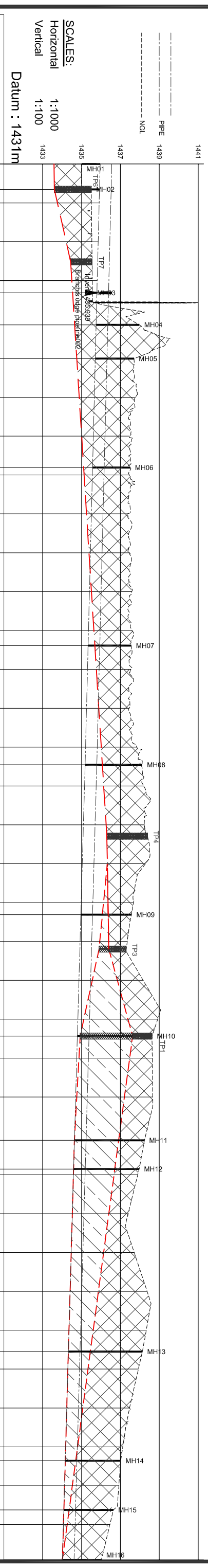
- FILL
- ALLUVIUM

INTERPRETATION BETWEEN BOREHOLES

- GEOLOGICAL BOUNDARY

EXCAVATABILITY:

- FILL : SOFT
- ALLUVIUM : SOFT



CHAINAGE (m)	DEPTH TO INVERTS	INVERT LEVEL	GROUND LEVEL
0.000	0.955	1435.955	1435.000
13.058	0.419	1435.922	1435.503
20.000	0.399	1435.905	1435.506
40.000	0.325	1435.855	1435.530
60.000	0.252	1435.805	1435.553
66.250	0.233	1435.789	1435.556
82.736	-2.225	1435.748	1437.973
100.145	-1.996	1435.705	1437.701
120.000	-2.120	1435.655	1437.775
140.000	-1.859	1435.605	1437.464
156.166	-1.937	1435.565	1437.502
160.000	-1.900	1435.555	1437.455
180.000	-1.870	1435.505	1437.375
200.000	-2.003	1435.455	1437.458
220.000	-2.178	1435.405	1437.583
240.000	-2.245	1435.355	1437.800
247.770	-2.216	1435.336	1437.552
260.000	-2.237	1435.305	1437.542
280.000	-2.194	1435.255	1437.449
300.000	-2.641	1435.205	1437.846
309.091	-2.937	1435.182	1438.119
320.000	-3.046	1435.151	1438.197
340.000	-3.139	1435.094	1438.233
360.000	-3.253	1435.037	1438.290
380.000	-2.691	1434.980	1437.671
386.186	-2.605	1434.962	1437.567
400.000	-2.428	1434.923	1437.351
420.000	-3.305	1434.865	1438.170
440.000	-4.109	1434.808	1438.917
448.692	-3.843	1434.783	1438.626
460.000	-3.889	1434.751	1438.640
480.000	-3.969	1434.694	1438.663
502.311	-3.604	1434.630	1438.234
517.055	-3.377	1434.588	1437.965
520.000	-3.312	1434.580	1437.892
540.000	-2.873	1434.523	1437.396
560.000	-3.244	1434.465	1437.709
580.000	-3.965	1434.408	1438.373
600.000	-3.978	1434.351	1438.329
610.975	-3.813	1434.320	1438.133
620.000	-3.630	1434.294	1437.924
640.000	-3.235	1434.237	1437.472
660.000	-2.942	1434.180	1437.122
667.161	-2.853	1434.159	1437.012
680.000	-2.795	1434.123	1436.918
692.466	-2.549	1434.087	1436.636
700.000	-2.391	1434.065	1436.456
718.176	-2.007	1434.013	1436.020

PIPE GRADES	PIPE DETAILS
33.089m	600mm HDPE (4K(N)2) Class B rigid pipe bedding
53.192m	1:400,001 0.250 %
16.489m	1:350
17.409m	0.286 %
56.021m	
61.321m	
77.099m	
62.509m	
53.619m	
14.744m	
93.929m	
25.309m	
25.711m	

HYDRAULICS	DESIGN: Q (l/s)	V (m/s)	Q (l/s)	V (m/s)	Q (l/s)	V (m/s)	Q (l/s)	V (m/s)	Q (l/s)	V (m/s)	Q (l/s)	V (m/s)	Q (l/s)	V (m/s)	Q (l/s)	V (m/s)	Q (l/s)	V (m/s)
MAK (0.80D): V (m/s)	1.61	1.81	1.61	1.81	1.61	1.81	1.61	1.81	1.61	1.81	1.61	1.81	1.61	1.81	1.61	1.81	1.61	1.81
	1.61	1.81	1.61	1.81	1.61	1.81	1.61	1.81	1.61	1.81	1.61	1.81	1.61	1.81	1.61	1.81	1.61	1.81

MH01 - MH16
Branch: sludge pipeline001

DRAWING PROVIDED BY BOSCH PROJECTS

KP Knight Piesold CONSULTING

VEREENIGING PUMP STATION SYSTEM 1 GEOTECHNICAL INVESTIGATION

SIMPLIFIED SECTION AND PLAN OF SLUDGE PIPELINE SHOWING TEST PITS

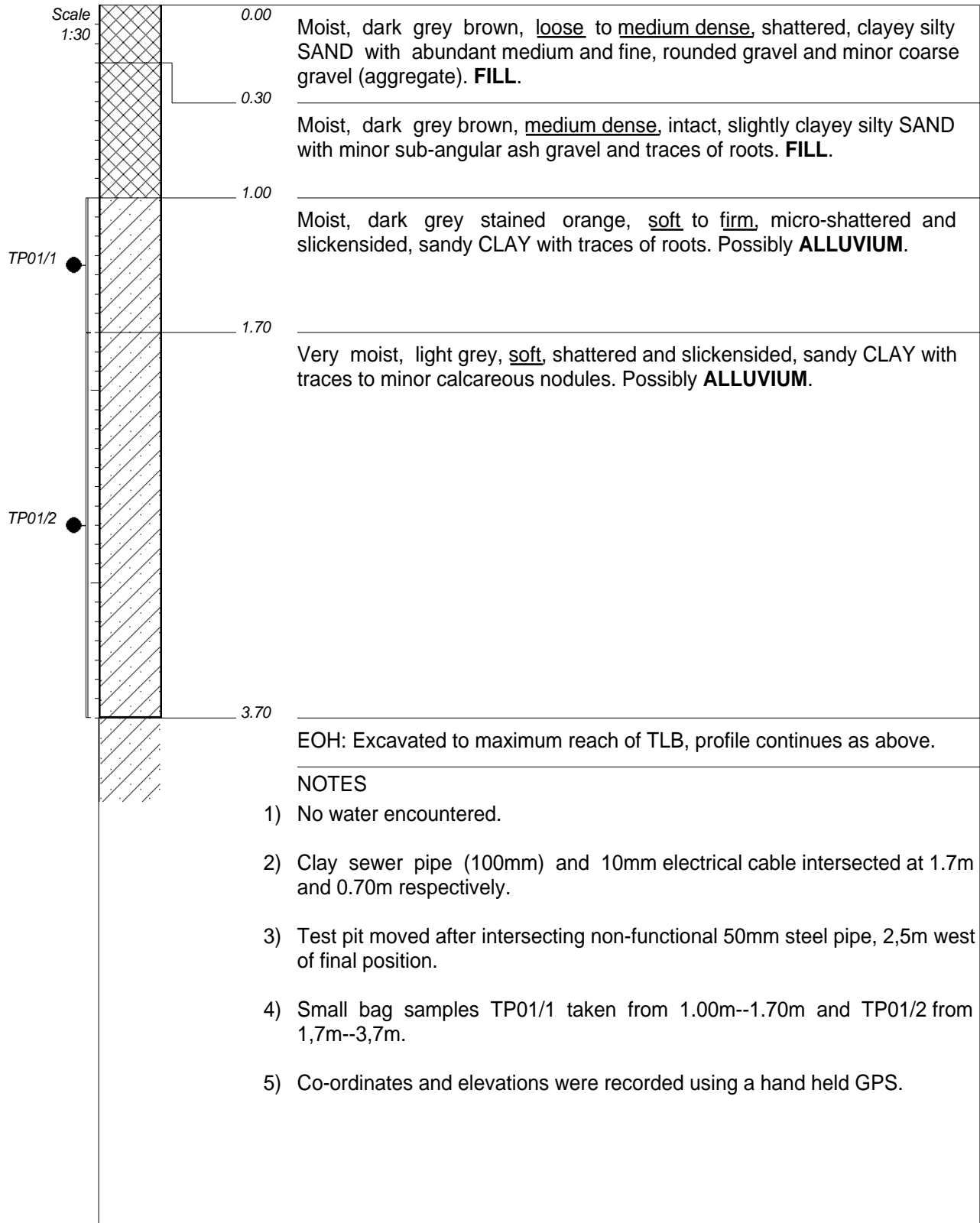
PROJECT NO: 30300496/03
FIGURE NO 5
SCALE 1 : 2000

COPYRIGHT: THIS DRAWING AND ALL THE INFORMATION THEREON IS THE PROPERTY OF KNIGHT PIESOLD AND MAY NOT BE COPIED, REPRODUCED OR TRANSMITTED IN ANY FORM OR BY ANY MEANS, WITHOUT THE WRITTEN CONSENT.

RAND WATER
VEREENIGING PUMPING STATION:
GEOTECHNICAL INVESTIGATION
225ML SEDIMENTATION TANK, FLOCCULATOR AND ASSOCIATED SYSTEM 1 PIPELINES

APPENDIX A

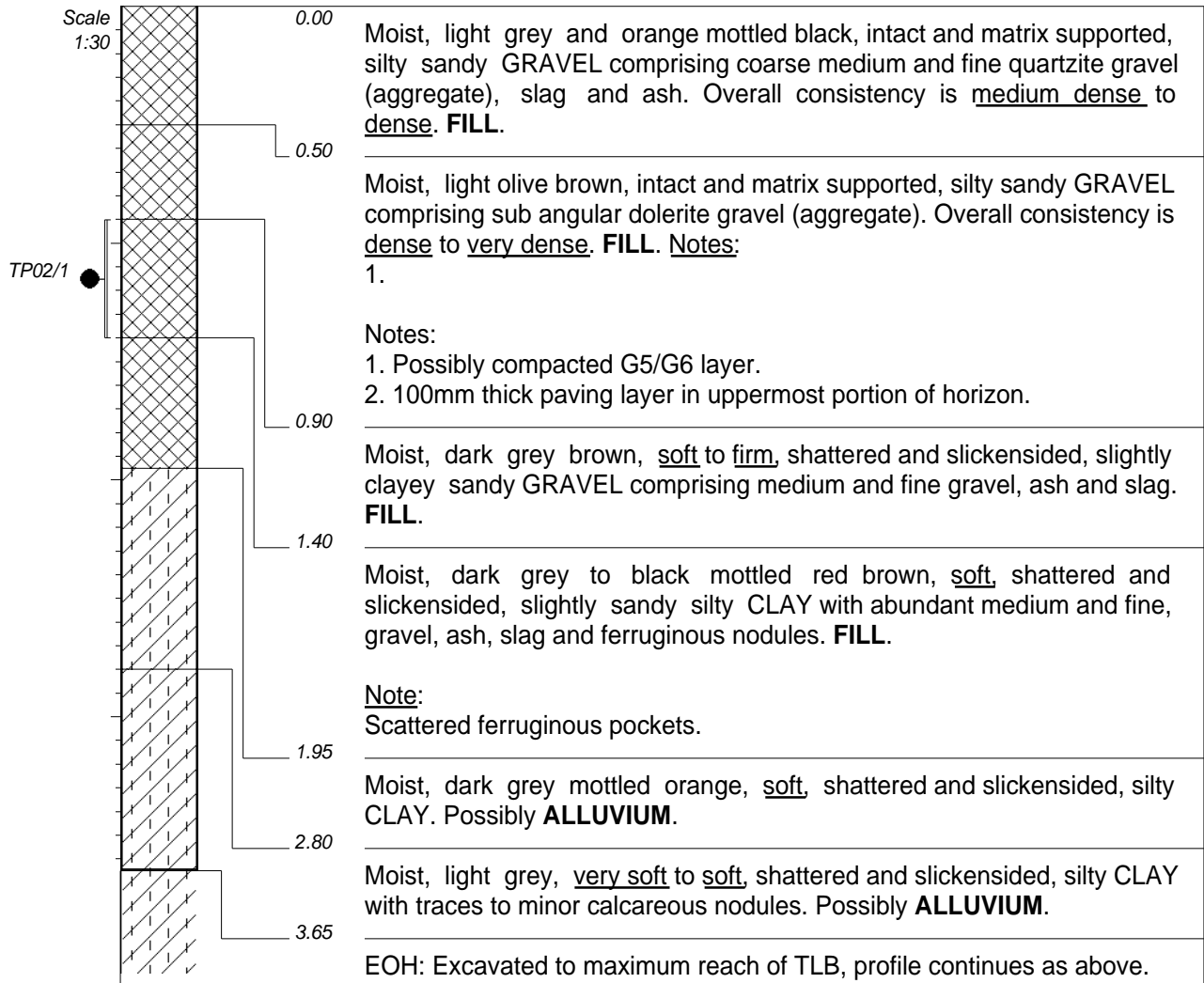
TEST PIT PROFILES



CONTRACTOR : V&S Plant Hire
MACHINE : CAT 422E
DRILLED BY : Patrick
PROFILED BY : DB
TYPE SET BY :
SETUP FILE : KPTP8.SET

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 19/11/2018
DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt

COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953735
Y-COORD : 108048



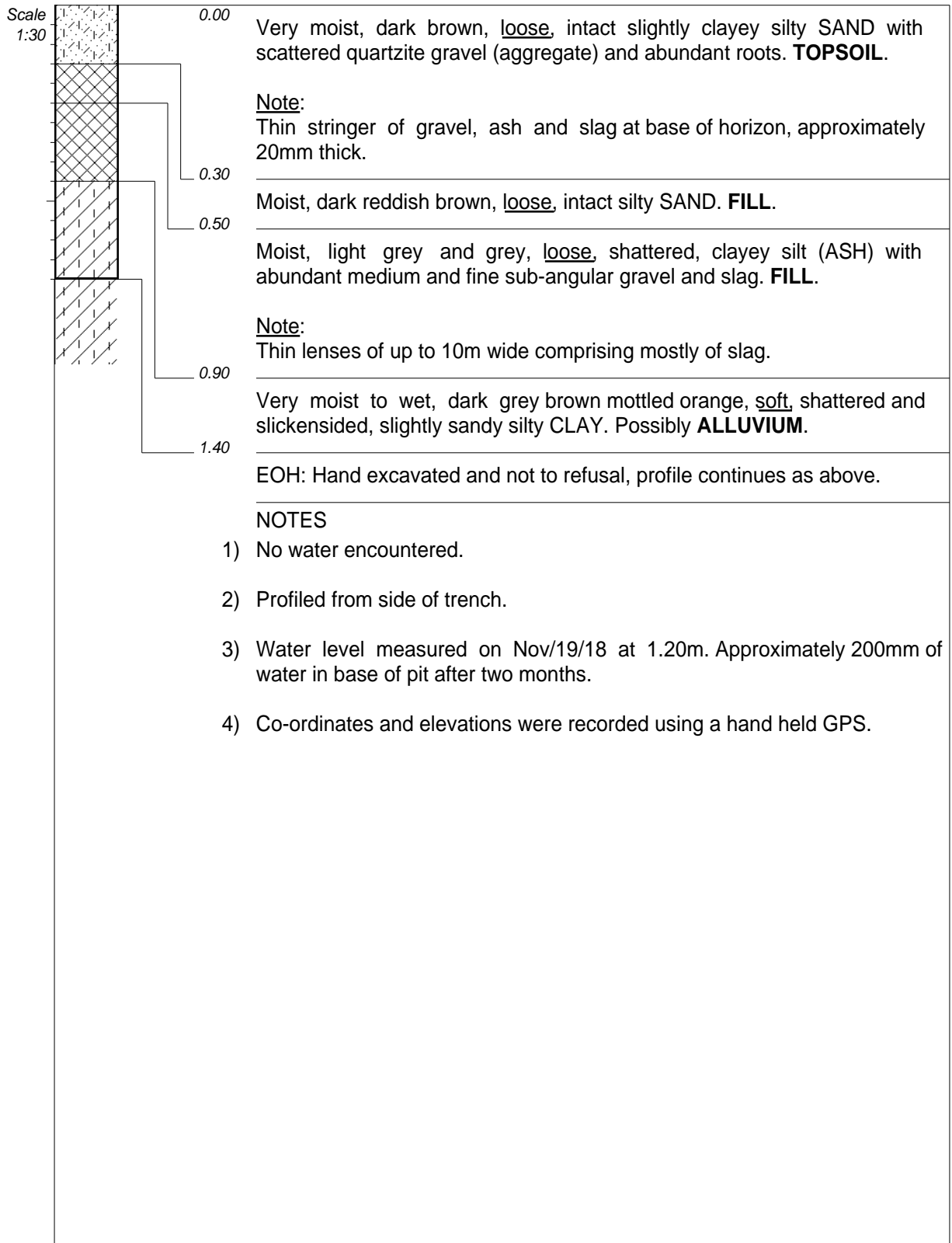
NOTES

- 1) No water encountered.
- 2) Profiled from spoil below 2,8m depth.
- 3) Two bulk (2x large bags) samples TP02/1 taken from 0.90m--1.40m.
- 4) Co-ordinates and elevations were recorded using a hand held GPS.

CONTRACTOR : V&S Plant Hire
MACHINE : CAT 422E
DRILLED BY : Patrick
PROFILED BY : DB
TYPE SET BY :
SETUP FILE : KPTP8.SET

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 20/11/2018
DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt

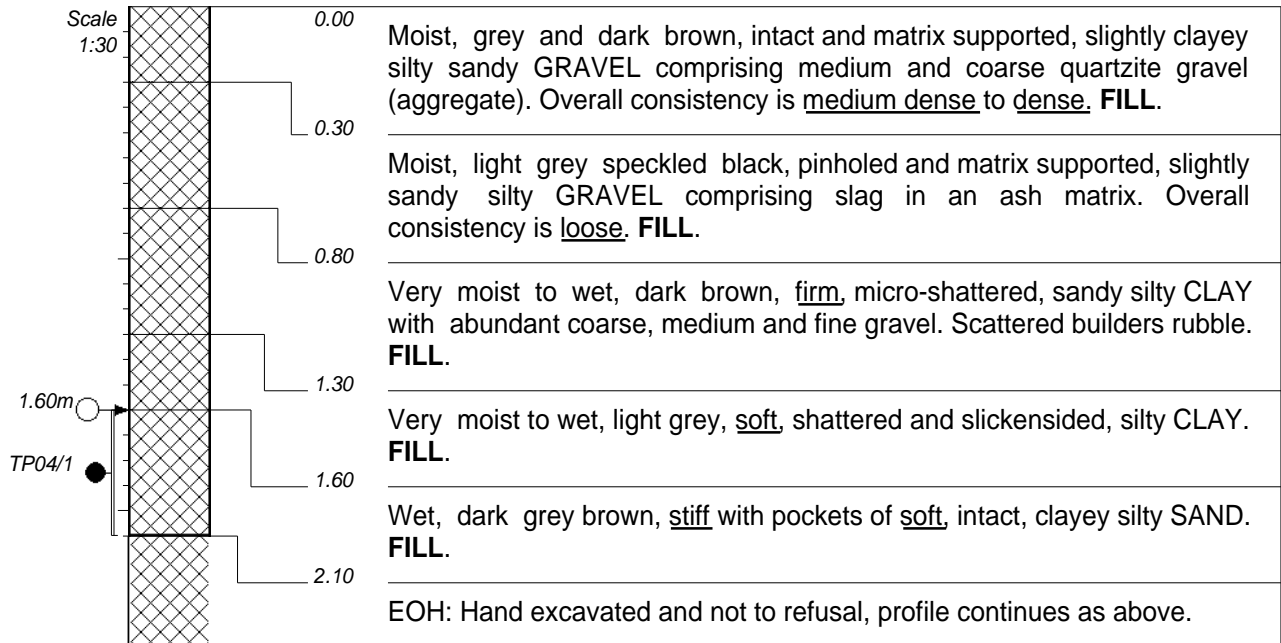
COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953666
Y-COORD : 107987



CONTRACTOR : V&S Plant Hire
MACHINE : Hand Excavated
DRILLED BY : Patrick
PROFILED BY : DB
TYPE SET BY :
SETUP FILE : KTP8.SET

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 20/11/2018
DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt

COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953667
Y-COORD : 108061



NOTES

- 1) Very slow water seepage from 1.60m. Approximately 10mm of water at base of pit after two hours.
- 2) Suspected bulk water mains below position, based on service detection survey to north.
- 3) Small bag sample TP04/1 taken from 1,6m--2,1m.
- 4) Co-ordinates and elevations were recorded using a hand held GPS.

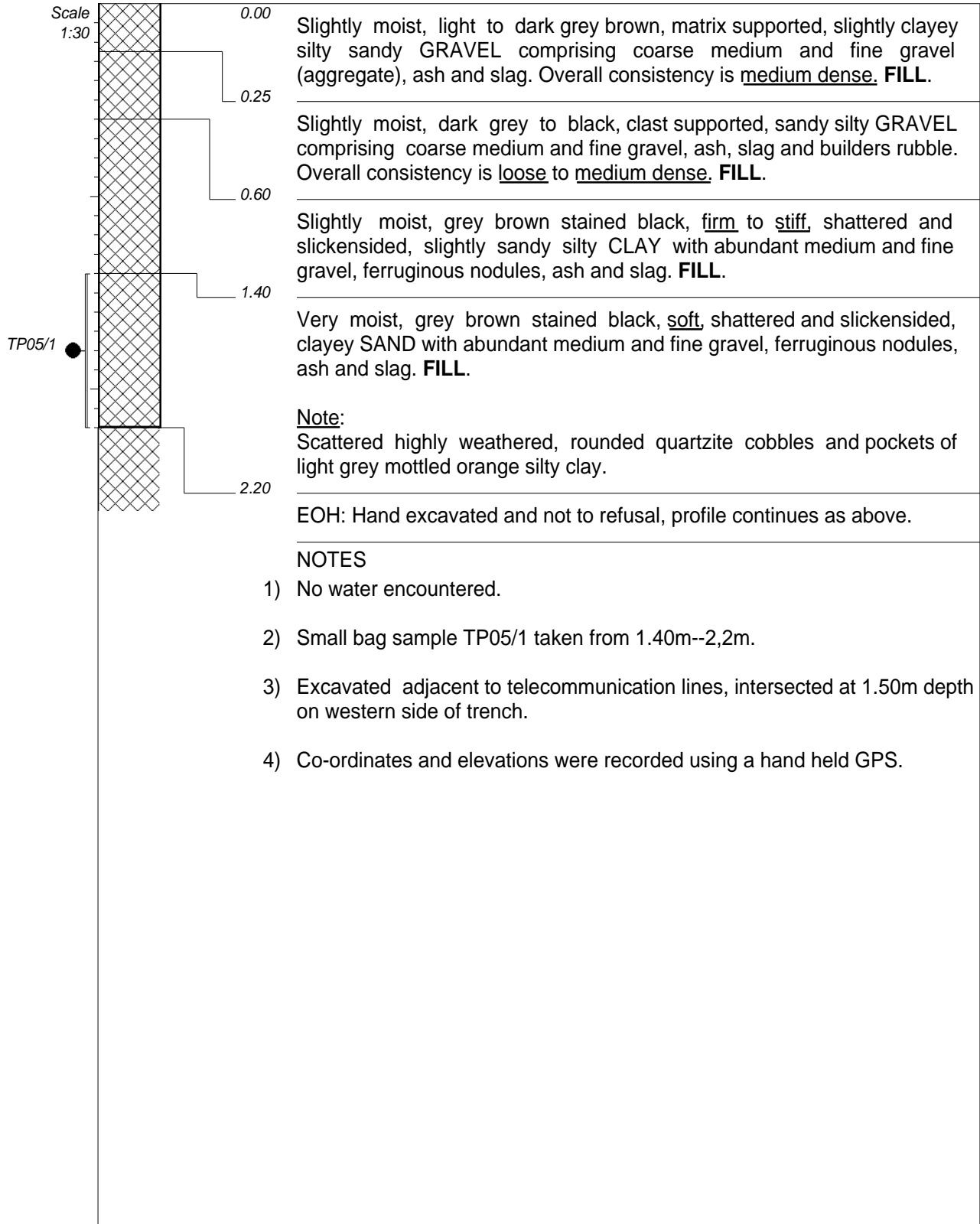
CONTRACTOR : V&S Plant Hire
MACHINE : Hand Excavated
DRILLED BY : Patrick
PROFILED BY : DB

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 20/11/2018

COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953635
Y-COORD : 108010

TYPE SET BY :
SETUP FILE : KPTP8.SET

DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt



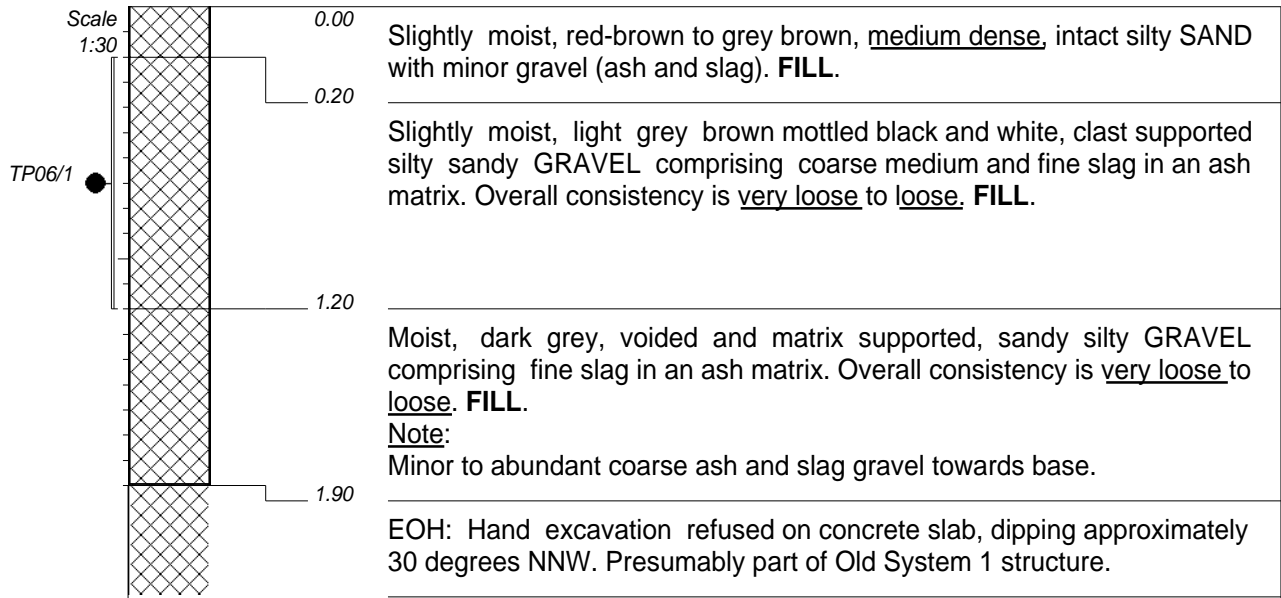
CONTRACTOR : V&S Plant Hire
MACHINE : Hand Excavated
DRILLED BY : Patrick
PROFILED BY : DB

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 21/11/2018

COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953363
Y-COORD : 107832

TYPE SET BY :
SETUP FILE : KPTP8.SET

DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt



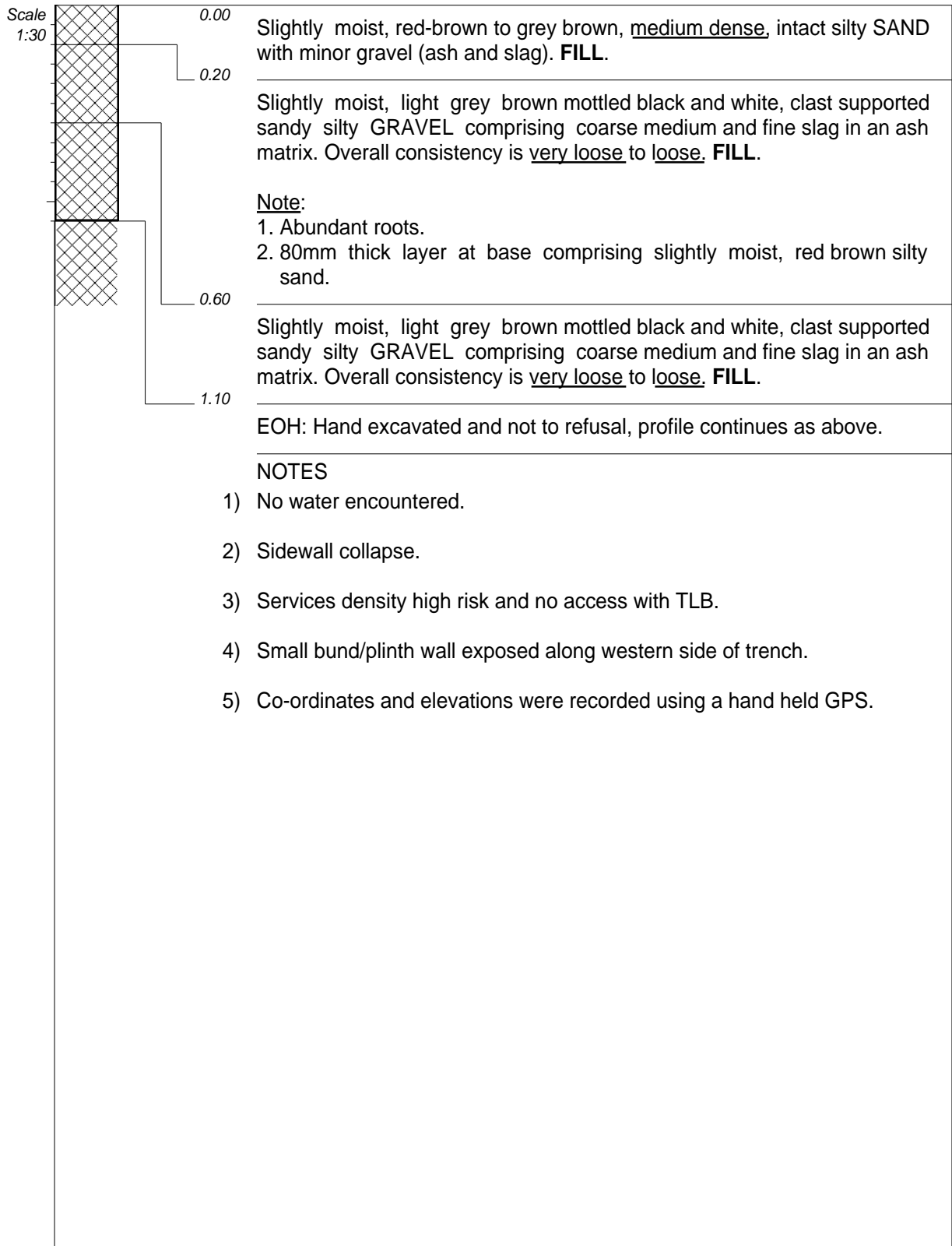
NOTES

- 1) No water encountered.
- 2) Bulk (2x large bags) sample TP06/1 taken from 0.20m--1.20m.
- 3) Co-ordinates and elevations were recorded using a hand held GPS.

CONTRACTOR : V&S Plant Hire
MACHINE : Hand Excavated
DRILLED BY : Patrick
PROFILED BY : DB
TYPE SET BY :
SETUP FILE : KPTP8.SET

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 21/11/2018
DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt

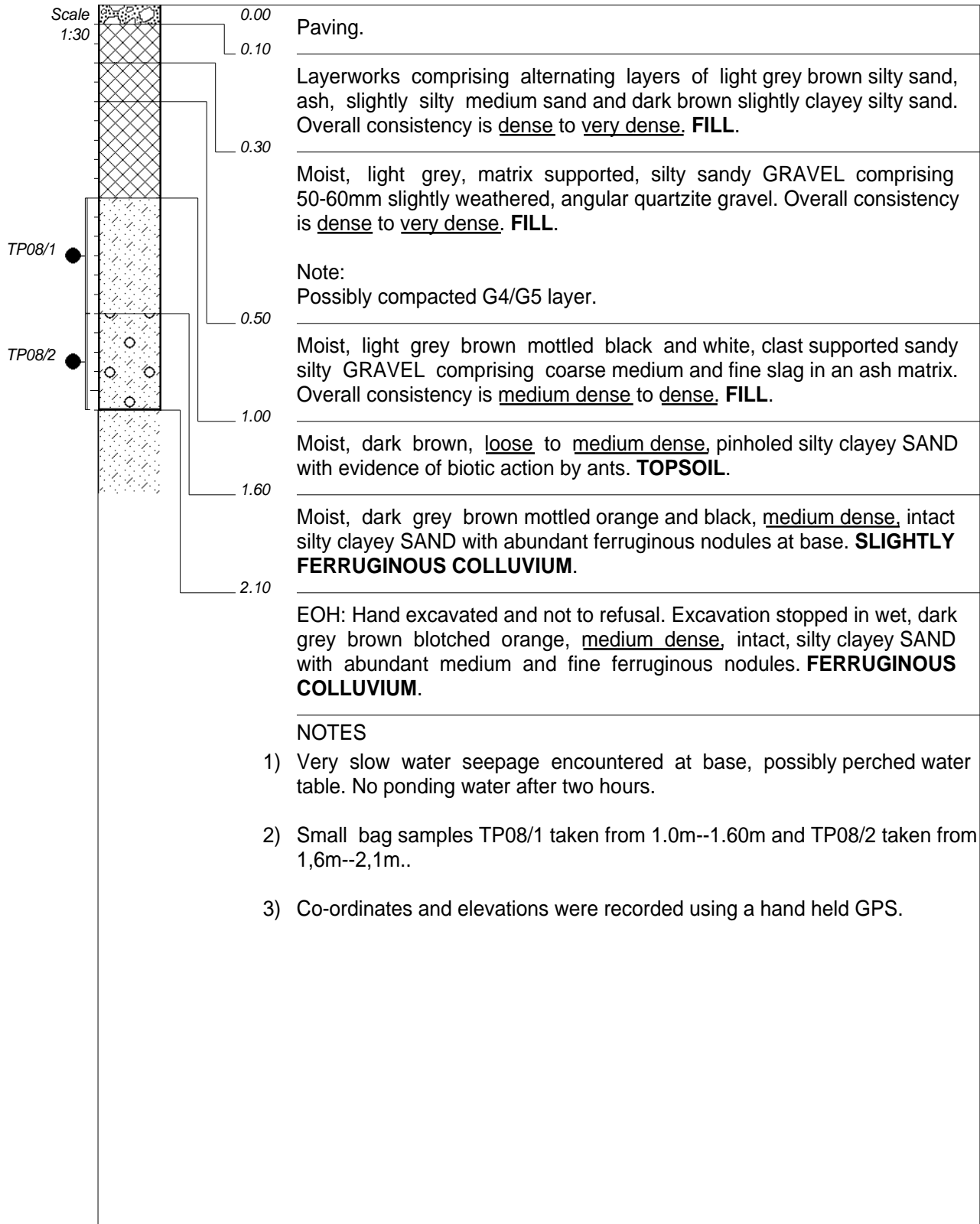
COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953465
Y-COORD : 107800



CONTRACTOR : V&S Plant Hire
MACHINE : Hand Excavated
DRILLED BY : Patrick
PROFILED BY : DB
TYPE SET BY :
SETUP FILE : KTP8.SET

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 21/11/2018
DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt

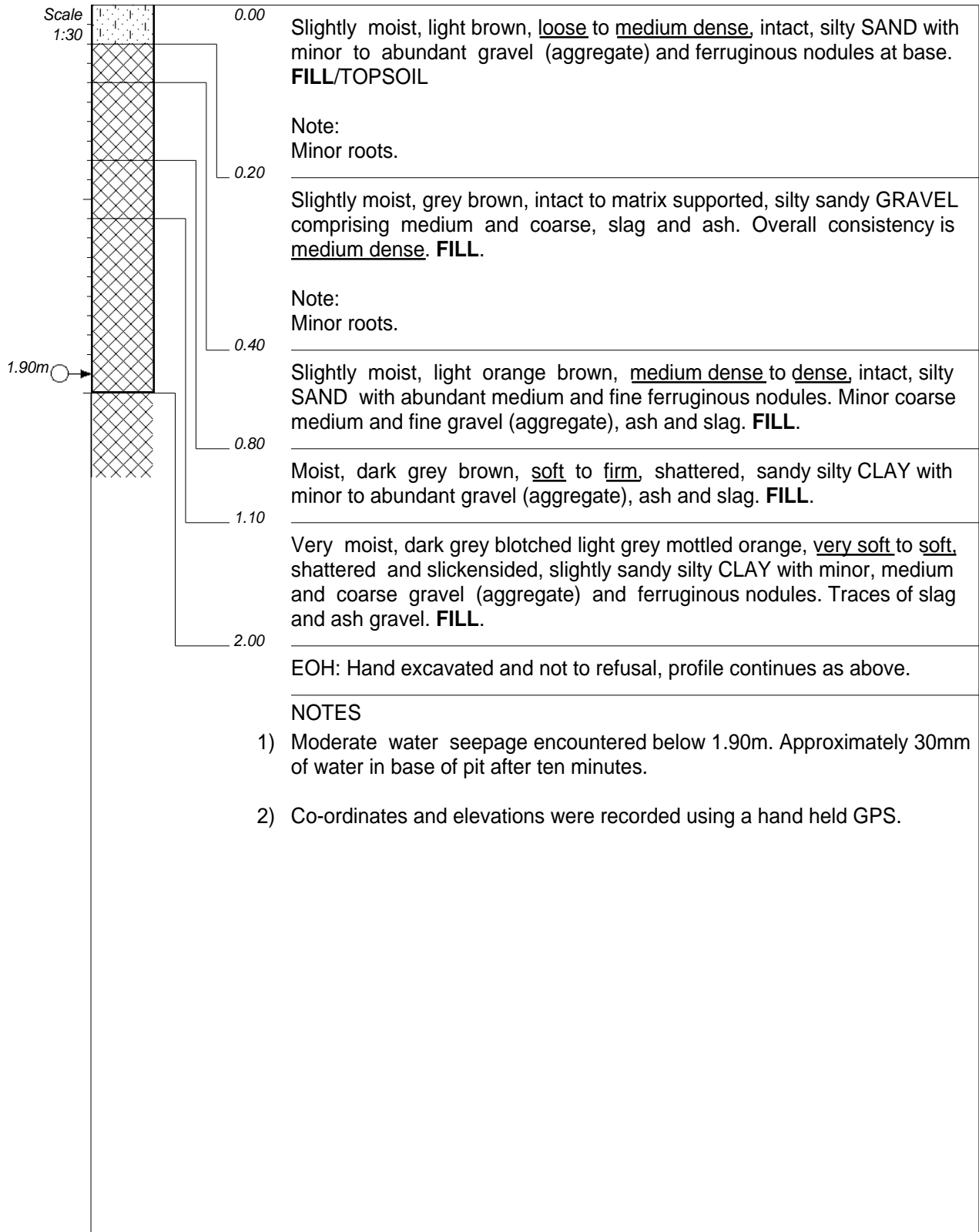
COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953517
Y-COORD : 107789



CONTRACTOR : V&S Plant Hire
MACHINE : Hand Excavated
DRILLED BY : Patrick
PROFILED BY : DB
TYPE SET BY :
SETUP FILE : KTP8.SET

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 21/11/2018
DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt

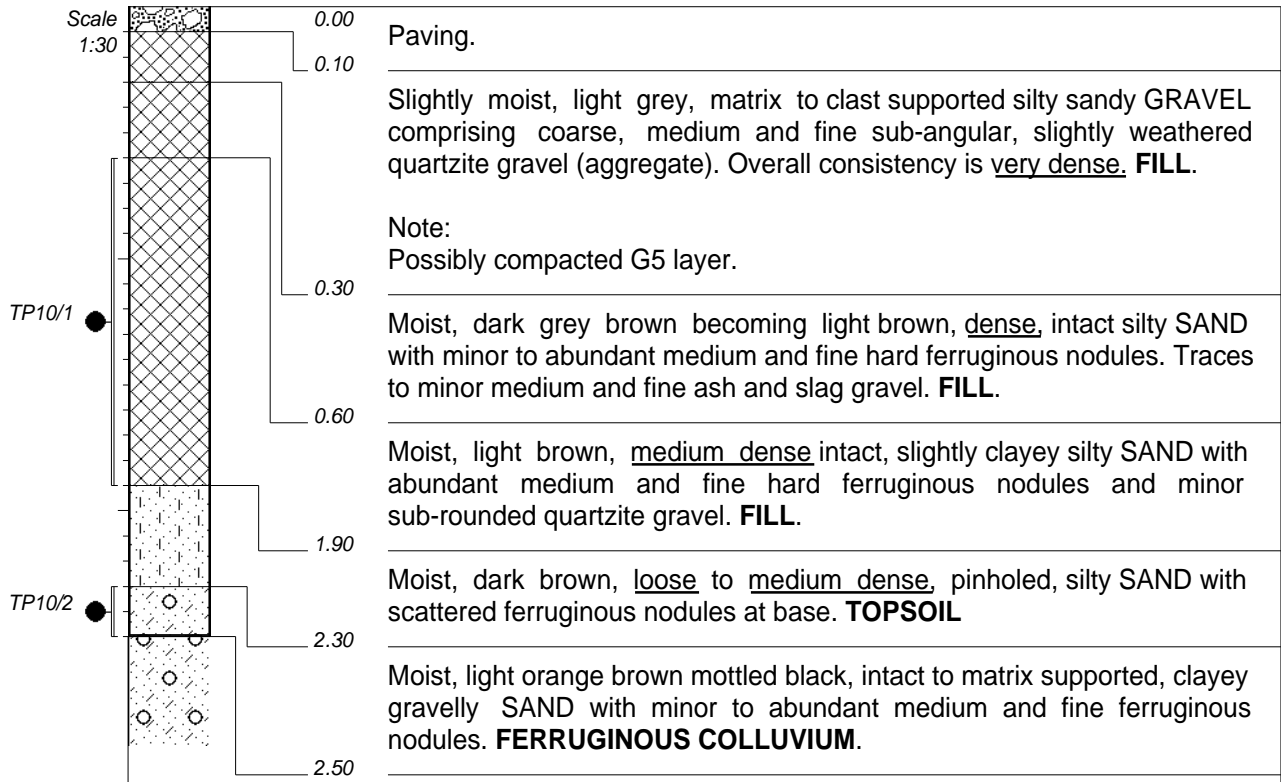
COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953332
Y-COORD : 107499



CONTRACTOR : V&S Plant Hire
MACHINE : Hand Excavated
DRILLED BY : Patrick
PROFILED BY : DB
TYPE SET BY :
SETUP FILE : KPTP8.SET

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 22/11/2018
DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt

COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953378
Y-COORD : 107482



EOH: Hand excavated and not to refusal, profile continues as above.

NOTES

- 1) No water encountered.
- 2) Bulk (2x large bags) sample TP10/1 taken from 0.60m--1.90m.
- 3) Small bag sample TP10/2 taken from 2,3m--2,5m.
- 4) Co-ordinates and elevations were recorded using a hand held GPS.

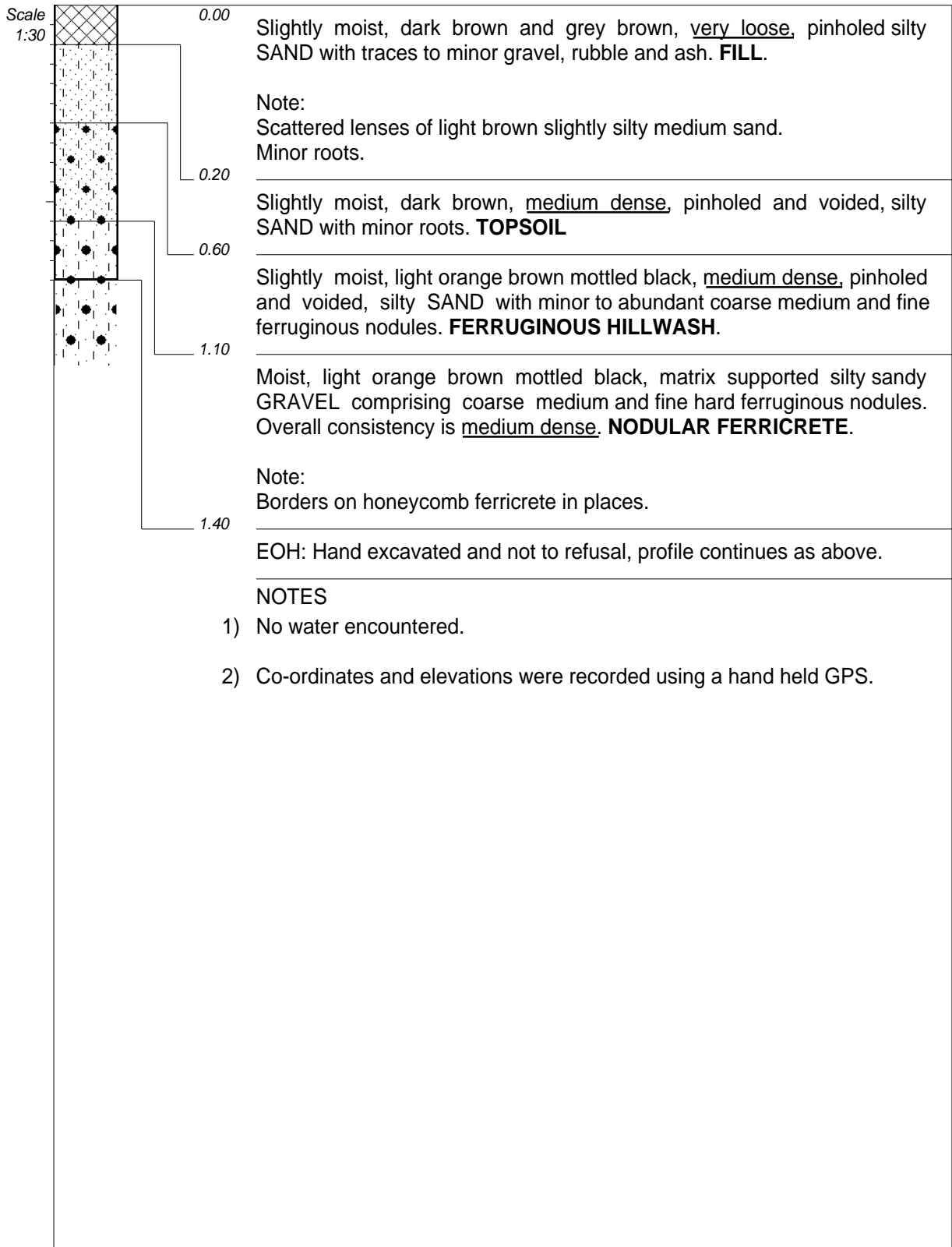
CONTRACTOR : V&S Plant Hire
MACHINE : Hand Excavated
DRILLED BY : Patrick
PROFILED BY : DB

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 22/11/2018

COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953457
Y-COORD : 107465

TYPE SET BY :
SETUP FILE : KPTP8.SET

DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt



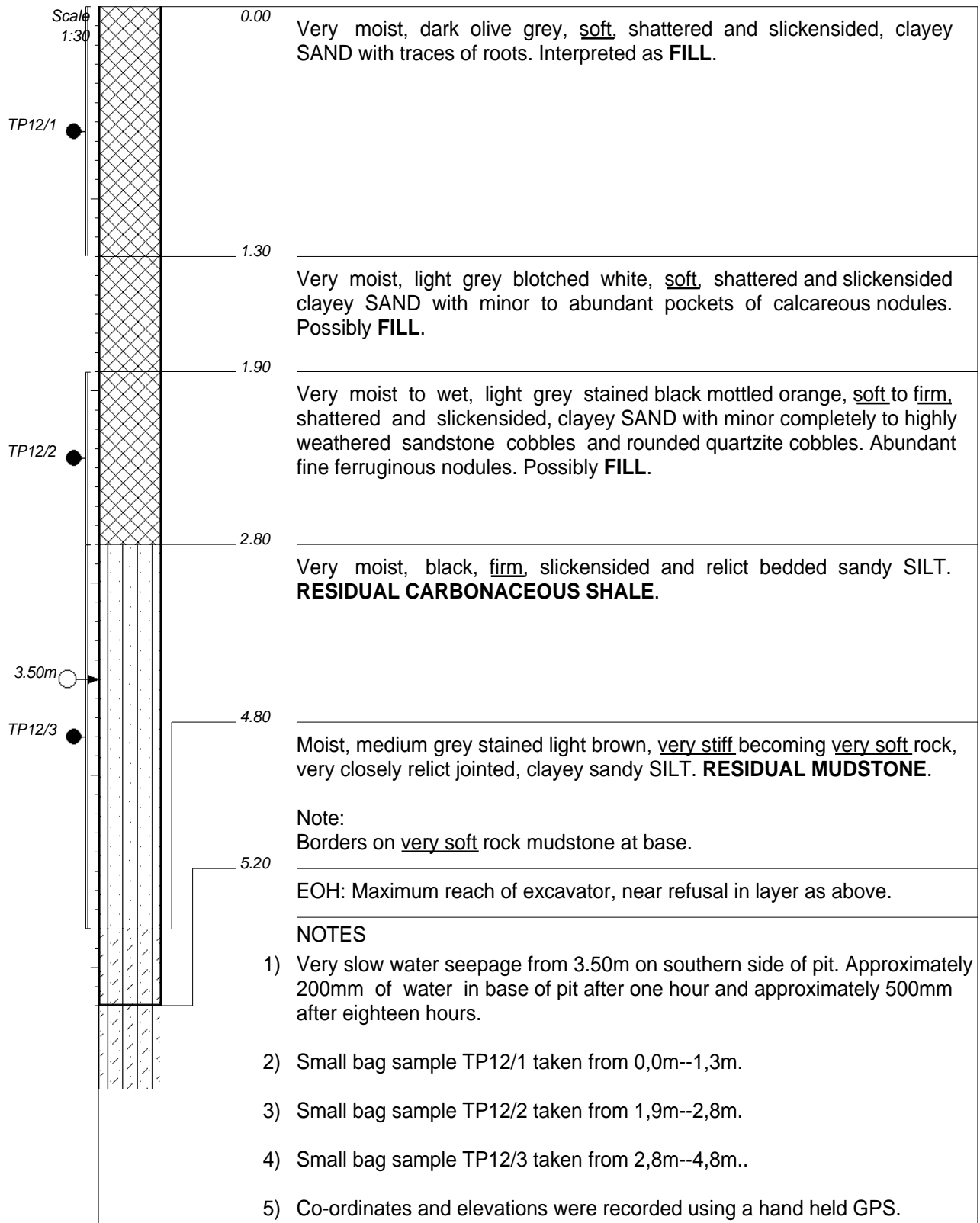
CONTRACTOR : V&S Plant Hire
MACHINE : Hand Excavated
DRILLED BY : Patrick
PROFILED BY : DB

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 22/11/2018

COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953518
Y-COORD : 107733

TYPE SET BY :
SETUP FILE : KTP8.SET

DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt



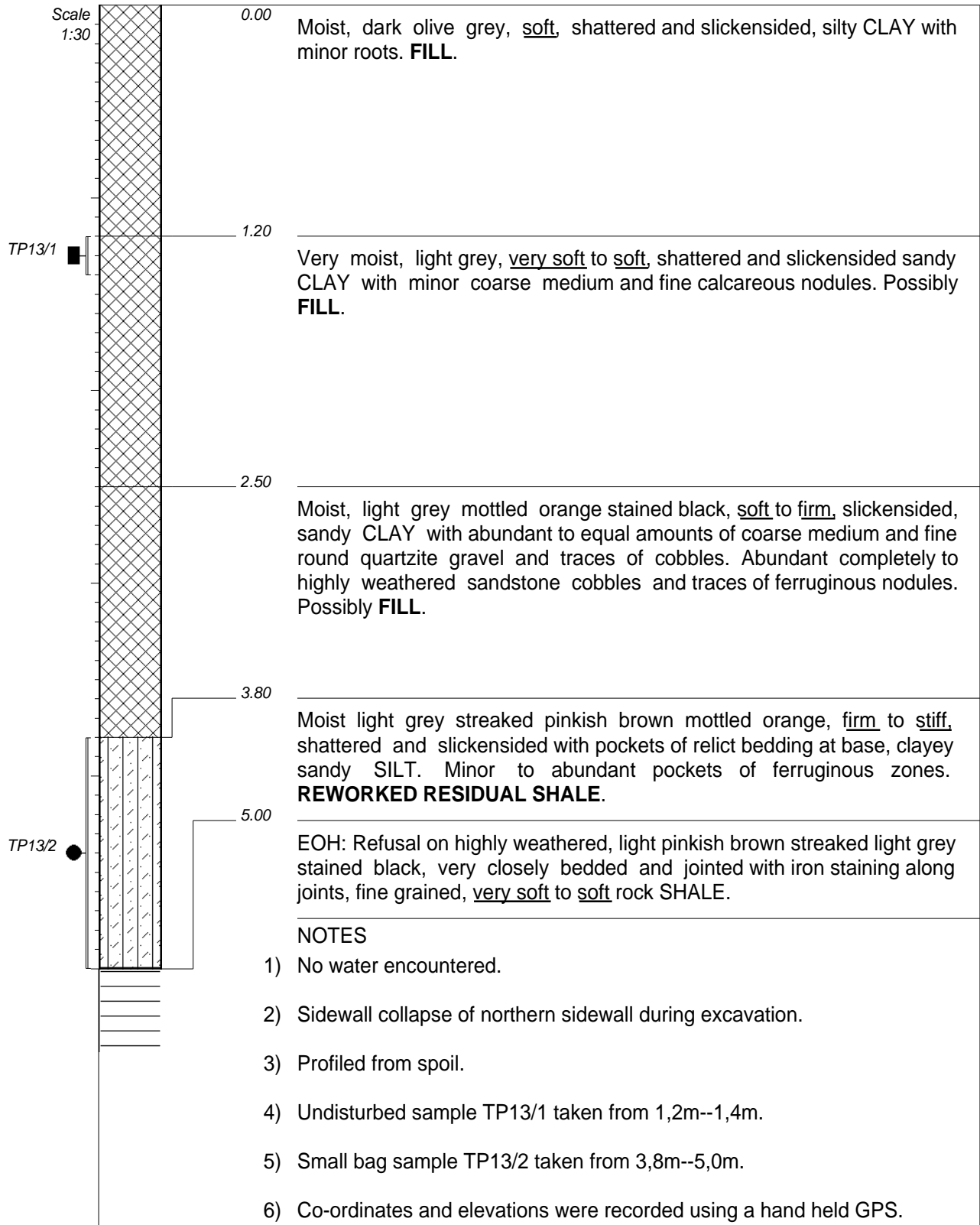
CONTRACTOR : V&S Plant Hire
MACHINE : CAT 320D
DRILLED BY : Patrick
PROFILED BY : DB

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 22/11/2018

COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953474
Y-COORD : 107720

TYPE SET BY :
SETUP FILE : KPTP8.SET

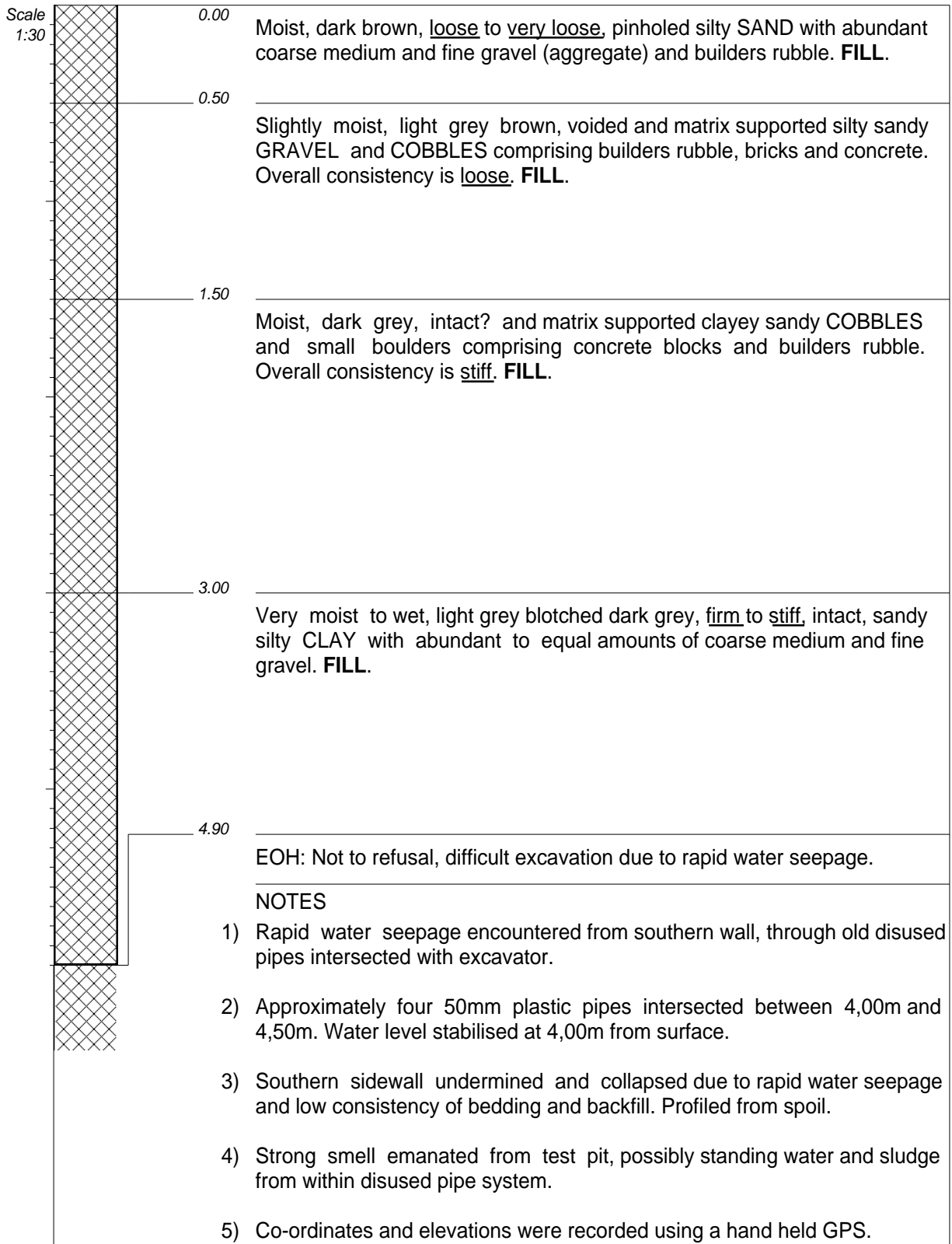
DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt



CONTRACTOR : V&S Plant Hire
MACHINE : CAT 320D
DRILLED BY : Patrick
PROFILED BY : DB
TYPE SET BY :
SETUP FILE : KPTP8.SET

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 22/11/2018
DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt

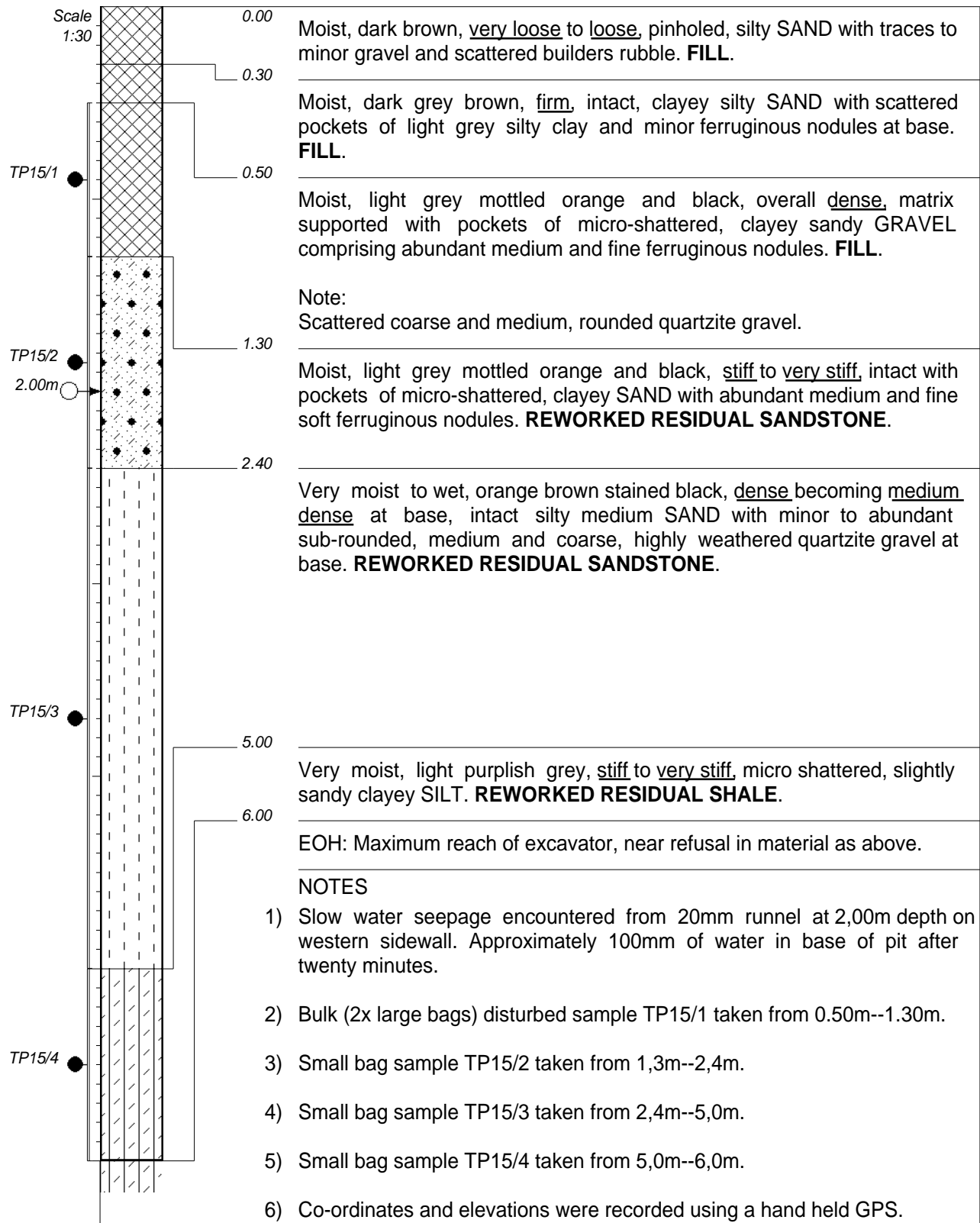
COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953442
Y-COORD : 107637



CONTRACTOR : V&S Plant Hire
MACHINE : CAT 320D
DRILLED BY : Patrick
PROFILED BY : DB
TYPE SET BY :
SETUP FILE : KPTP8.SET

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 23/11/2018
DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt

COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953485
Y-COORD : 107646

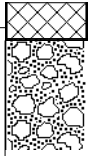


CONTRACTOR : V&S Plant Hire
MACHINE : CAT 320D
DRILLED BY : Patrick
PROFILED BY : DB
TYPE SET BY :
SETUP FILE : KTP8.SET

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 23/11/2018
DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt

COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953441
Y-COORD : 107590

Scale
1:30



0.00

Slightly moist, light brown, loose to medium dense, intact, silty SAND with minor to abundant gravel (aggregate) and ferruginous nodules, and with minor roots. **FILL**

0.15

EOH: Abrupt refusal on concrete slab.

NOTES

- 1) No water encountered.
- 2) Co-ordinates and elevations were recorded using a hand held GPS.

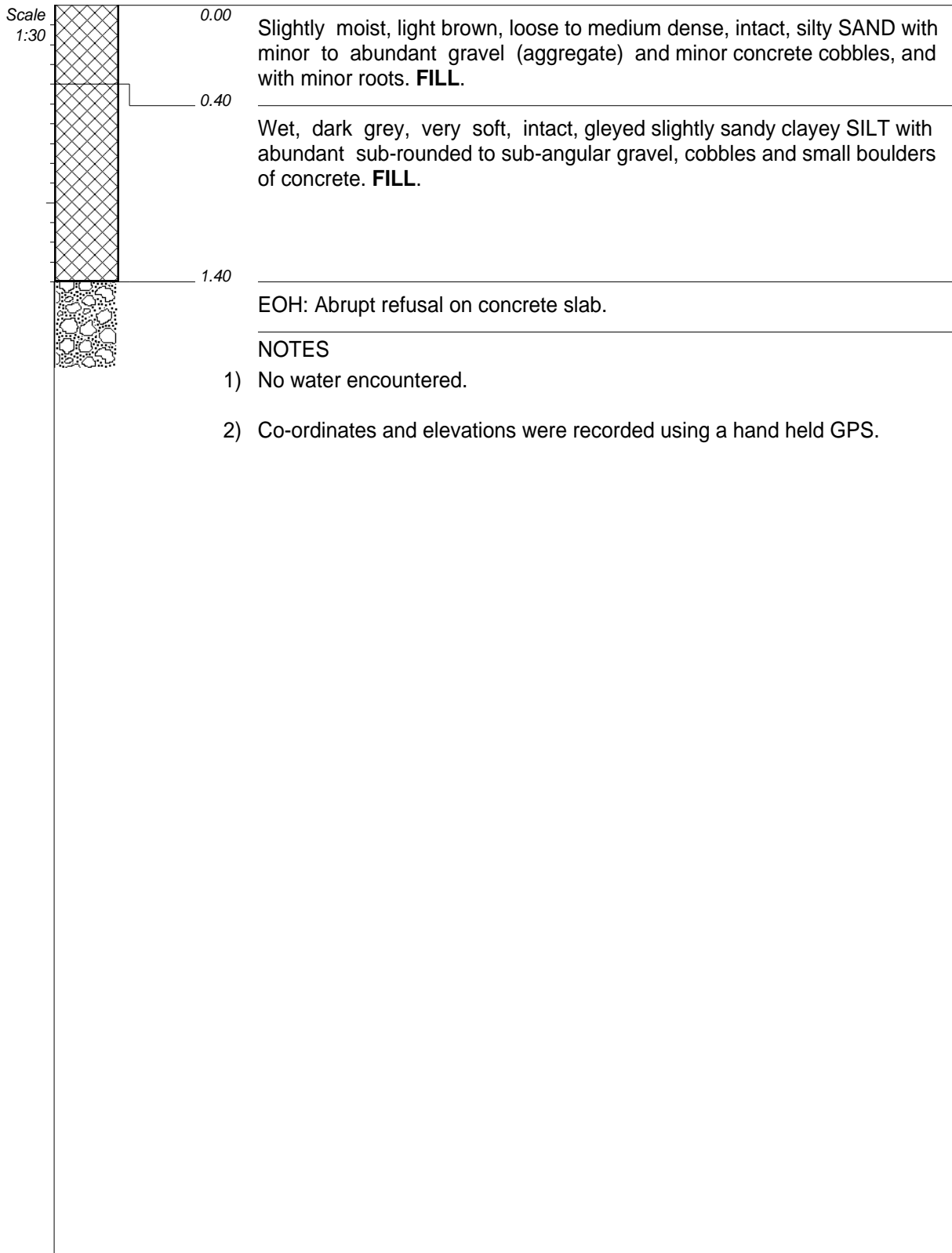
CONTRACTOR : V&S Plant Hire
MACHINE : CAT 320D
DRILLED BY : Patrick
PROFILED BY : DB

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 23/11/2018

COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953446
Y-COORD : 107395

TYPE SET BY :
SETUP FILE : KPTP8.SET

DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt



CONTRACTOR : V&S Plant Hire
MACHINE : CAT 320D
DRILLED BY : Patrick
PROFILED BY : DB

INCLINATION :
DIAM : 650mm
DATE : 02/05/2018
DATE : 23/11/2018

COORDINATE SYSTEM : WGS84 (Lo29)
X-COORD : 2953465
Y-COORD : 107585

TYPE SET BY :
SETUP FILE : KTP8.SET

DATE : 04/03/2019 09:31
TEXT : ..tation3030049603rev1.txt

HOLE No: TP16A

RAND WATER
VEREENIGING PUMPING STATION:
GEOTECHNICAL INVESTIGATION
225ML SEDIMENTATION TANK, FLOCCULATOR AND ASSOCIATED SYSTEM 1 PIPELINES

APPENDIX B

SITE PHOTOGRAPHS

VEREENIGING PUMPING STATION SITE PHOTOGRAPHS



Plate 1. TP1 excavation with a TLB in progress.



Plate 2.
Trench excavation TP3 soil profile.

RAND WATER
VEREENIGING PUMPING STATION:
GEOTECHNICAL INVESTIGATION
225ML SEDIMENTATION TANK, FLOCCULATOR AND ASSOCIATED SYSTEM 1 PIPELINES



Plate 3.
View of TP15 soil profile.



Plate 4.
View of typical trench excavation on site,
which is partially filled with water.

RAND WATER
VEREENIGING PUMPING STATION:
GEOTECHNICAL INVESTIGATION
225ML SEDIMENTATION TANK, FLOCCULATOR AND ASSOCIATED SYSTEM 1 PIPELINES



Plate 5.
View of trench excavation near TP4.



Plate 6.
Large number of services visible in one of the trench excavations.

RAND WATER
VEREENIGING PUMPING STATION:
GEOTECHNICAL INVESTIGATION
225ML SEDIMENTATION TANK, FLOCCULATOR AND ASSOCIATED SYSTEM 1 PIPELINES



Plate 7. North-western corner of old System 1A excavation, which is partially filled with water.

RAND WATER
VEREENIGING PUMPING STATION:
GEOTECHNICAL INVESTIGATION
225ML SEDIMENTATION TANK, FLOCCULATOR AND ASSOCIATED SYSTEM 1 PIPELINES

APPENDIX C

LABORATORY TEST RESULTS

Client : KNIGHT PIESOLD (PTY) LTD
Address : P O BOX 221
 : RIVONIA
 : 2128

Client Reference :
Order No. : KHH 551/18

Attention :
Facsimile : 011 806 7100
E-mail : sdeen@knightpiesold.com

Date Received : 28/11/2018
Date Tested : 28/11/2018 - 06/02/2019
Date Reported : 28/02/2019

Project : Vereeniging Pump Station
Project No. : 2018-B-2286

Report Status : Final
Page : 1 of 20

Herewith please find the test report(s) pertaining to the above project. All tests were conducted in accordance with prescribed test method(s). Information herein consists of the following:

Test(s) conducted / Item(s) measured	Qty.	Test Method(s)	Authorized By**	Page(s)
Moisture Density Relationship	5.000	SANS3001: GR30	S Pullen	13-17
Relative density of soil (SG)	1.000	TMH1 A12T	J Marques	2-12
Moisture Content as received	10.000	SANS 3001: GR20	J Marques	2-12
Atterberg Limits <0.425mm	20.000	SANS3001: GR10	S Pullen/B Mvubu/J Marques	2-12, 18-20
Sieve Analysis 0.075mm	20.000	SANS3001: GR1	S Pullen/J Marques	2-12, 18-20
California Bearing Ratio (CBR)	5.000	SANS3001: GR40	S Pullen/J Marques	18-20
Hydrometer Analysis	20.000	ASTM D422	S Pullen/J Marques	2-12

Any test results contained in this report and marked with * in the table above are "not SANAS accredited" and are not included in the schedule of accreditation for this laboratory.

Any information contained in this test report pertain only to the areas and/or samples tested. Documents may only be reproduced or published in their full context.

While every care is taken to ensure that all tests are carried out in accordance with recognised standards, neither Civilab (Proprietary) Limited nor its employess shall be liable in any way whatsoever for any error made in the execution or reporting of tests or any erroneous conclusions drawn therefrom or for any consequences thereof.

All interpretations, Interpolations, Opinions and/or Classifications contained in this report falls outside our scope of accreditation.

The following parameters, where applicable, were excluded from the classification procedure: Chemical modifications, Additional fines, Fractured Faces, Soluble Salts, pH, Conductivity, Coarse Sand Ratio, Durability (COLTO: G4-G9).

The following parameters, where applicable, were assumed: Rock types were assumed to be of an Arenaceous nature with Siliceous cementing material.

Unless otherwise requested or stated, all samples will be discarded after a period of 3 months.

Deviations in Test Methods:

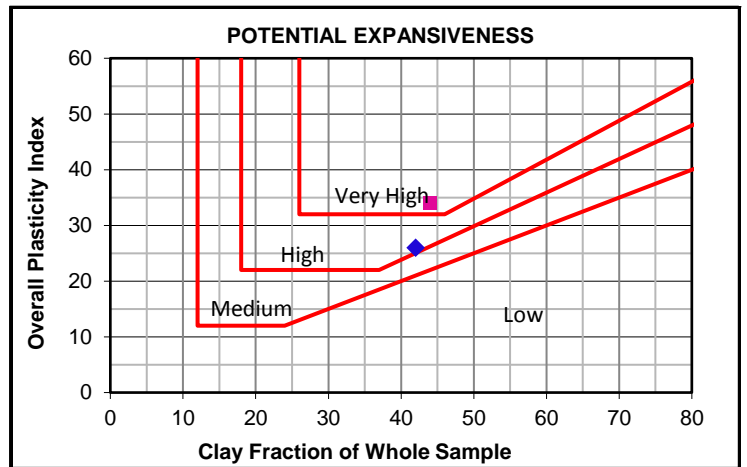
**All results are authorized electronically by approved managers and/or technical signatories.

Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No : 2018-B-2286

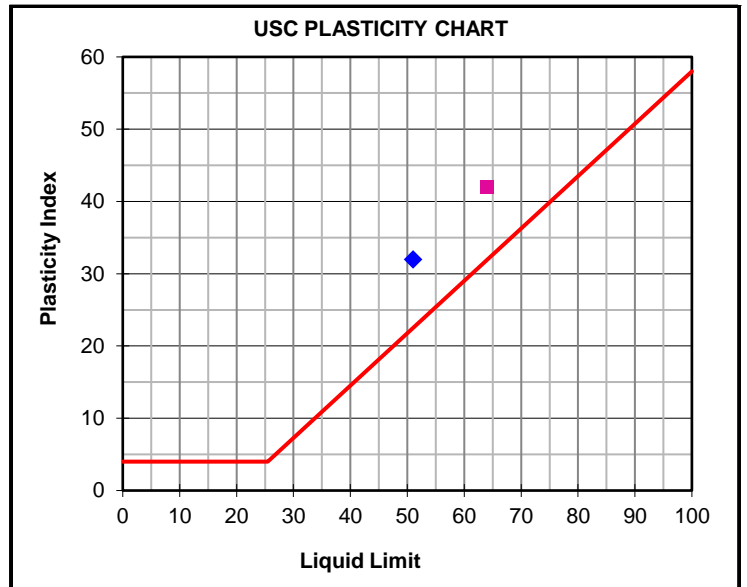
Date Received: 28/11/2018
 Date Reported: 14/02/2019
 Page No. : 2 of 20

FOUNDATION INDICATOR

Laboratory Number	1 ◆	2 ■
Field Number	TP01	TP01
Client Reference		
Depth (m)	1.00-1.70	1.70-3.70
Position		
Coordinates	X Y	
Description		
Additional Information	Alluvium	Alluvium
Calcrete / Crushed Stabilizing Agent		



Moisture Content & Relative Density		
Moisture Content (%)	14.7	34.6
Relative Density (S.G.)		



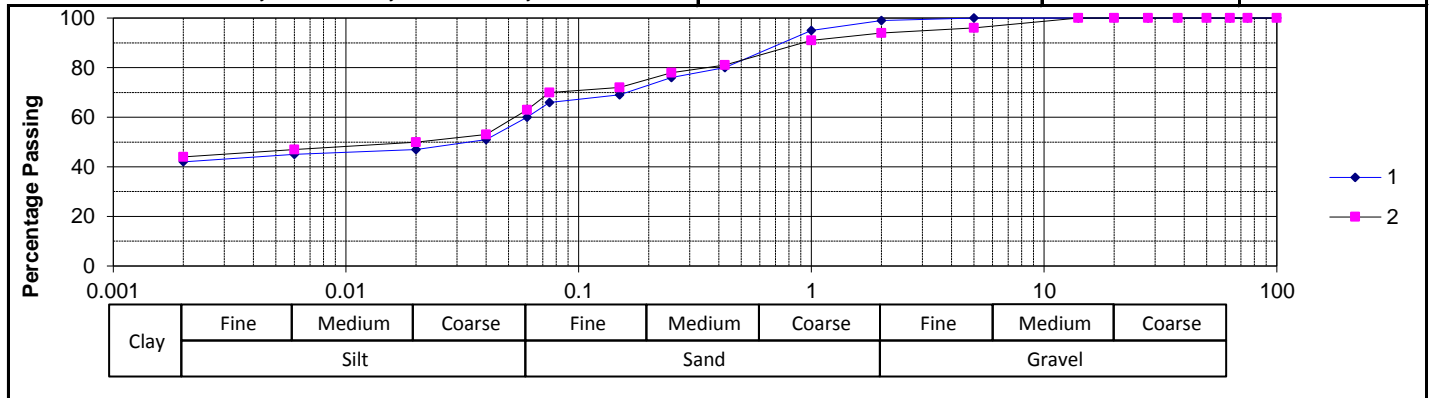
Sieve Analysis (Wet Prep) SANS3001: GR1			
Percentage Passing	100 mm	100	100
	75 mm	100	100
	63 mm	100	100
	50 mm	100	100
	37.5 mm	100	100
	28 mm	100	100
	20 mm	100	100
	14 mm	100	100
	5 mm	100	96
	2 mm	99	94
	1 mm	95	91
	0.425 mm	80	81
	0.250 mm	76	78
	0.150 mm	69	72
0.075 mm	66	70	
Grading Modulus	0.55	0.55	

Hydrometer Analysis ASTM D422			
Percentage Passing	0.060 mm	60	63
	0.040 mm	51	53
	0.020 mm	47	50
	0.006 mm	45	47
	0.002 mm	42	44
Gravel	%	1	6
Sand	%	39	31
Silt	%	18	19
Clay	%	42	44

Laboratory Number	1 ◆	2 ■	
Atterberg Limits -425µ SANS3001: GR10			
Liquid Limit	%	51	64
Plasticity Index	%	32	42
Linear Shrinkage	%	15.5	17.0
Overall PI	%	26	34

Classifications		
HRB (AASHTO)	A-7-6(19)	A-7-6(20)
Unified (ASTM D2487)	CH	CH
Weston Swell @ 1 kPa	4.1	1.5

Note: An assumed S.G. may be used in Hydrometer Analysis calculations

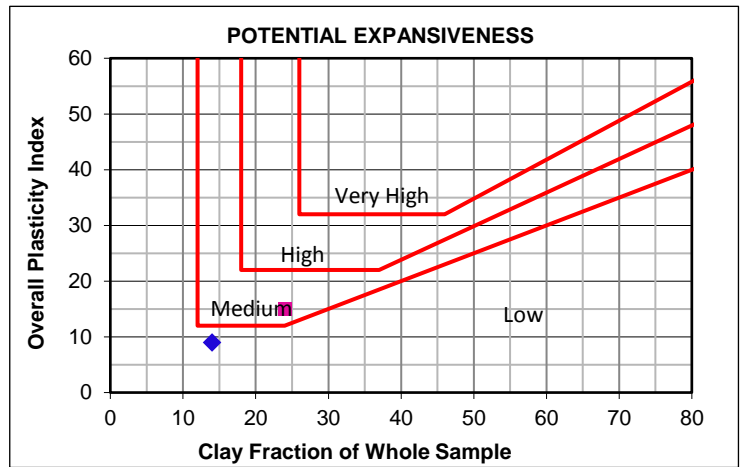


Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No : 2018-B-2286

Date Received: 28/11/2018
 Date Reported: 14/02/2019
 Page No. : 3 of 20

FOUNDATION INDICATOR

Laboratory Number	3 ◆	4 ■
Field Number	TP02	TP04
Client Reference		
Depth (m)	0.90-1.40	1.60-2.10
Position		
Coordinates	X Y	
Description		
Additional Information	Fill	Alluvium
Calcrete / Crushed Stabilizing Agent		

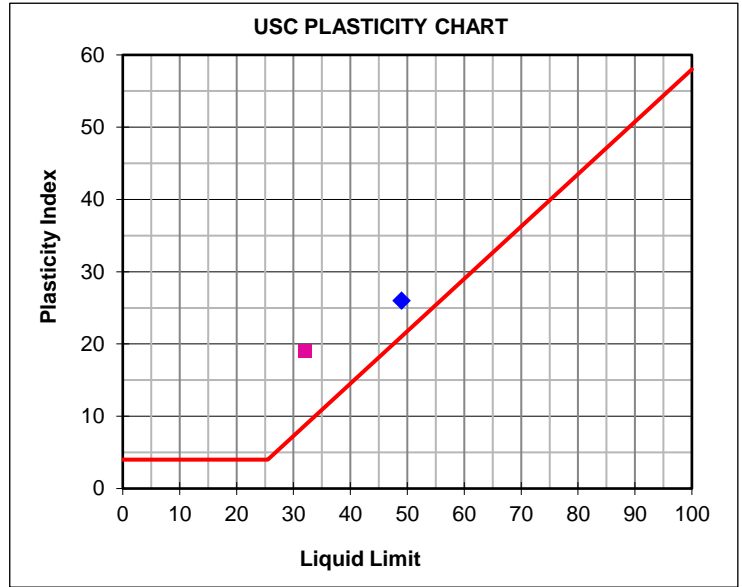


Moisture Content & Relative Density SANS3001: GR30

Moisture Content (%)		17.3
Relative Density (S.G.)		

Sieve Analysis (Wet Prep) SANS3001: GR1

Percentage Passing	100 mm	100	100
	75 mm	100	100
	63 mm	100	100
	50 mm	100	100
	37.5 mm	93	100
	28 mm	83	100
	20 mm	72	100
	14 mm	65	100
	5 mm	55	99
	2 mm	49	98
	1 mm	44	95
	0.425 mm	35	81
	0.250 mm	33	74
	0.150 mm	30	66
0.075 mm	29	62	
Grading Modulus	1.87	0.59	



Hydrometer Analysis ASTM D422

Percentage Passing	0.060 mm	25	50
	0.040 mm	19	34
	0.020 mm	17	30
	0.006 mm	16	27
	0.002 mm	14	24
Gravel	%	51	2
Sand	%	24	48
Silt	%	11	26
Clay	%	14	24

Laboratory Number 3 ◆ 4 ■

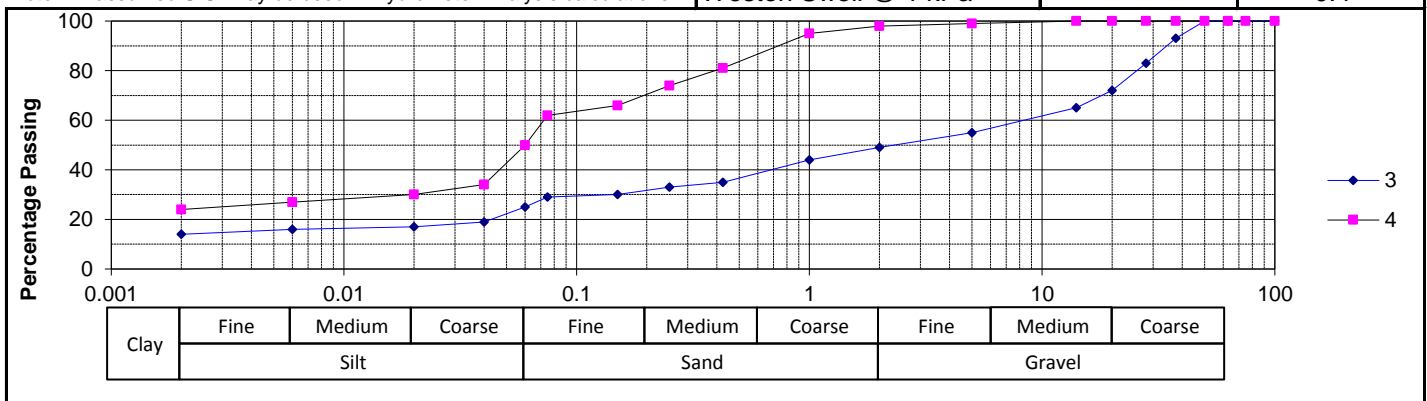
Atterberg Limits -425µ SANS3001: GR10

Liquid Limit	%	49	32
Plasticity Index	%	26	19
Linear Shrinkage	%	13.5	9.0
Overall PI	%	9	15

Classifications

HRB (AASHTO)	A-2-7(2)	A-6(9)
Unified (ASTM D2487)	GC	CL
Weston Swell @ 1 kPa		0.4

Note: An assumed S.G. may be used in Hydrometer Analysis calculations

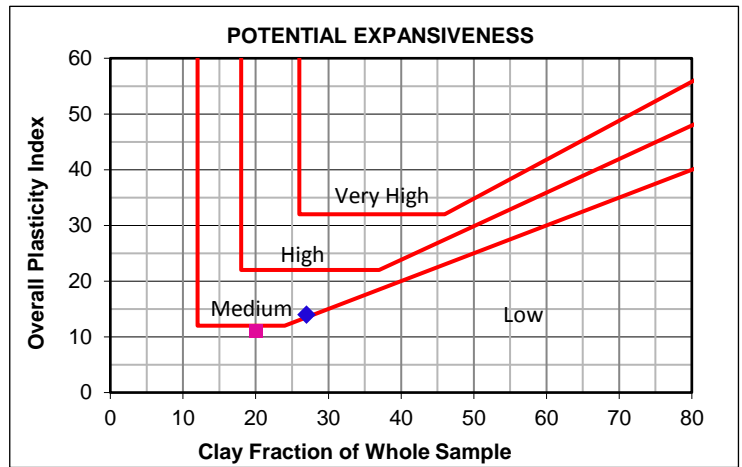


Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No : 2018-B-2286

Date Received: 28/11/2018
 Date Reported: 14/02/2019
 Page No. : 5 of 20

FOUNDATION INDICATOR

Laboratory Number	7 ◆	8 ■
Field Number	TP08	TP08
Client Reference		
Depth (m)	1.5	1.60-2.10
Position		
Coordinates	X Y	
Description		
Additional Information	Topsoil	Slightly Ferruginous
Calcrete / Crushed Stabilizing Agent		

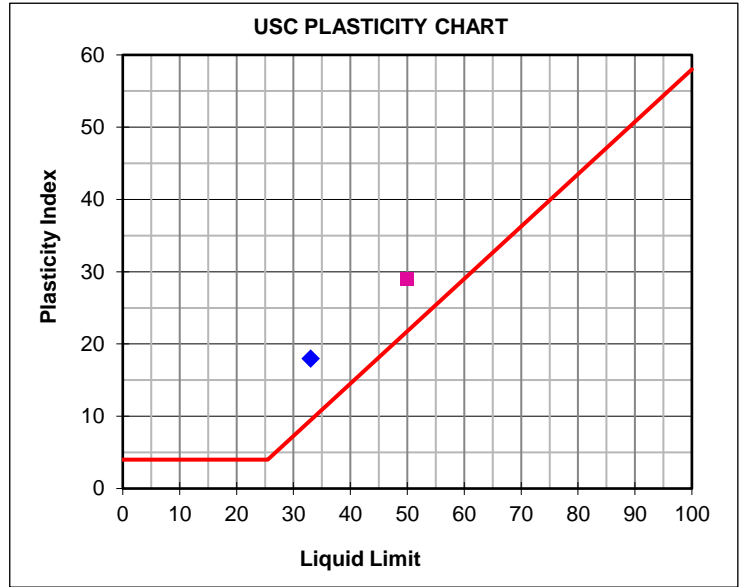


Moisture Content & Relative Density

Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Prep) SANS3001: GR1

Percentage Passing	100 mm	100	100
	75 mm	100	100
	63 mm	100	100
	50 mm	100	100
	37.5 mm	100	100
	28 mm	100	100
	20 mm	100	100
	14 mm	100	100
	5 mm	100	78
	2 mm	98	61
	1 mm	93	52
	0.425 mm	80	38
	0.250 mm	71	36
	0.150 mm	61	33
0.075 mm	58	33	
Grading Modulus	0.64	1.68	



Hydrometer Analysis ASTM D422

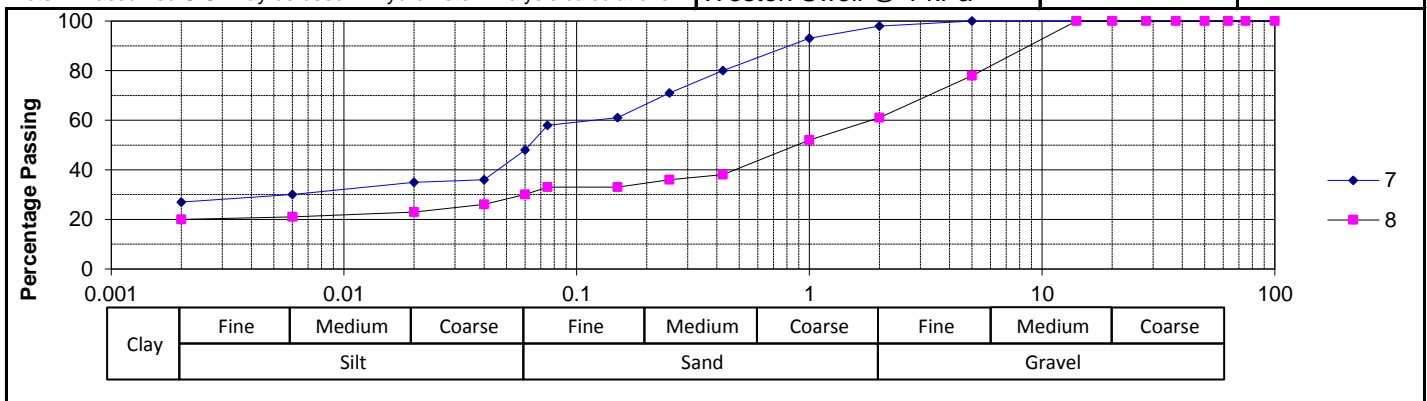
Percentage Passing	0.060 mm	48	30
	0.040 mm	36	26
	0.020 mm	35	23
	0.006 mm	30	21
	0.002 mm	27	20
Gravel	%	2	39
Sand	%	50	31
Silt	%	21	10
Clay	%	27	20

Laboratory Number	7 ◆	8 ■
Atterberg Limits -425µ	SANS3001: GR10	
Liquid Limit	% 33	50
Plasticity Index	% 18	29
Linear Shrinkage	% 9.5	13.0
Overall PI	% 14	11

Classifications

HRB (AASHTO)	A-6(7)	A-2-7(3)
Unified (ASTM D2487)	CL	SC
Weston Swell @ 1 kPa		

Note: An assumed S.G. may be used in Hydrometer Analysis calculations

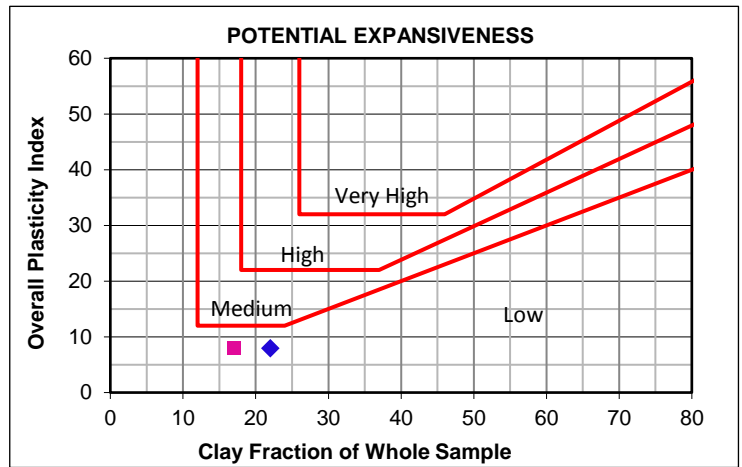


Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No : 2018-B-2286

Date Received: 28/11/2018
 Date Reported: 14/02/2019
 Page No. : 6 of 20

FOUNDATION INDICATOR

Laboratory Number	10 ◆	11 ■
Field Number	TP10	TP10
Client Reference		
Depth (m)	2.30-2.50	0.60-1.90
Position		
Coordinates	X Y	
Description		
Additional Information	Ferruginous Colluvium	Fill
Calcrete / Crushed Stabilizing Agent		

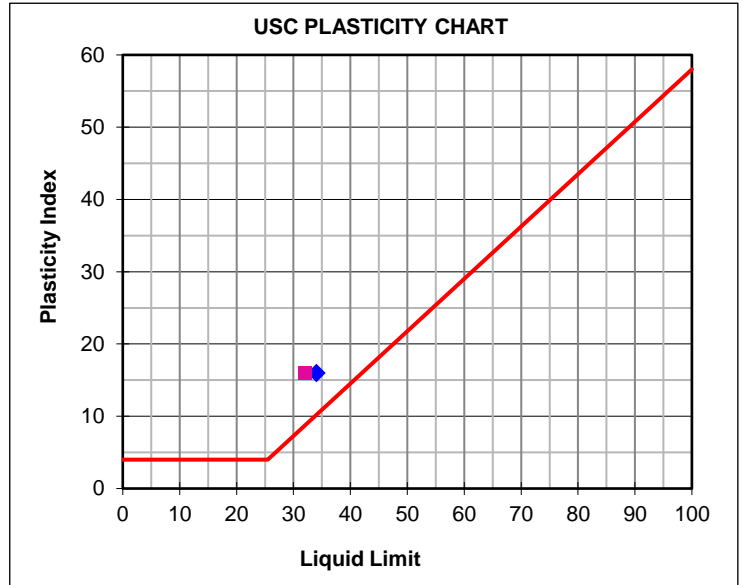


Moisture Content & Relative Density

Moisture Content (%)	15.9
Relative Density (S.G.)	

Sieve Analysis (Wet Prep) SANS3001: GR1

Percentage Passing	100 mm	75 mm	63 mm	50 mm	37.5 mm	28 mm	20 mm	14 mm	5 mm	2 mm	1 mm	0.425 mm	0.250 mm	0.150 mm	0.075 mm
	100	100	100	100	100	100	100	100	82	74	68	53	49	44	42
Grading Modulus	1.31	1.47													



Hydrometer Analysis ASTM D422

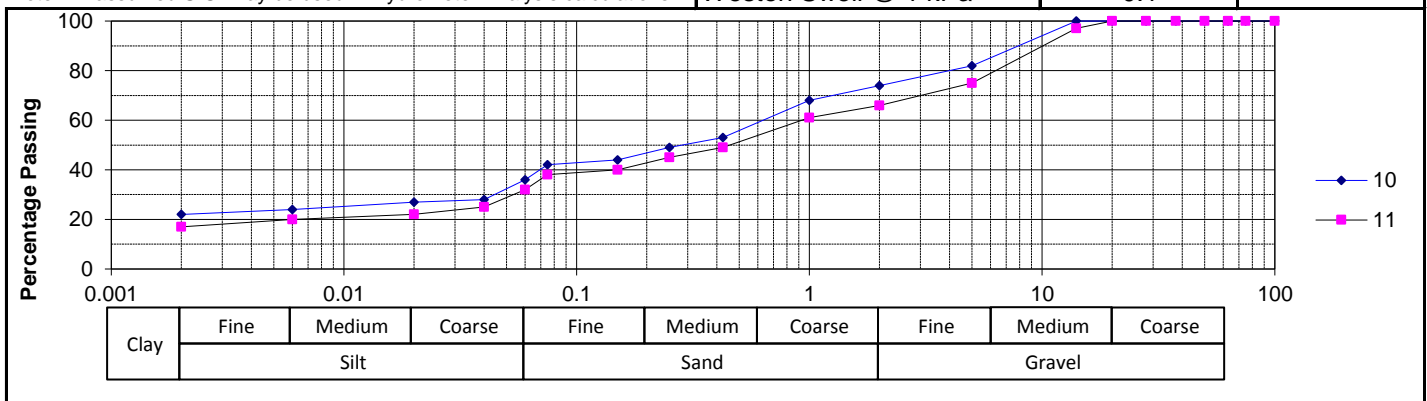
Percentage Passing	0.060 mm	0.040 mm	0.020 mm	0.006 mm	0.002 mm
	36	28	27	24	22
Gravel	%	26	34		
Sand	%	38	34		
Silt	%	14	15		
Clay	%	22	17		

Laboratory Number	10 ◆	11 ■	
Atterberg Limits -425µ	SANS3001: GR10		
Liquid Limit	%	34	32
Plasticity Index	%	16	16
Linear Shrinkage	%	7.0	8.0
Overall PI	%	8	8

Classifications

HRB (AASHTO)	A-6(3)	A-6(2)
Unified (ASTM D2487)	SC	SC
Weston Swell @ 1 kPa	0.1	

Note: An assumed S.G. may be used in Hydrometer Analysis calculations

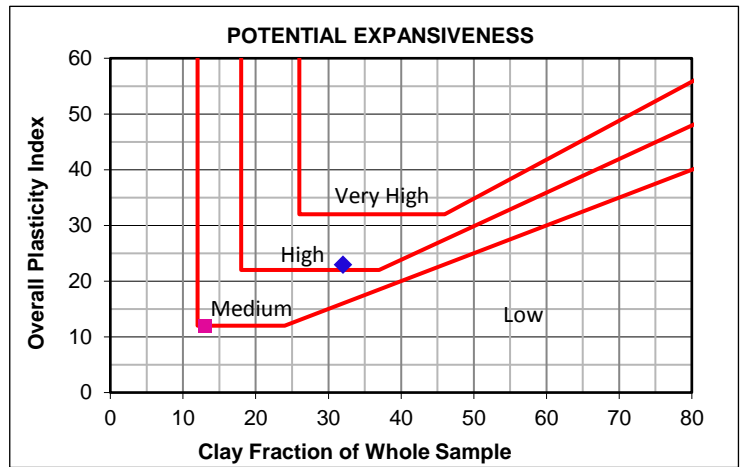


Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No : 2018-B-2286

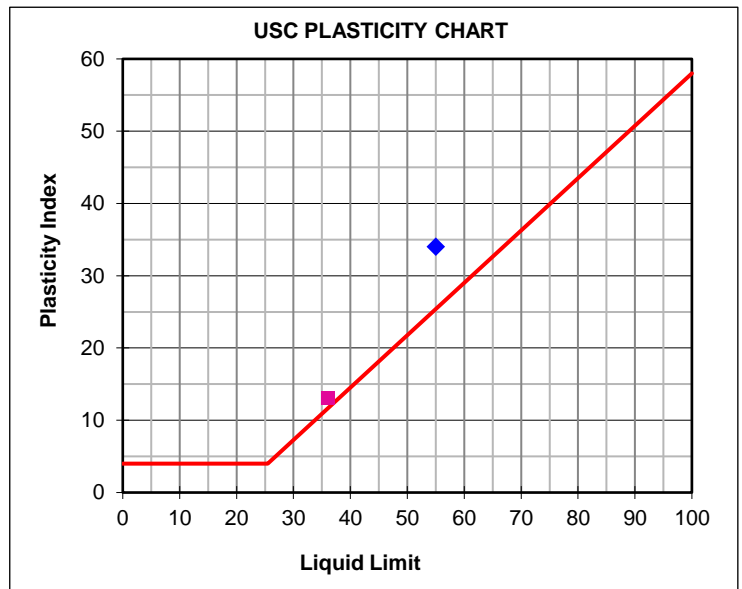
Date Received: 28/11/2018
 Date Reported: 14/02/2019
 Page No. : 7 of 20

FOUNDATION INDICATOR

Laboratory Number	12 ◆	14 ■
Field Number	TP12	TP12
Client Reference		
Depth (m)	0.00-1.30	2.80-4.80
Position		
Coordinates	X Y	
Description		
Additional Information	Organic Rich Vlei Deposit	Residual Carbonaceous
Calcrete / Crushed Stabilizing Agent		



Moisture Content & Relative Density		
Moisture Content (%)	23.5	23.7
Relative Density (S.G.)		



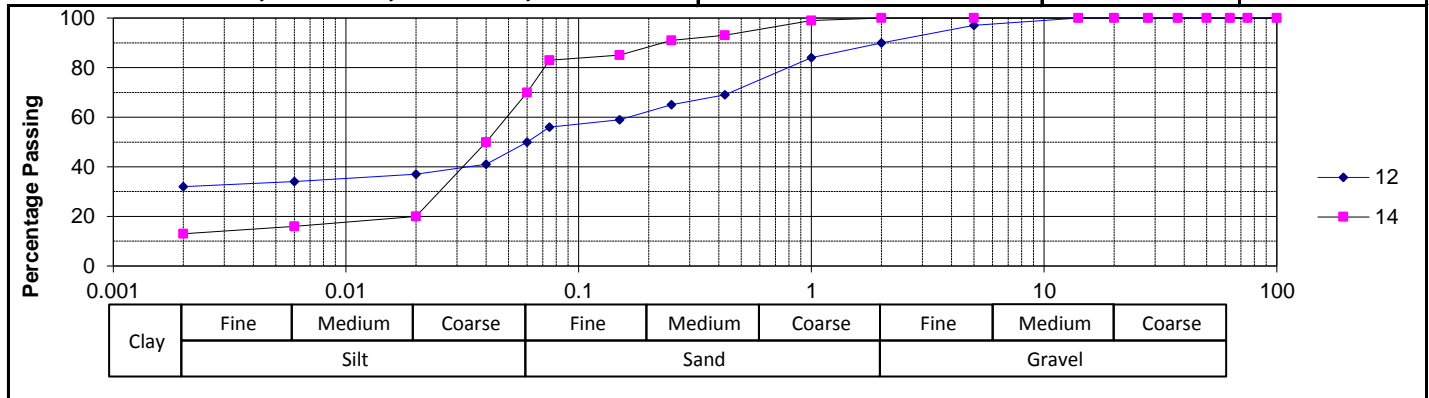
Sieve Analysis (Wet Prep) SANS3001: GR1			
Percentage Passing	100 mm	100	100
	75 mm	100	100
	63 mm	100	100
	50 mm	100	100
	37.5 mm	100	100
	28 mm	100	100
	20 mm	100	100
	14 mm	100	100
	5 mm	97	100
	2 mm	90	100
	1 mm	84	99
	0.425 mm	69	93
	0.250 mm	65	91
	0.150 mm	59	85
0.075 mm	56	83	
Grading Modulus	0.85	0.24	

Laboratory Number	12 ◆	14 ■
Atterberg Limits -425µ SANS3001: GR10		
Liquid Limit	% 55	36
Plasticity Index	% 34	13
Linear Shrinkage	% 16.0	5.0
Overall PI	% 23	12

Hydrometer Analysis ASTM D422			
Percentage Passing	0.060 mm	50	70
	0.040 mm	41	50
	0.020 mm	37	20
	0.006 mm	34	16
	0.002 mm	32	13
Gravel	%	10	
Sand	%	40	30
Silt	%	18	57
Clay	%	32	13

Classifications		
HRB (AASHTO)	A-7-6(16)	A-6(11)
Unified (ASTM D2487)	CH	CL
Weston Swell @ 1 kPa	1.0	0.6

Note: An assumed S.G. may be used in Hydrometer Analysis calculations

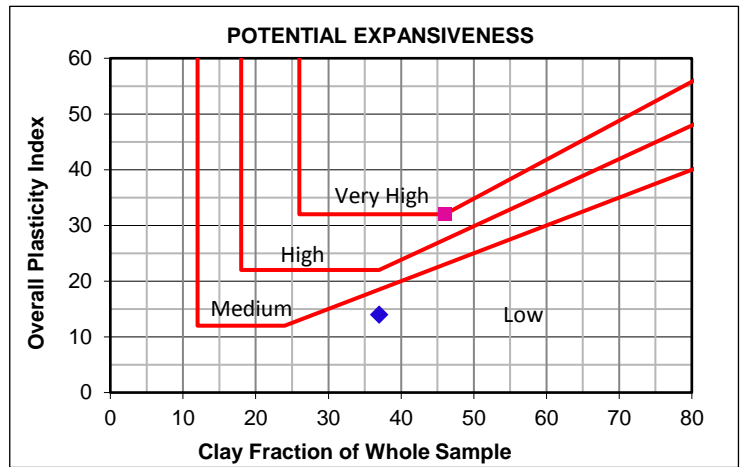


Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No : 2018-B-2286

Date Received: 28/11/2018
 Date Reported: 14/02/2019
 Page No. : 8 of 20

FOUNDATION INDICATOR

Laboratory Number	15 ◆	16 ■
Field Number	TP13	TP13
Client Reference		
Depth (m)	3.80-5.00	1.20-1.40
Position		
Coordinates	X Y	
Description		
Additional Information	Slightly Ferruginous	Alluvium
Calcrete / Crushed Stabilizing Agent		

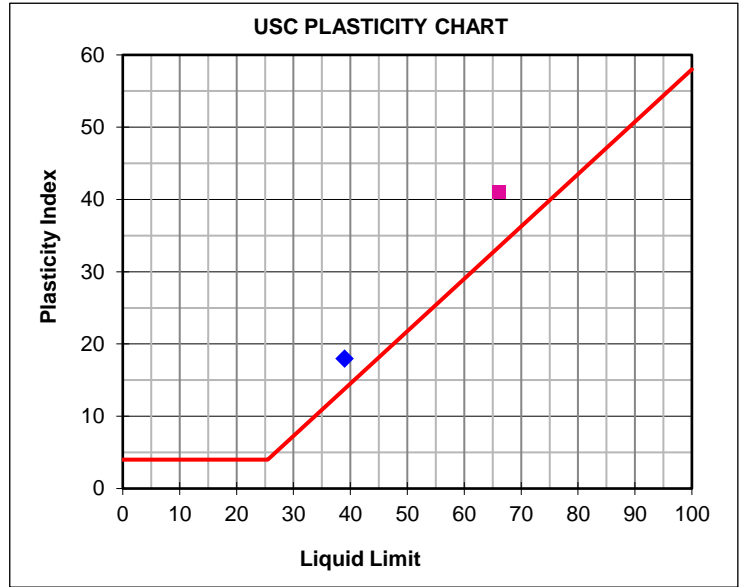


Moisture Content & Relative Density

Moisture Content (%)		
Relative Density (S.G.)		2.519

Sieve Analysis (Wet Prep) SANS3001: GR1

Percentage Passing	15 ◆	16 ■
100 mm	100	100
75 mm	100	100
63 mm	100	100
50 mm	100	100
37.5 mm	100	100
28 mm	100	100
20 mm	100	100
14 mm	100	100
5 mm	99	99
2 mm	95	95
1 mm	90	91
0.425 mm	79	79
0.250 mm	78	76
0.150 mm	76	71
0.075 mm	76	69
Grading Modulus	0.50	0.57



Hydrometer Analysis ASTM D422

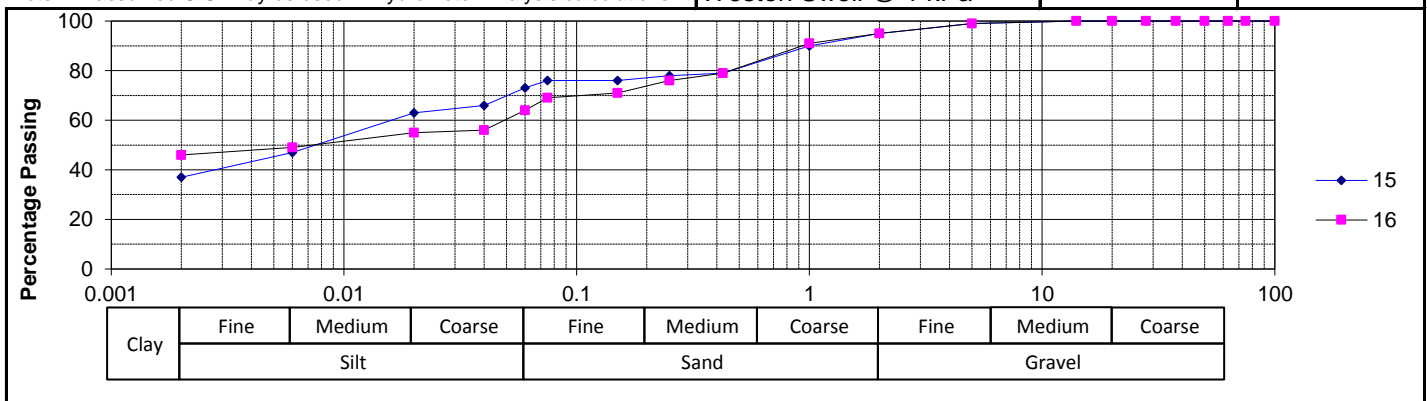
Percentage Passing	15 ◆	16 ■
0.060 mm	73	64
0.040 mm	66	56
0.020 mm	63	55
0.006 mm	47	49
0.002 mm	37	46
Gravel	5	5
Sand	22	31
Silt	36	18
Clay	37	46

Laboratory Number	15 ◆	16 ■
Atterberg Limits -425µ	SANS3001: GR10	
Liquid Limit	% 39	66
Plasticity Index	% 18	41
Linear Shrinkage	% 9.5	17.5
Overall PI	% 14	32

Classifications

HRB (AASHTO)	A-6(13)	A-7-6(20)
Unified (ASTM D2487)	CL	CH
Weston Swell @ 1 kPa		

Note: An assumed S.G. may be used in Hydrometer Analysis calculations

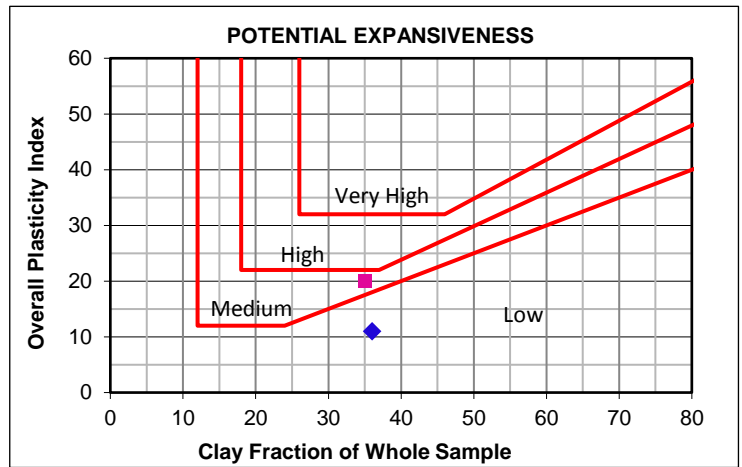


Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No : 2018-B-2286

Date Received: 28/11/2018
 Date Reported: 14/02/2019
 Page No. : 9 of 20

FOUNDATION INDICATOR

Laboratory Number	17 ◆	18 ■
Field Number	TP15	TP15
Client Reference		
Depth (m)	0.50-1.30	1.30-2.40
Position		
Coordinates	X Y	
Description		
Additional Information	Reworked Residual	Slightly Ferruginous
Calcrete / Crushed Stabilizing Agent		

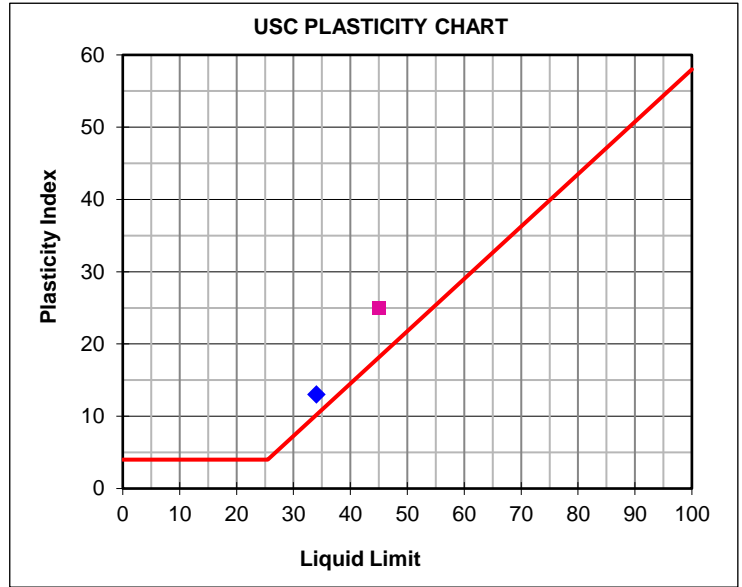


Moisture Content & Relative Density

Moisture Content (%)	15.3	19.4
Relative Density (S.G.)		

Sieve Analysis (Wet Prep) SANS3001: GR1

Percentage Passing	100 mm	75 mm	63 mm	50 mm	37.5 mm	28 mm	20 mm	14 mm	5 mm	2 mm	1 mm	0.425 mm	0.250 mm	0.150 mm	0.075 mm	Grading Modulus
	100	100	100	100	100	100	100	100	99	97	93	82	81	80	79	0.42
	100	100	100	100	100	100	100	100	100	97	93	80	72	65	62	0.61



Hydrometer Analysis ASTM D422

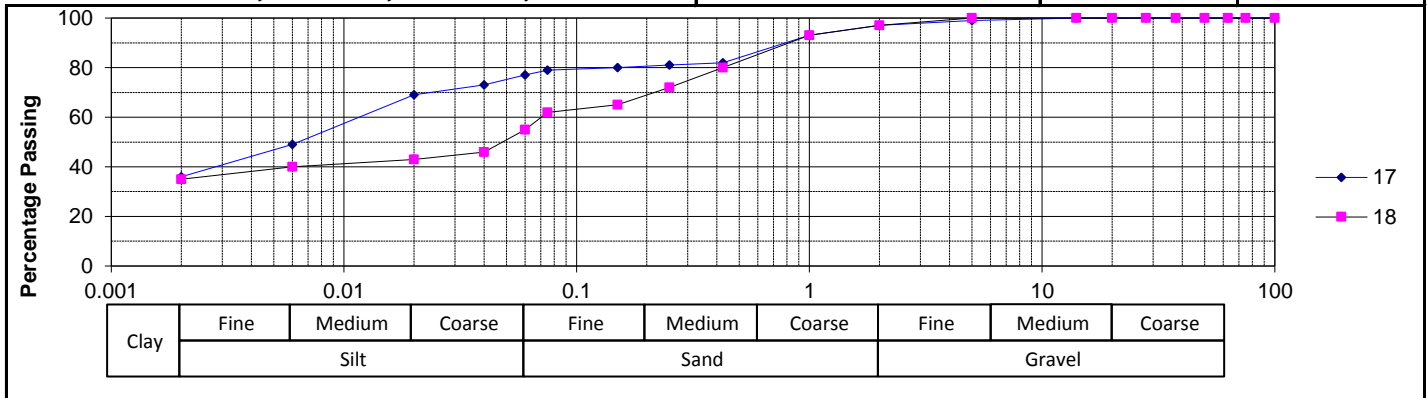
Percentage Passing	0.060 mm	0.040 mm	0.020 mm	0.006 mm	0.002 mm	Gravel	Sand	Silt	Clay
	77	73	69	49	36	3	20	41	36
	55	46	43	40	35	3	42	20	35

Laboratory Number	17 ◆	18 ■
Atterberg Limits -425µ	SANS3001: GR10	
Liquid Limit	% 34	45
Plasticity Index	% 13	25
Linear Shrinkage	% 7.0	11.5
Overall PI	% 11	20

Classifications

HRB (AASHTO)	A-6(9)	A-7-6(13)
Unified (ASTM D2487)	CL	CL
Weston Swell @ 1 kPa	0.8	1.3

Note: An assumed S.G. may be used in Hydrometer Analysis calculations

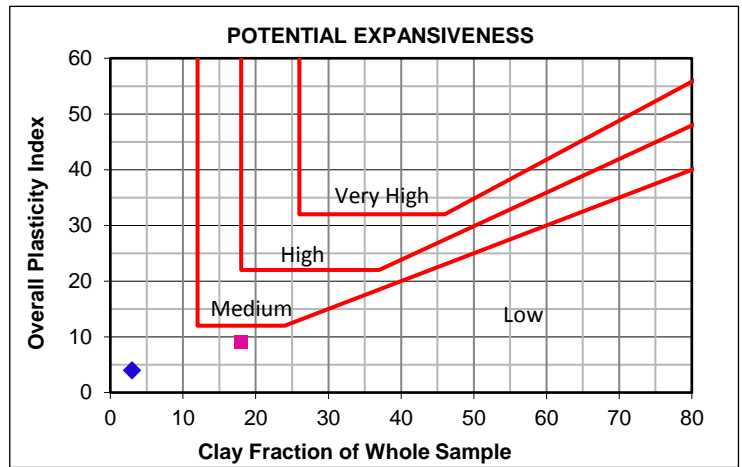


Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No : 2018-B-2286

Date Received: 28/11/2018
 Date Reported: 14/02/2019
 Page No. : 10 of 20

FOUNDATION INDICATOR

Laboratory Number	19	20
Field Number	TP15	TP15
Client Reference		
Depth (m)	2.6	0.50-1.30
Position		
Coordinates	X Y	
Description		
Additional Information		Fill
Calcrete / Crushed Stabilizing Agent		

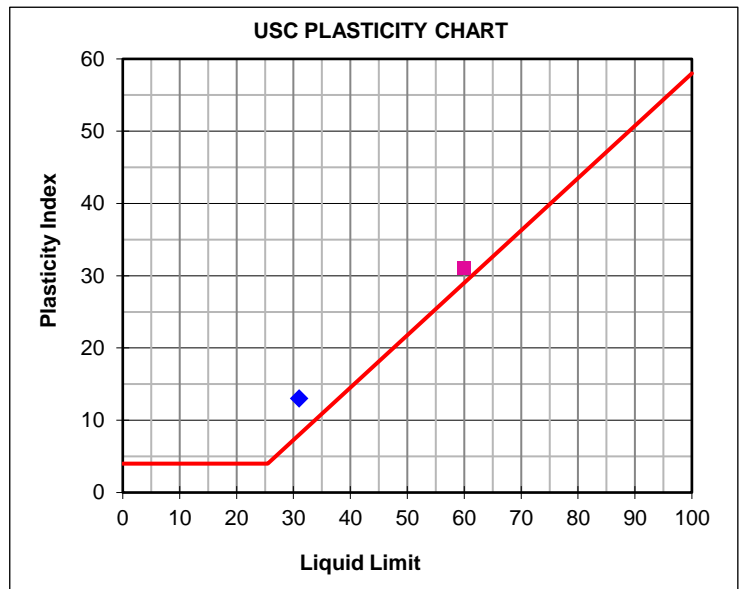


Moisture Content & Relative Density

Moisture Content (%)	14
Relative Density (S.G.)	

Sieve Analysis (Wet Prep) SANS3001: GR1

Sieve Size	Sample 19 (%)	Sample 20 (%)
100 mm	100	100
75 mm	100	100
63 mm	100	100
50 mm	100	100
37.5 mm	100	100
28 mm	100	100
20 mm	100	100
14 mm	100	98
5 mm	100	66
2 mm	95	49
1 mm	82	41
0.425 mm	33	29
0.250 mm	16	28
0.150 mm	14	27
0.075 mm	14	27
Grading Modulus	1.58	1.95



Hydrometer Analysis ASTM D422

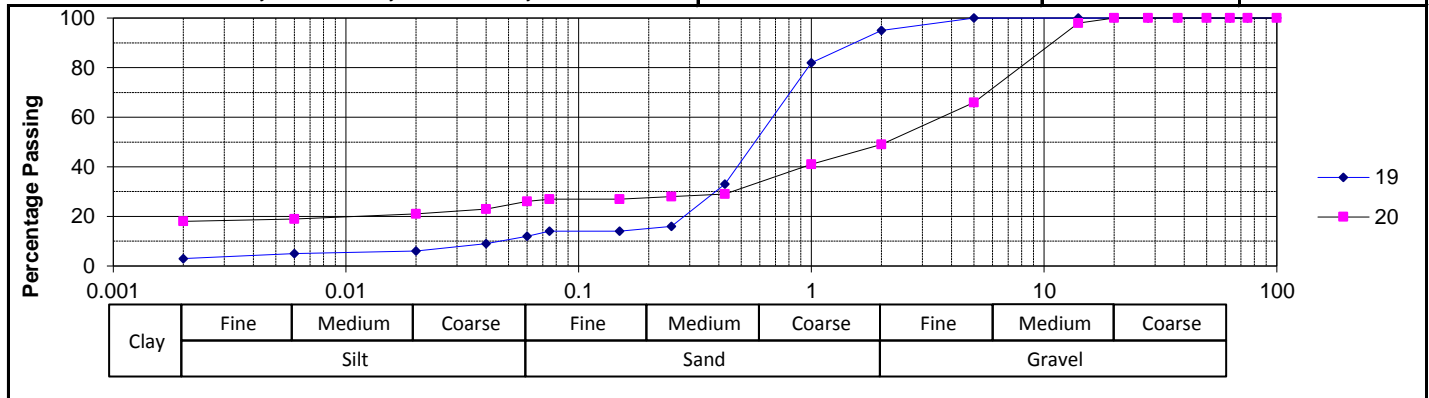
Percentage Passing	Sample 19 (%)	Sample 20 (%)
0.060 mm	12	26
0.040 mm	9	23
0.020 mm	6	21
0.006 mm	5	19
0.002 mm	3	18
Gravel	5	51
Sand	83	23
Silt	9	8
Clay	3	18

Laboratory Number	19	20
Atterberg Limits -425µ	SANS3001: GR10	
Liquid Limit	31	60
Plasticity Index	13	31
Linear Shrinkage	6.5	15.5
Overall PI	4	9

Classifications

HRB (AASHTO)	A-2-6(0)	A-2-7(3)
Unified (ASTM D2487)	SC	SC
Weston Swell @ 1 kPa	0.0	

Note: An assumed S.G. may be used in Hydrometer Analysis calculations

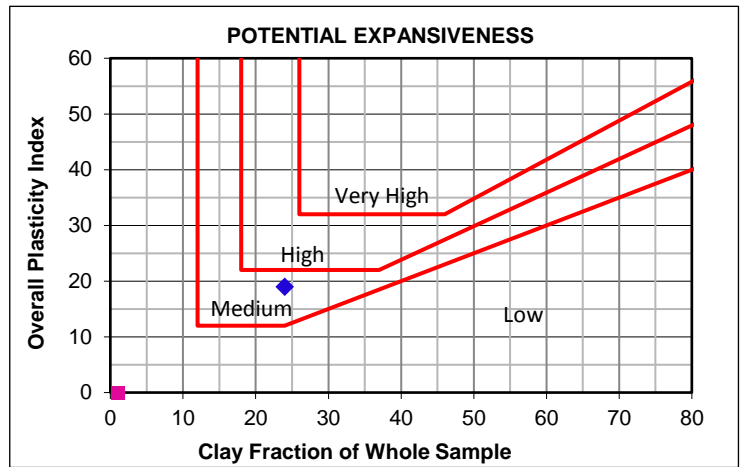


Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No : 2018-B-2286

Date Received: 28/11/2018
 Date Reported: 14/02/2019
 Page No. : 12 of 20

FOUNDATION INDICATOR

Laboratory Number	13	
Field Number	TP12	
Client Reference		
Depth (m)	1.90-2.80	
Position		
Coordinates	X Y	
Description		
Additional Information	Ferruginous Alluvium	
Calcrete / Crushed Stabilizing Agent		

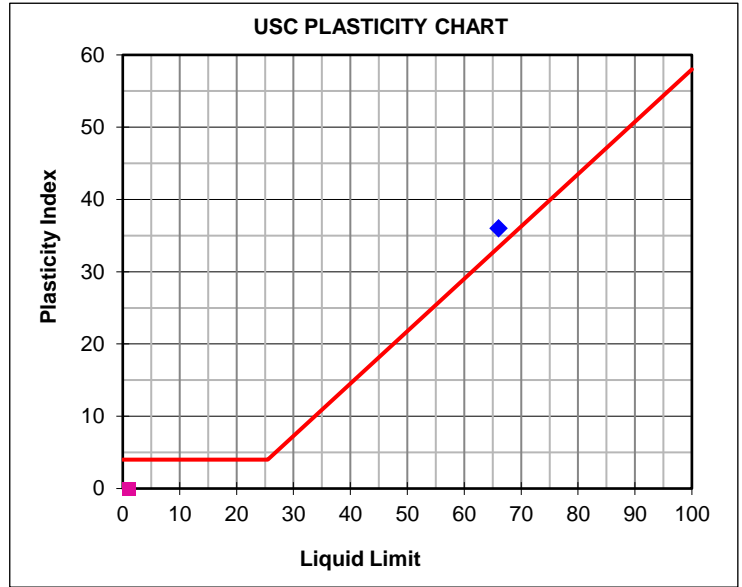


Moisture Content & Relative Density

Moisture Content (%)	31.4
Relative Density (S.G.)	

Sieve Analysis (Wet Prep) SANS3001: GR1

Sieve Size	Percentage Passing
100 mm	100
75 mm	100
63 mm	100
53 mm	100
37.5 mm	100
26.5 mm	100
19 mm	100
13.2 mm	100
4.75 mm	96
2 mm	85
0.85 mm	73
0.425 mm	52
0.250 mm	50
0.150 mm	47
0.075 mm	47
Grading Modulus	1.16



Hydrometer Analysis ASTM D422

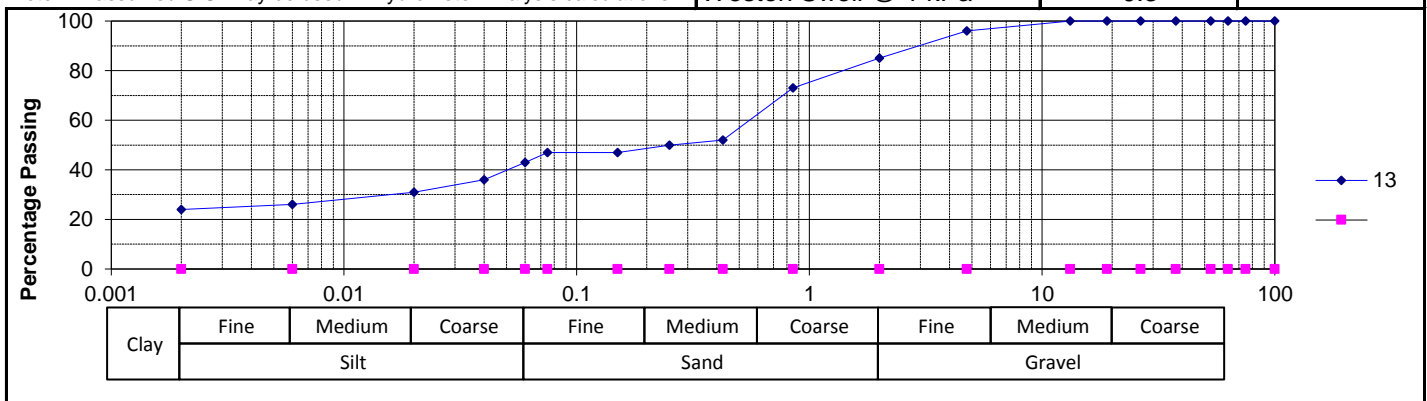
Sieve Size	Percentage Passing
0.060 mm	43
0.040 mm	36
0.020 mm	31
0.006 mm	26
0.002 mm	24
Gravel	% 15
Sand	% 42
Silt	% 19
Clay	% 24

Laboratory Number	13
Atterberg Limits -425µ	SANS3001: GR10
Liquid Limit	% 66
Plasticity Index	% 36
Linear Shrinkage	% 18.0
Overall PI	% 19

Classifications

HRB (AASHTO)	A-7-5(12)
Unified (ASTM D2487)	SC
Weston Swell @ 1 kPa	0.3

Note: An assumed S.G. may be used in Hydrometer Analysis calculations



Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No: 2018-B-2286

Date Received: 28/11/2018
 Date Reported: 14/02/2019
 Page No. : 13 of 20

MOISTURE DENSITY RELATIONSHIP

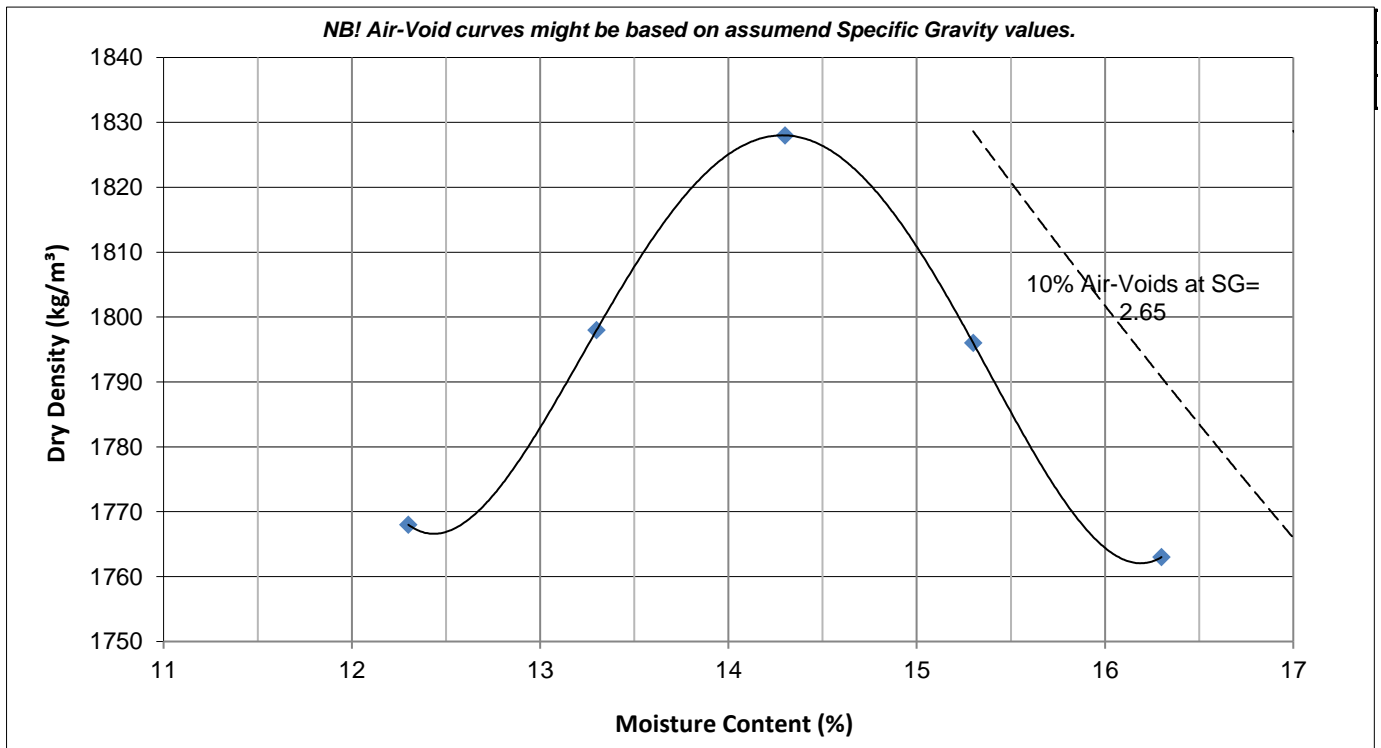
Laboratory Number	3	
Field Number	TP02	
Client Reference		
Depth (m)	0.90-1.40	
Position		
Coordinates	X	
	Y	
Description		
Additional Information	Fill	
Calcrete / Crushed Stabilizing Agent		

Maximum Dry Density & Optimum Moisture Content - SANS3001: GR30

Compactive Effort:	Modified AASHTO
--------------------	-----------------

Dry Density	kg/m ³	1768	1798	1828	1796	1763	
Moisture Content	%	12.3	13.3	14.3	15.3	16.3	

Max. Dry Density	kg/m ³	1828
Optimum Moisture	%	14.3



Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No: 2018-B-2286

Date Received: 28/11/2018
 Date Reported: 14/02/2019
 Page No. : 14 of 20

MOISTURE DENSITY RELATIONSHIP

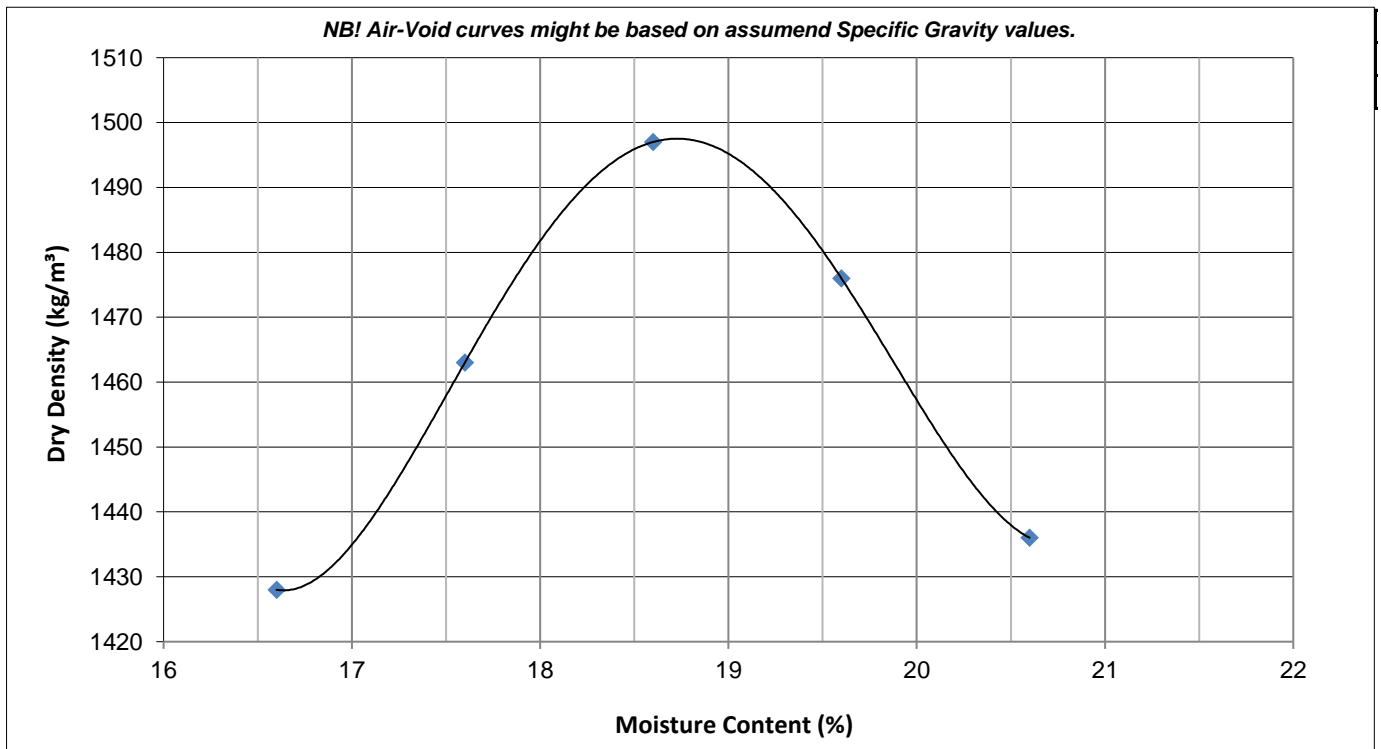
Laboratory Number	6	
Field Number	TP06	
Client Reference		
Depth (m)	0.20-1.20	
Position		
Coordinates	X	
	Y	
Description		
Additional Information	Fill	
Calcrete / Crushed		
Stabilizing Agent		

Maximum Dry Density & Optimum Moisture Content - SANS3001: GR30

Compactive Effort:	Modified AASHTO
--------------------	-----------------

Dry Density	kg/m ³	1428	1463	1497	1476	1436	
Moisture Content	%	16.6	17.6	18.6	19.6	20.6	

Max. Dry Density	kg/m ³	1497
Optimum Moisture	%	18.7



Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No: 2018-B-2286

Date Received: 28/11/2018
 Date Reported: 14/02/2019
 Page No. : 15 of 20

MOISTURE DENSITY RELATIONSHIP

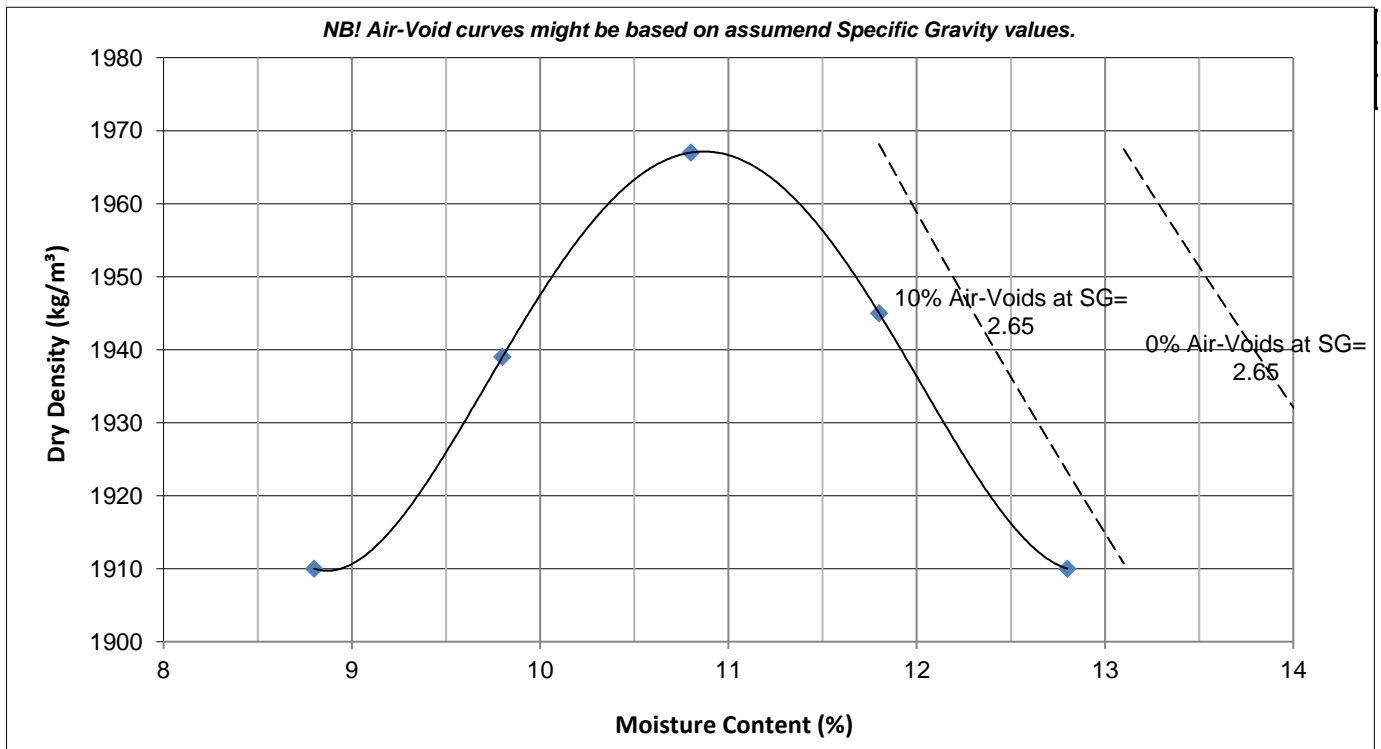
Laboratory Number	11	
Field Number	TP10	
Client Reference		
Depth (m)	0.60-1.90	
Position		
Coordinates	X	
	Y	
Description		
Additional Information	Fill	
Calcrete / Crushed		
Stabilizing Agent		

Maximum Dry Density & Optimum Moisture Content - SANS3001: GR30

Compactive Effort:	Modified AASHTO
--------------------	-----------------

Dry Density	kg/m ³	1910	1939	1967	1945	1910	
Moisture Content	%	8.8	9.8	10.8	11.8	12.8	

Max. Dry Density	kg/m ³	1967
Optimum Moisture	%	10.9



Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No: 2018-B-2286

Date Received: 28/11/2018
 Date Reported: 14/02/2019
 Page No. : 16 of 20

MOISTURE DENSITY RELATIONSHIP

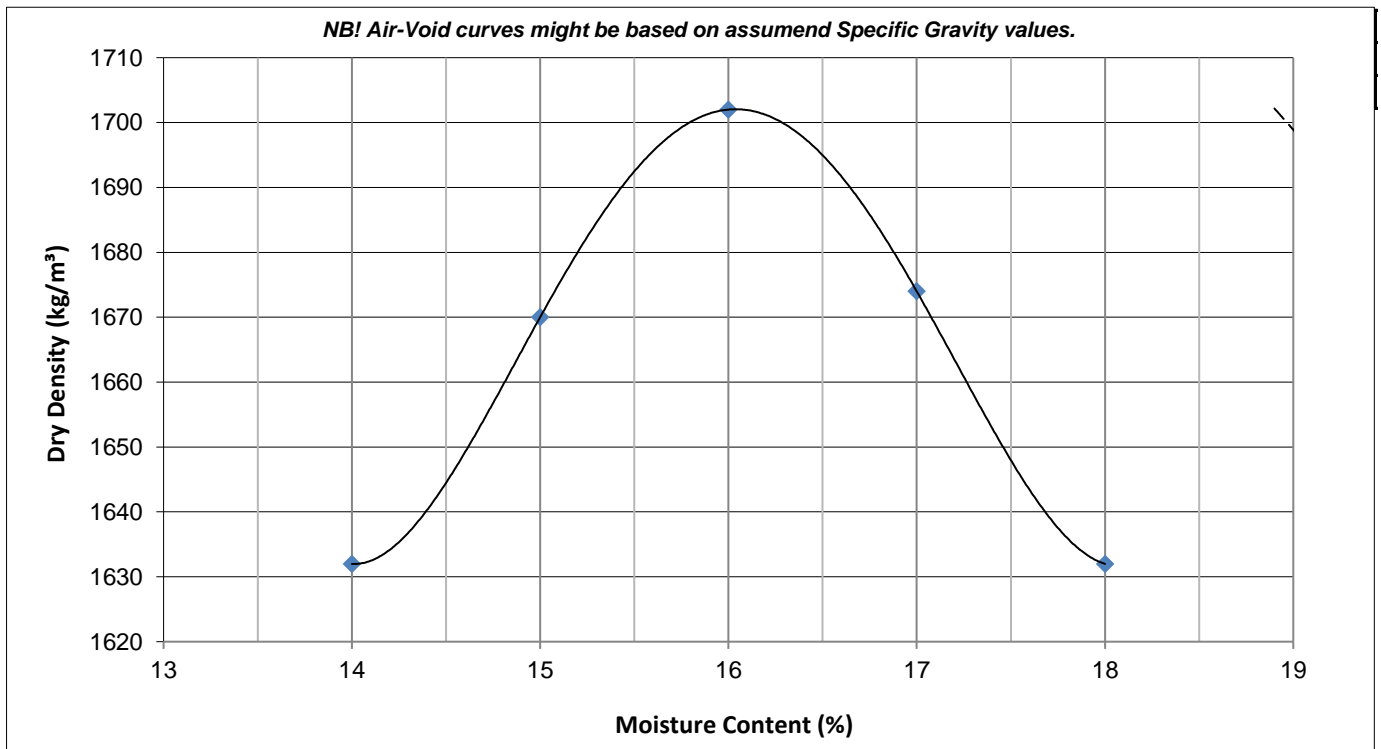
Laboratory Number	20	
Field Number	TP15	
Client Reference		
Depth (m)	0.50-1.30	
Position		
Coordinates	X	
	Y	
Description		
Additional Information	Fill	
Calcrete / Crushed		
Stabilizing Agent		

Maximum Dry Density & Optimum Moisture Content - SANS3001: GR30

Compactive Effort:	Modified AASHTO
--------------------	-----------------

Dry Density	kg/m ³	1632	1670	1702	1674	1632	
Moisture Content	%	14	15	16	17	18	

Max. Dry Density	kg/m ³	1702
Optimum Moisture	%	16



Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No: 2018-B-2286

Date Received: 28/11/2018
 Date Reported: 14/02/2019
 Page No. : 17 of 20

MOISTURE DENSITY RELATIONSHIP

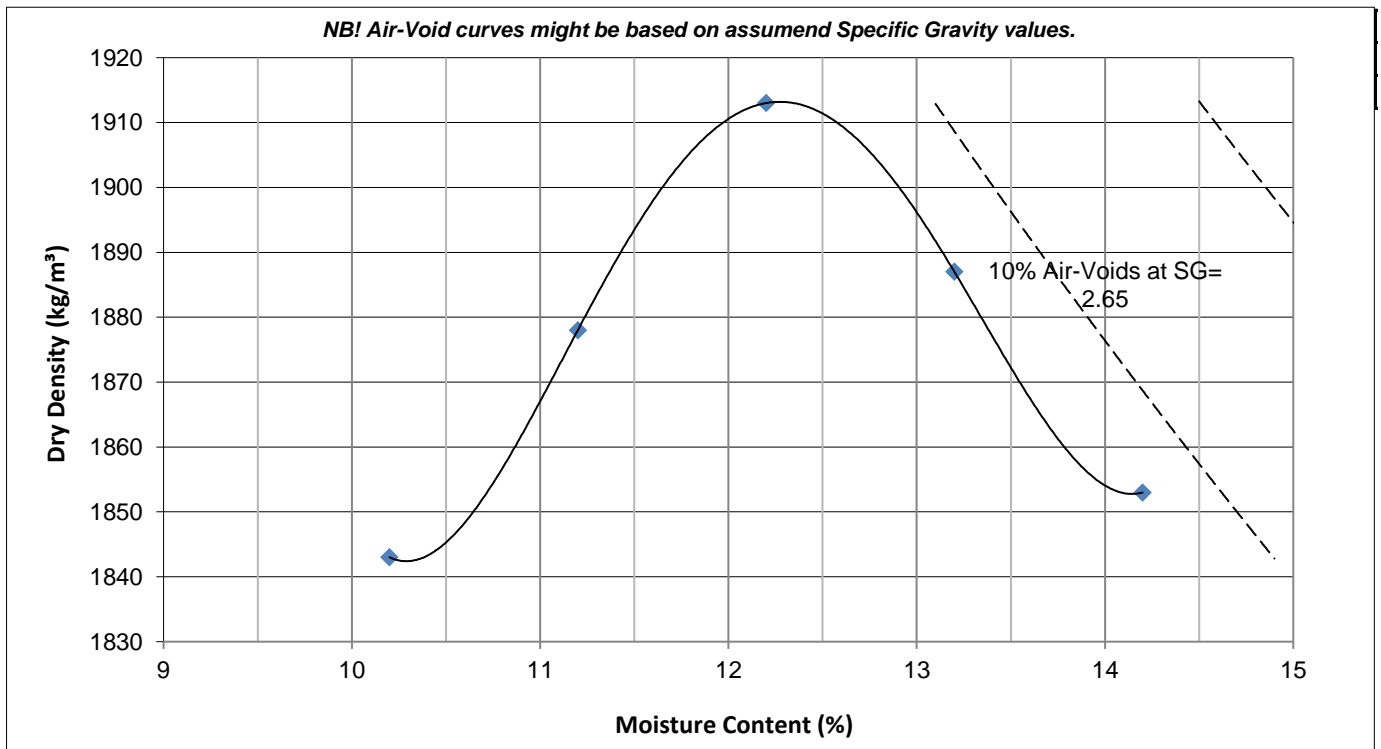
Laboratory Number	21	
Field Number	WBA2	
Client Reference		
Depth (m)	Stockpile	
Position		
Coordinates	X	
	Y	
Description		
Additional Information	Fill- Nodular Ferricrete	
Calcrete / Crushed		
Stabilizing Agent		

Maximum Dry Density & Optimum Moisture Content - SANS3001: GR30

Compactive Effort:	Modified AASHTO
--------------------	-----------------

Dry Density	kg/m ³	1843	1878	1913	1887	1853	
Moisture Content	%	10.2	11.2	12.2	13.2	14.2	

Max. Dry Density	kg/m ³	1913
Optimum Moisture	%	12.3



Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No. : 2018-B-2286

Date Received : 28/11/2018
 Date Reported : 14/02/2019
 Page No. : 18 of 20

CALIFORNIA BEARING RATIO (CBR) & ROAD INDICATOR REPORT

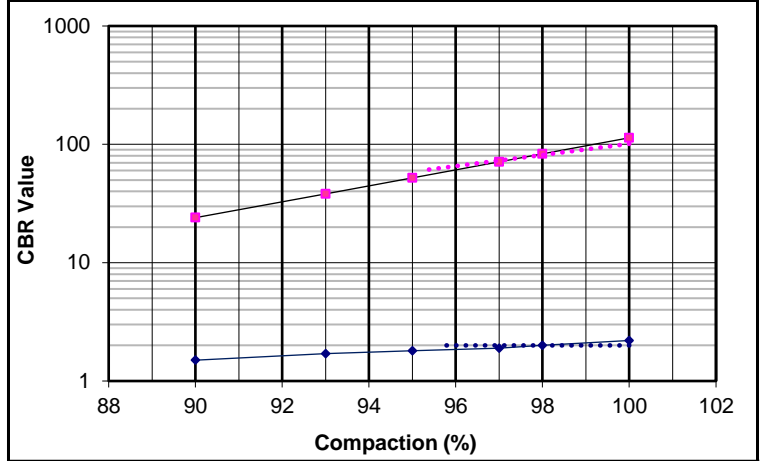
Laboratory No.	3	6
Field Number	TP02	TP06
Client Reference		
Depth (m)	0.90-1.40	0.20-1.20
Position		
Coordinates	X Y	
Description		
Additional information	Fill	Fill
Calcrete/Crushed		
Stabilizing Agent		

Laboratory No.	3	6
Maximum Dry Density & Optimum Moisture Content		SANS3001: GR30
MDD	kg/m ³	1828
OMC	%	14.3
		1497
		18.7

California Bearing Ratio		SANS3001: GR40				
Compaction Data						
Moisture	%	14.4			18.8	
Dry Density	kg/m ³	1833	1752	1639	1499	1427
Compaction	%	100.0	95.6	89.4	100.0	95.2

Penetration Data						
CBR at	2.50 mm	2	2	1	101	60
	5.00 mm	2	2	1	125	67
	7.50 mm	2	2	1	130	69
Swell	%	7.4	8.2	8.4	0	0.1
Final Moisture (%)		22.2	23.9	27.5	20.6	23.6

Sieve Analysis (Wet preparation)		SANS3001: GR1
Percentage Passing	100 mm	100
	75 mm	100
	63 mm	100
	50 mm	100
	37.5 mm	93
	28 mm	83
	20 mm	72
	14 mm	65
	5 mm	55
	2 mm	49
	1 mm	44
	0.425 mm	35
	0.250 mm	33
	0.150 mm	30
0.075 mm	29	
Grading Modulus	1.9	2.3

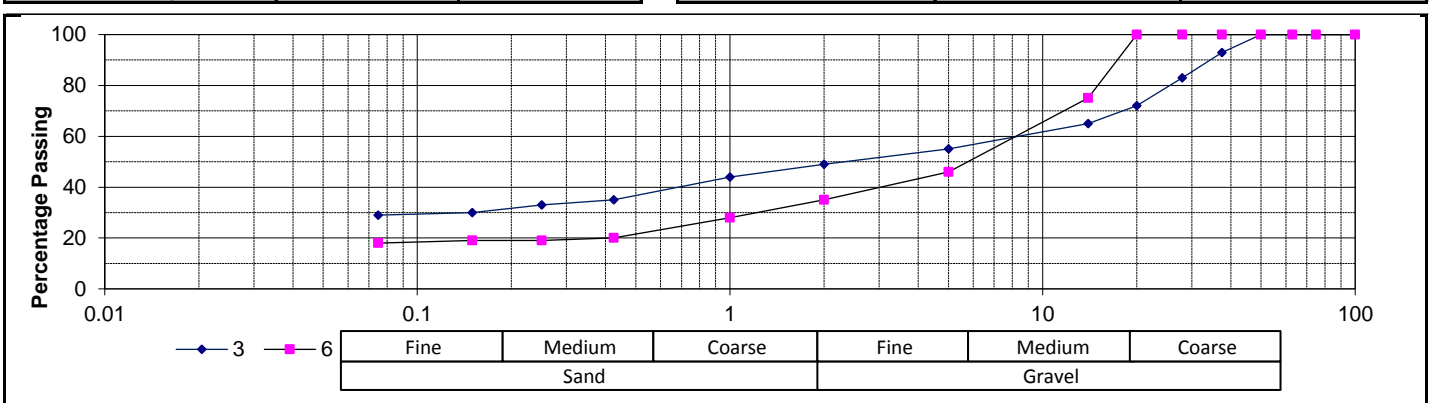


Soil Mortar Analysis	
Coarse Sand	29
Coarse Fine Sand	5
Medium Fine Sand	5
Fine Fine Sand	3
Silt and Clay	59

Interpolated CBR Data		
@ 100%	2	114
@ 98%	2	83
@ 97%	2	71
@ 95%	2	52
@ 93%	2	38
@ 90%	2	24
@ SANS3001 Midpoint	2	78

Atterberg Limits		SANS3001: GR10
Liquid Limit (%)	49	
Plasticity Index (%)	26	SP
Linear Shrinkage (%)	13.5	1.0

Classifications	
HRB (AASHTO)	A-2-7(2)
COLTO	None
TRH14	None



Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No. : 2018-B-2286

Date Received : 28/11/2018
 Date Reported : 14/02/2019
 Page No. : 19 of 20

CALIFORNIA BEARING RATIO (CBR) & ROAD INDICATOR REPORT

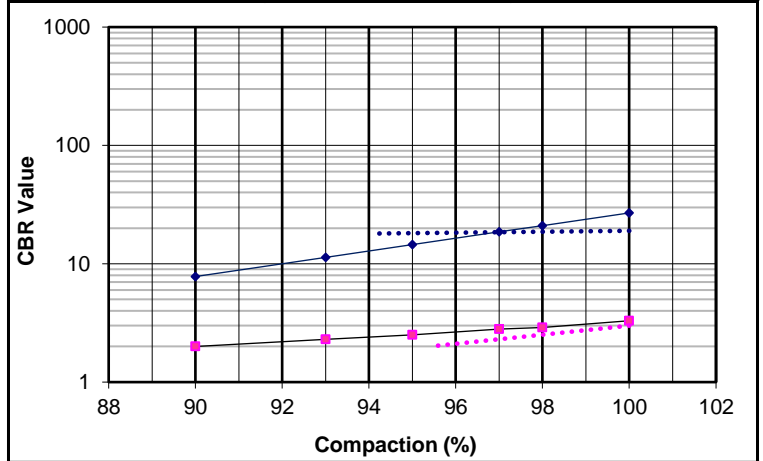
Laboratory No.	11	20
Field Number	TP10	TP15
Client Reference		
Depth (m)	0.60-1.90	0.50-1.30
Position		
Coordinates	X	
	Y	
Description		
Additional information	Fill	Fill
Calcrete/Crushed		
Stabilizing Agent		

Laboratory No.	11	20
Maximum Dry Density & Optimum Moisture Content		SANS3001: GR30
MDD	kg/m ³	1967
OMC	%	10.9
		1702
		16

California Bearing Ratio		SANS3001: GR40
Compaction Data		
Moisture	%	10.9
Dry Density	kg/m ³	1983 1866 1770
Compaction	%	100.0 94.1 89.3
		1702 1623 1552
		100.0 95.4 91.2

Penetration Data		
CBR at	2.50 mm	19 18 7
	5.00 mm	17 16 6
	7.50 mm	16 14 6
Swell	%	0.5 0.7 0.8
Final Moisture (%)		2.5 3 3.8
		13.2 18 20.6
		24.7 26.4 30.6

Sieve Analysis (Wet preparation)		SANS3001: GR1
Percentage Passing	100 mm	100
	75 mm	100
	63 mm	100
	50 mm	100
	37.5 mm	100
	28 mm	100
	20 mm	100
	14 mm	97
	5 mm	75
	2 mm	66
	1 mm	61
	0.425 mm	49
	0.250 mm	45
	0.150 mm	40
	0.075 mm	38
Grading Modulus		1.5
		2.0

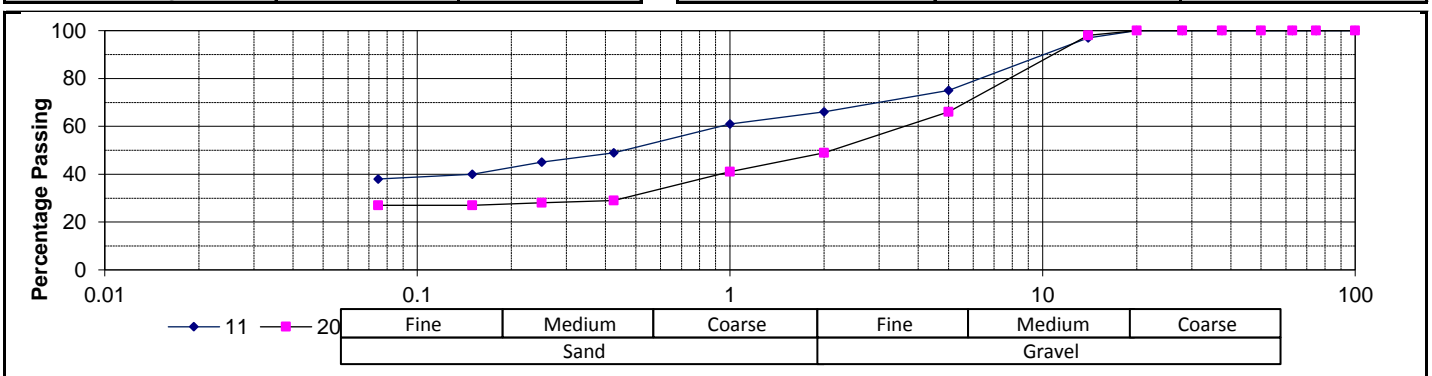


Interpolated CBR Data		
CBR	@ 100%	27
	@ 98%	21
	@ 97%	19
	@ 95%	15
	@ 93%	11
	@ 90%	8
	@ SANS3001 Midpoint	19
	Mod. AASHTO	3
		3
		3
		3
		2
		2
		3

Soil Mortar Analysis	
Coarse Sand	26
Coarse Fine Sand	6
Medium Fine Sand	8
Fine Fine Sand	3
Silt and Clay	57

Classifications		
HRB (AASHTO)	A-6(2)	A-2-7(3)
COLTO	None	None
TRH14	G9	None

Atterberg Limits		SANS3001: GR10
Liquid Limit (%)	32	60
Plasticity Index (%)	16	31
Linear Shrinkage (%)	8.0	15.5



Client : KNIGHT PIESOLD (PTY) LTD
 Project : Vereeniging Pump Station
 Project No. : 2018-B-2286

Date Received : 28/11/2018
 Date Reported : 14/02/2019
 Page No. : 20 of 20

CALIFORNIA BEARING RATIO (CBR) & ROAD INDICATOR REPORT

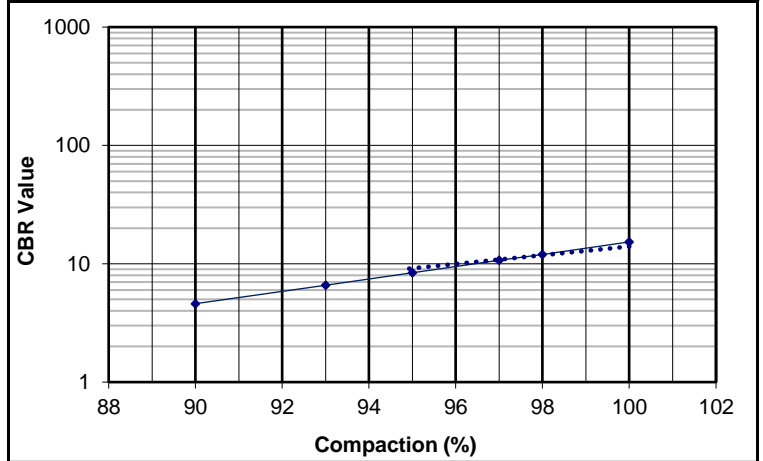
Laboratory No.	21	
Field Number	WBA2	
Client Reference		
Depth (m)	Stockpile	
Position		
Coordinates	X	
	Y	
Description		
Additional information	Fill- Nodular Ferricrete	
Calcrete/Crushed		
Stabilizing Agent		

Laboratory No.	21	
Maximum Dry Density & Optimum Moisture Content		SANS3001: GR30
MDD	kg/m ³	1913
OMC	%	12.3

California Bearing Ratio		SANS3001: GR40
Compaction Data		
Moisture	%	12.2
Dry Density	kg/m ³	1918 1819 1725
Compaction	%	100.0 94.8 89.9

Penetration Data		
CBR at	2.50 mm	14 9 5
	5.00 mm	14 7 4
	7.50 mm	14 7 4
Swell	%	1.5 1.6 1.9
Final Moisture (%)		16.8 19.4 22

Sieve Analysis (Wet preparation)		SANS3001: GR1
Percentage Passing	100 mm	100
	75 mm	100
	63 mm	100
	50 mm	100
	37.5 mm	100
	28 mm	100
	20 mm	100
	14 mm	96
	5 mm	69
	2 mm	61
	1 mm	55
	0.425 mm	41
	0.250 mm	37
	0.150 mm	34
	0.075 mm	32
Grading Modulus		1.7

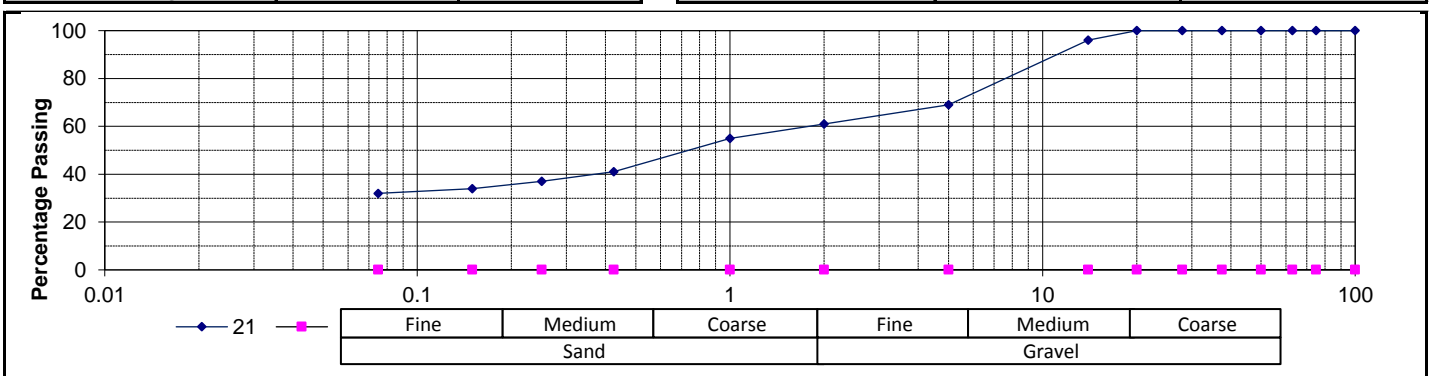


Interpolated CBR Data		
CBR	@ 100%	15
	@ 98%	12
	@ 97%	11
	@ 95%	8
	@ 93%	7
	@ 90%	5
	@ SANS3001 Midpoint	11

Soil Mortar Analysis	
Coarse Sand	33
Coarse Fine Sand	6
Medium Fine Sand	6
Fine Fine Sand	3
Silt and Clay	52

Classifications	
HRB (AASHTO)	A-2-7(2)
COLTO	None
TRH14	G10

Atterberg Limits		SANS3001: GR10
Liquid Limit (%)	41	
Plasticity Index (%)	23	
Linear Shrinkage (%)	11.5	

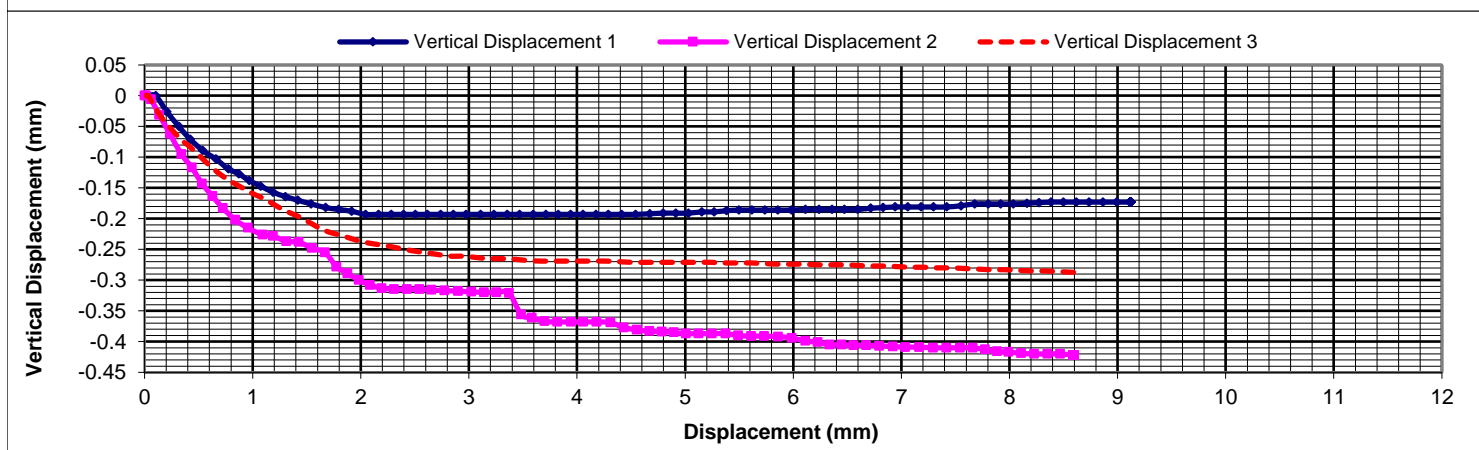
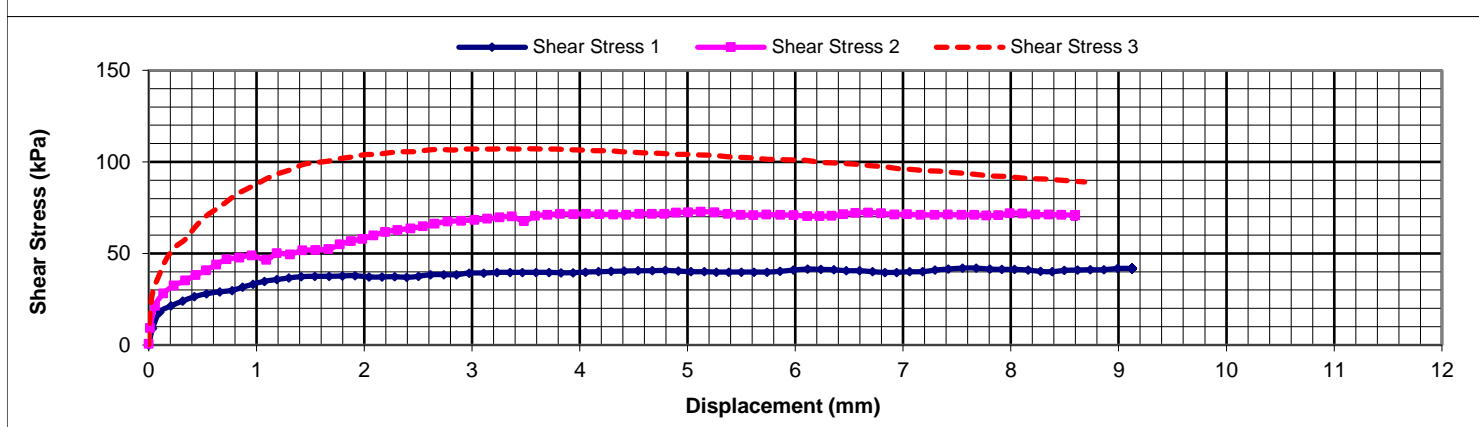
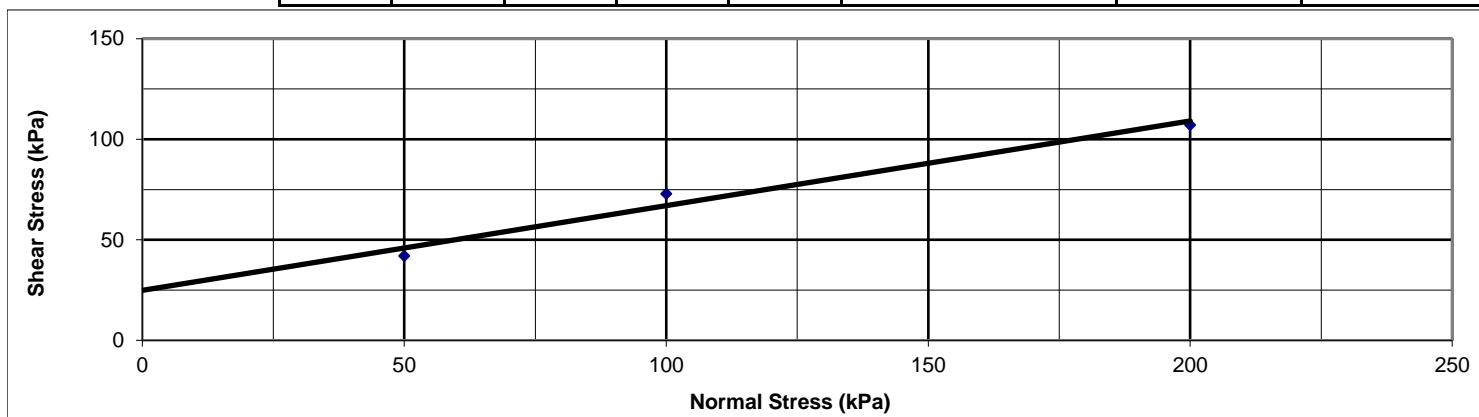


Direct Shear Test Results

Project: VEREENIGING PUMP STATION	Date Tested: 4/12/2018
Batch No.: 2018-B-2286	Laboratory Number: 16
Field Sample Number: TP 13	Depth (m): 1.2 - 1.4

Remark: **A slow drained test on an undisturbed sample.**

		Height mm	Area mm ²	Moisture Content %	Dry Unit Weight	Void Ratio e	Saturation %	Normal Stress kPa	Peak Shear	
									Stress kPa	Displacement mm
Test 1	Initial	17.77	2807.68	25.1	1.26	0.996	63.4	50.0	42.0	7.68
	Final			34.9						
Test 2	Initial	17.77	2807.68	27.2	1.35	0.864	79.4	100.0	72.9	5.12
	Final			32.1						
Test 3	Initial	17.77	2807.68	26.2	1.47	0.710	93.0	200.0	107.2	3.54
	Final			29.9						
		Box Type	Rate of shear (mm/min)			Specific Gravity		2.519	Internal Friction (deg)	Cohesion (kPa)
			Test 1	Test 2	Test 3					
		ROUND	0.0585	0.0569	0.0564			22.8	24.9	



Falling Head Permeability Test Results

Project:	VEREENIGING PUMP STATION		
Project No:	2018-B-2286	Date:	21-Jan-19

Lab. Sample Reference	Field Sample Reference	Depth (m)	Moisture Contents		Dry density Kg/m ³		Coefficient of Permeability (m/s)		
			Before Test (%)	After Test (%)	Initial	As tested	Range		Average
							Minimum	Maximum	
2286-20	TP 15	5.0 - 6.0	17.6	26.2	1576	1639	3.8E-08	4.8E-08	4.1E-08
2286-21	WBA 2	Stockpile	15.1	22.6	1774	1781	3.0E-09	3.9E-09	3.2E-09

Remarks: Samples remoulded to approximately 95% Mod.AASHTO
 Saturated and tested under a load of 100kPa.
 Densities reported are under a load of 100kPa.

COMPACTIBILITY FACTOR

Project : VEREENIGING PUMP STATION	
Project No. : 2018-B-2286	Date : 15 JANUARY 2019

Lab. Sample Ref.	Field Sample Ref.	Depth (m)	Compaction Moisture Content %	Compactibility Factor
2286-6	TP 06	0.2 – 1.2	12.6	0.316
2286-11	TP 10	0.6 – 1.9	8.0	0.333
2286-21	WBA	STOCKPILE	10.1	0.366

REMARKS:

Results reported relate only to the samples tested.

Documents may only be reproduced or published in their full context. While every care is taken to ensure that all tests are carried out in accordance with recognised standards, neither **Civilab** nor its employees shall be liable in any way whatsoever for any error made in the execution or reporting of tests or any erroneous conclusions drawn therefrom or for any consequences thereof.



WATERLAB

WATERLAB (PTY) LTD

23B De Havilland Crescent
Perseus Techno Park,
Meiring Naudé Road, Pretoria
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066
Facsimile: +2712 – 349 – 2064
Email: accounts@waterlab.co.za

CERTIFICATE OF ANALYSES BASSON INDEX

Date received: 2019-01-14
Project number: 150

Report number: 80018

Date completed: 2019-02-05
Order number: PTA06279

Client name: Soillab
Address: PO Box 72928, Lynnwood Ridge, 0040
Telephone: 012 813 4914 / 082 553 1297

Fax: 086 721 3827

Contact person: Ms C Edwards
Email: edwardsc@soillab.co.za

Analyses in mg/ℓ (Unless specified otherwise)	Sample Identification:	
	TP02	TP10
Sample Number	52060	52061
pH Value at 25°C	7.8	7.9
pHs Value at 20°C (calc)	7.9	8.2
Electrical Conductivity in mS/m at 25°C	88.0	30.9
Total Dissolved Solids* (calc)	590	207
Total Alkalinity as CaCO ₃	64	64
Total Hardness as CaCO ₃ (calc)	343	125
Calcium Hardness as CaCO ₃ (calc)	244	92
Calcium as Ca	98	37
Magnesium as Mg	24	8
Free & Saline Ammonia	<0.1	<0.1
Ammonium as NH ₄ (calc)	<0.3	<0.3
Sulphate as SO ₄	375	62
Chloride as Cl	6	<2
Langelier Index at 20°C (calc)	-0.1	-0.3
Ryznar Index at 20°C (calc)	7.9	8.6
Corrosivity Ratio (calc)	6.2	1.1
Leaching Index [LCSI] (calc)	346	636
Spalling Index [SCSI] (calc)	43	8
Aggressiveness Index [N _c] (calc)	388	644

*TDS Calculated EC X 6.7
2:1 Distilled Water : Soil Extract

S. Laubscher
Geochemistry Project Manager

The information contained in this report is relevant only to the sample/samples supplied to **WATERLAB (Pty) Ltd**. Any further use of the above information is not the responsibility or liability of **WATERLAB (Pty) Ltd**. Except for the full report, parts of this report may not be reproduced without written approval of **WATERLAB (Pty) Ltd**.



WATERLAB

WATERLAB (PTY) LTD

23B De Havilland Crescent
Perseus Techno Park,
Meiring Naudé Road, Pretoria
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066
Facsimile: +2712 – 349 – 2064
Email: accounts@waterlab.co.za

CERTIFICATE OF ANALYSES BASSON INDEX

Date received: 2019-01-14
Project number: 150

Report number: 80018

Date completed: 2019-02-05
Order number: PTA06279

Client name: Soillab
Address: PO Box 72928, Lynnwood Ridge, 0040
Telephone: 012 813 4914 / 082 553 1297

Fax: 086 721 3827

Contact person: Ms C Edwards
Email: edwardsc@soillab.co.za

Analyses in mg/ℓ (Unless specified otherwise)	Sample Identification:	
	TP13	TP15
Sample Number	52062	52063
pH Value at 25°C	7.5	6.5
pHs Value at 20°C (calc)	8.2	9.8
Electrical Conductivity in mS/m at 25°C	9.2	2.6
Total Dissolved Solids* (calc)	62	17
Total Alkalinity as CaCO ₃	56	16
Total Hardness as CaCO ₃ (calc)	192	20
Calcium Hardness as CaCO ₃ (calc)	100	7
Calcium as Ca	44	3
Magnesium as Mg	20	3
Free & Saline Ammonia	0.2	0.1
Ammonium as NH ₄ (calc)	0.3	<0.3
Sulphate as SO ₄	67	5
Chloride as Cl	61	6
Langelier Index at 20°C (calc)	-0.7	-3.3
Ryznar Index at 20°C (calc)	8.9	13.2
Corrosivity Ratio (calc)	2.9	0.9
Leaching Index [LCSI] (calc)	870	2782
Spalling Index [SCSI] (calc)	12	2
Aggressiveness Index [N _c] (calc)	881	2783

*TDS Calculated EC X 6.7
2:1 Distilled Water : Soil Extract

Important notes (see table for corrections on p.4):

1. The above aggressiveness index is only applicable for conditions of laminar flow at a mean annual temperature of 20°C.
2. For stagnant/turbulent conditions the aggressiveness index must be corrected.
3. For wet/dry cycling conditions (for example in tidal zones) the aggressiveness index must be corrected.
4. For mean annual temperatures lower/higher than 20°C the aggressiveness index must be corrected.

S. Laubscher
Geochemistry Project Manager

The information contained in this report is relevant only to the sample/samples supplied to **WATERLAB (Pty) Ltd**. Any further use of the above information is not the responsibility or liability of **WATERLAB (Pty) Ltd**. Except for the full report, parts of this report may not be reproduced without written approval of **WATERLAB (Pty) Ltd**.



WATERLAB

WATERLAB (PTY) LTD

23B De Havilland Crescent
Persequor Techno Park,
Meiring Naudé Road, Pretoria
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066
Facsimile: +2712 – 349 – 2064
Email: accounts@waterlab.co.za

CERTIFICATE OF ANALYSES BASSON INDEX

Date received: 2019-01-14
Project number: 150

Report number: 80018

Date completed: 2019-02-05
Order number: PTA06279

Client name: Soillab
Address: PO Box 72928, Lynnwood Ridge, 0040
Telephone: 012 813 4914 / 082 553 1297

Fax: 086 721 3827

Contact person: Ms C Edwards
Email: edwardsc@soillab.co.za

Guidelines for assessing overall aggressiveness (N_c):

N_c	Aggressiveness
Not greater than 300	None to mild
400-700	Mild to moderate
800-1000	High
= or > 1 100	Very high

Aggressiveness Towards Concrete and Fibre Cement Pipes			
Index	Aggressive	Neutral	Non- Aggressive
a) Stability pH (pHs)	>Ph	= pH	<pH
b) Langelier Index	Neg. Value	Zero	Pos. Value
c) Ryznar Index	>7.5	6-7	<6

Corrosiveness Towards metals	
Corrosivity	>0.2

Sample Name	Sample Number	Corrosivity Indices	Basson Index
TP02	52060	Corrosive	Aggressive
TP10	52601	Corrosive	Aggressive
TP13	52062	Corrosive	Aggressive
TP15	52063	Corrosive	Aggressive

S. Laubscher
Geochemistry Project Manager

The information contained in this report is relevant only to the sample/samples supplied to WATERLAB (Pty) Ltd. Any further use of the above information is not the responsibility or liability of WATERLAB (Pty) Ltd. Except for the full report, parts of this report may not be reproduced without written approval of WATERLAB (Pty) Ltd.



WATERLAB

WATERLAB (PTY) LTD

23B De Havilland Crescent
Perseus Techno Park,
Meiring Naudé Road, Pretoria
P.O. Box 283, 0020

Telephone: +2712 – 349 – 1066
Facsimile: +2712 – 349 – 2064
Email: accounts@waterlab.co.za

CERTIFICATE OF ANALYSES BASSON INDEX

Date received: 2019-01-14
Project number: 150

Report number: 80018

Date completed: 2019-02-05
Order number: PTA06279

Client name: Soillab
Address: PO Box 72928, Lynnwood Ridge, 0040
Telephone: 012 813 4914 / 082 553 1297

Fax: 086 721 3827

Contact person: Ms C Edwards
Email: edwardsc@soillab.co.za

To correct for:	Multiply	By: (see Notes 2 to 5 below)
Turbulence	LCSI	1.75
Stagnance	LCSI	0.5
Temperature	LCSI, SCSi, N7 Where N7=0.2 x Cl in mg/l	(1+ [0.05 x (T-20)])
Wet-dry cycles	SCSi	0.23 x 10 ⁻⁶ x TDS x DTF x CPA Where: DTF = Dry Time Fraction CPA = wet-dry cycles per annum

Note 1: Only if the concrete contains embedded steel.

Note 2: To preserve the correct logical relationships when dealing with the negative sub indices (ie LCSI or SCSi having minus values) they should be multiplied by the reciprocal of the relevant factor indicated in this column

Note 3: If more than one correction is required, multiply by the product of the individual correction factors

Note 4: Use subscript c to indicate that the index has been corrected, eg for turbulent conditions LCSI_c = LCSI x 1.75

Note 5: Round off corrected indices to the nearest 100.

S. Laubscher
Geochemistry Project Manager

The information contained in this report is relevant only to the sample/samples supplied to **WATERLAB (Pty) Ltd**. Any further use of the above information is not the responsibility or liability of **WATERLAB (Pty) Ltd**. Except for the full report, parts of this report may not be reproduced without written approval of **WATERLAB (Pty) Ltd**.

CONSOLIDATION TEST RESULTS - BS 1377: Part 5

Project	VEREENIGING PUMP STATION	Date Tested:	30/11/2018
Project No.	2018-B-2286	Laboratory Number:	16
Field Sample Reference	TP 13	Depth (m):	1.2 - 1.4

Test No.	1	
Test Type	Swell	
Remarks	Swell: 1.91%	

Specimen-, Preparation- & Test Conditions

Specimen Type	Undisturbed	
Moulding Dry Density		
Moulding Moisture		
Testing Moisture	Soaked @ 10kPa	

Equipment Detail

Machiene No.	OED18	
Ring	No.	G
	Mass (g)	79.3
	Height (mm)	18.79
	Diameter (mm)	69.96

Specimen Parameters

Stage	Initial	Final (Unloaded)	Initial	Final (Unloaded)
Relative density (S.G.)	2.519			
Moisture Content (%)	24.8	30.0		
Dry Density (kg/m ³)	1227	1537		
Void Ratio, e	1.054	0.639		
Degree of Saturation (%)	59	118		

Test Data

Test 1														
Cycle	No.	1	2	3	4	5	6	7	8	9	10	11		
Total time	min	14109	1394	1429	228	1129	515.3	1544	1246	1467	2809	4186		
Stress	kPa	10	10	51	100	198	398	787	1571	395	100	10		
Strain	%	6.14	4.23	6.35	9.65	13.60	17.81	22.41	29.45	27.96	25.94	20.20		
Void Ratio	e	0.928	0.967	0.923	0.856	0.775	0.688	0.594	0.449	0.480	0.521	0.639		
Mv (1/MPa)		0.000		0.517	0.674	0.402	0.211	0.118	0.090	0.013	0.068	0.638		
t90	min													
Cv	m ² /year													

Test 2														
Cycle	No.													
Total time	min													
Stress	kPa													
Strain	%													
Void Ratio	e													
Mv (1/MPa)														
t90	min													
Cv	m ² /year													

The t90 values reported, if any, which are used to calculate the coefficient of consolidation at different loads are selected by the operator conducting the test and checked by the appropriate technical signatories. They may however not reflect an engineer's interpretation of the time settlement graphs and are by no means final.

CONSOLIDATION TEST RESULTS - BS 1377: Part 5

Project	VEREENIGING PUMP STATION	Date Tested	30/11/2018
Project No.	2018-B-2286	Laboratory Number	16
Field Sample Reference	TP 13	Depth (m)	1.2 - 1.4

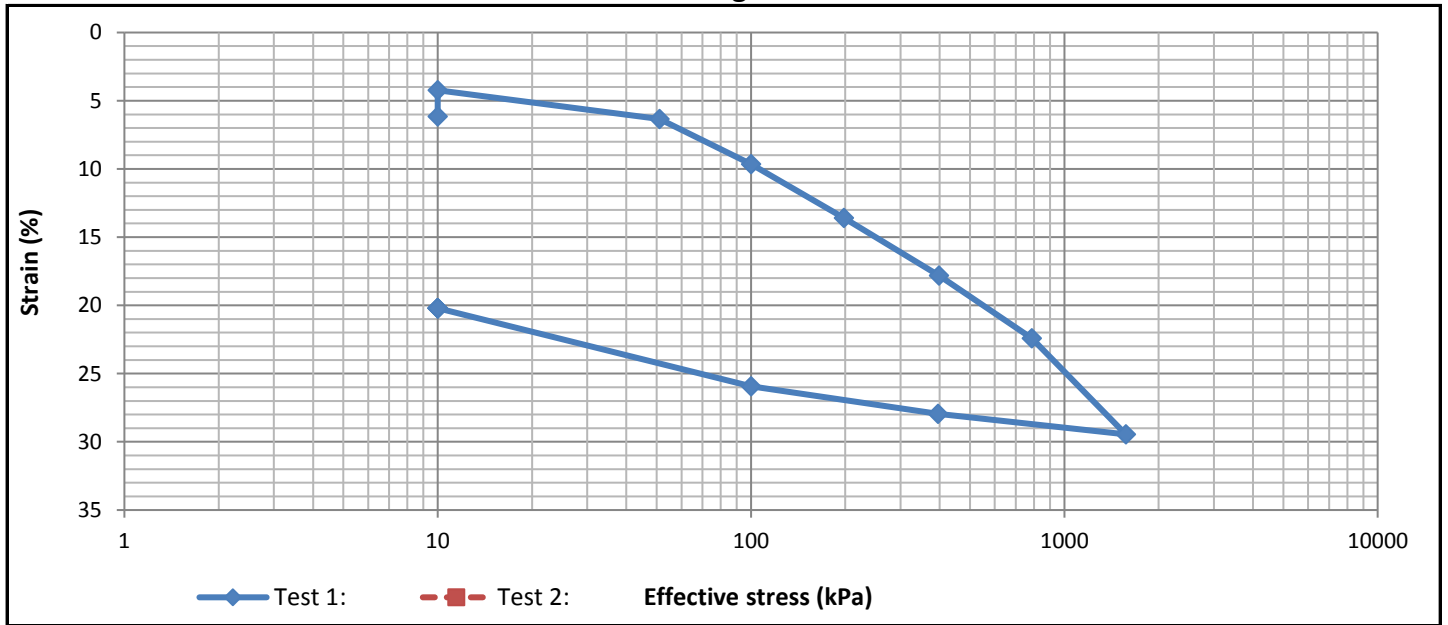
Test 1: Specimen: Undisturbed , Testing Moisture: Soaked @ 10kPa

Cycle	1	2	3	4	5	6	7	8	9	10	11						
Stress (kPa)	10	10	51	100	198	398	787	1571	395	100	10						
Strain (%)	6.14	4.23	6.35	9.65	13.60	17.81	22.41	29.45	27.96	25.94	20.20						
Void Ratio, e	0.928	0.967	0.923	0.856	0.775	0.688	0.594	0.449	0.480	0.521	0.639						

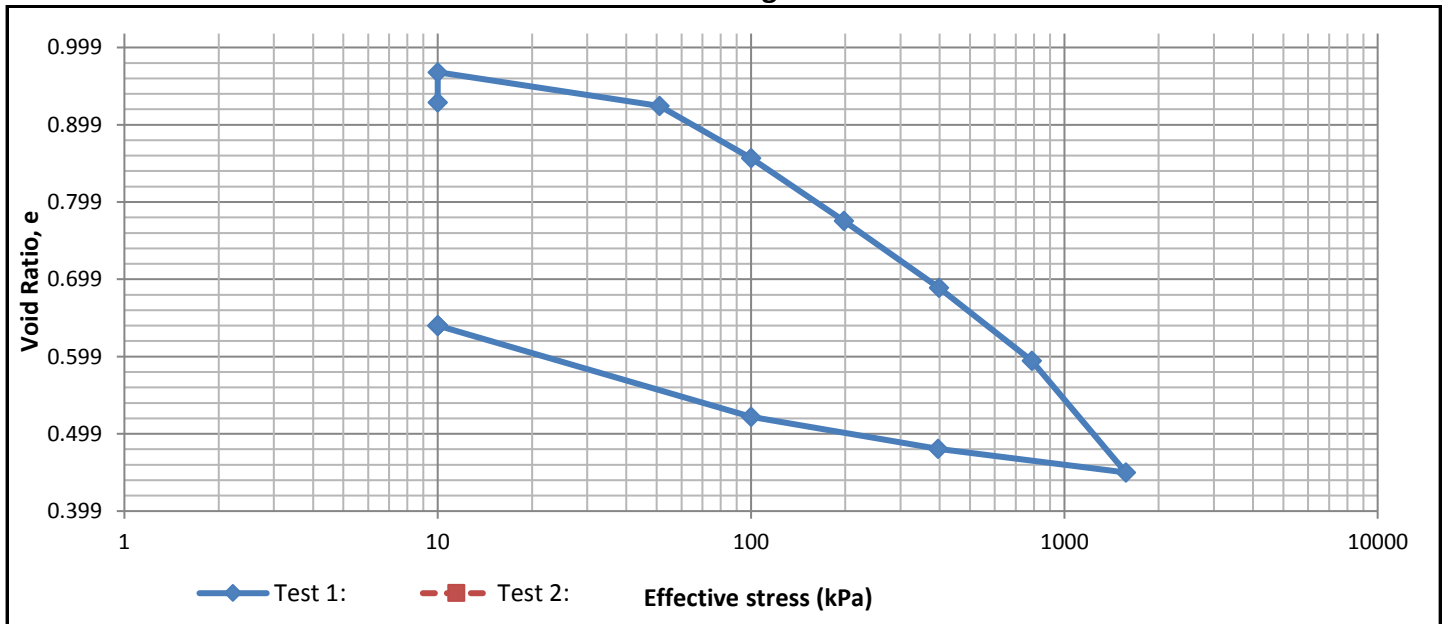
Test 2:

Cycle																	
Stress (kPa)																	
Strain (%)																	
Void Ratio, e																	

Strain Log Stress



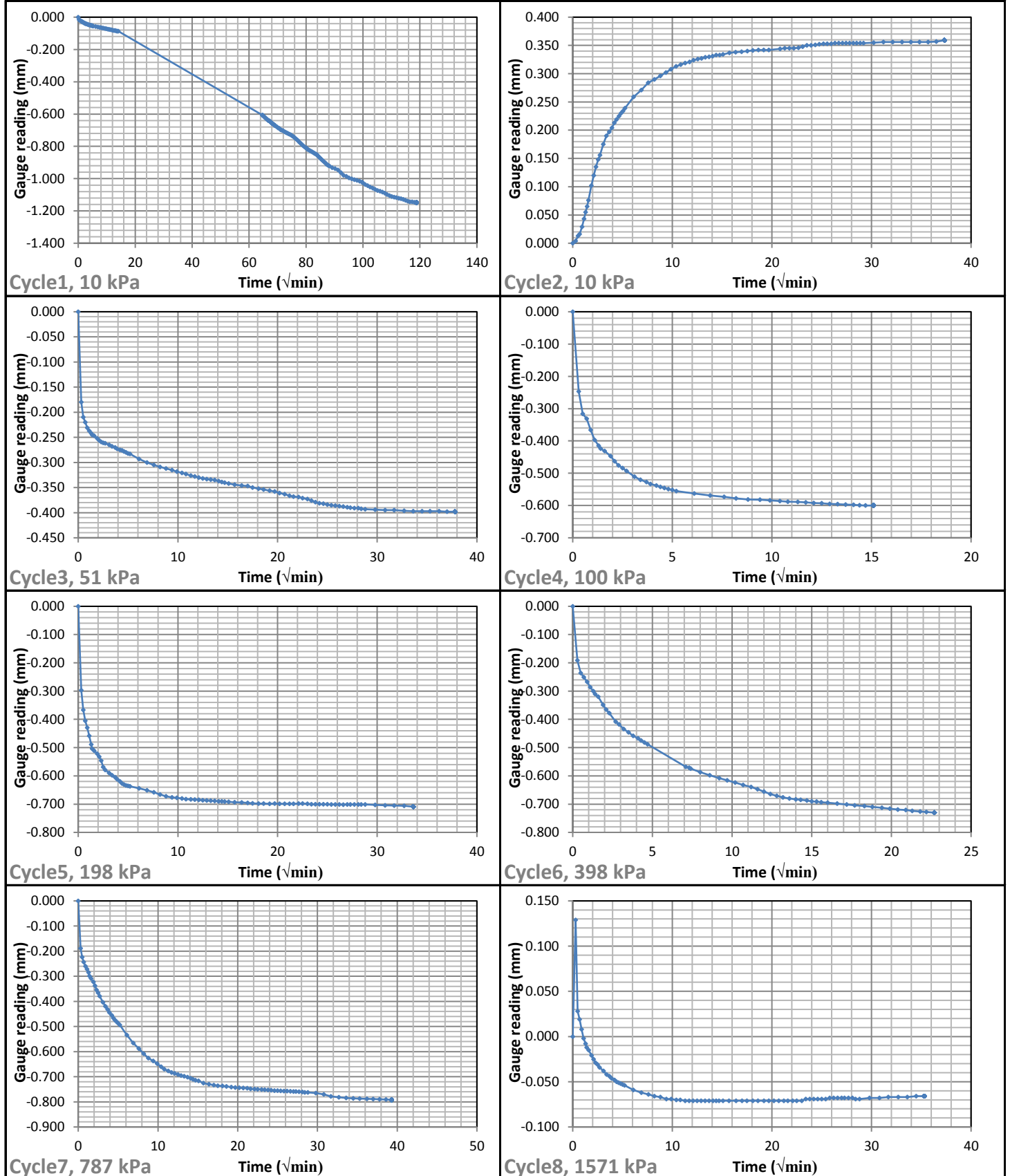
Void Ratio Log Stress



CONSOLIDATION TEST RESULTS - BS 1377: Part 5

Project	VEREENIGING PUMP STATION	Date Tested:	30/11/2018
Project No.	2018-B-2286	Laboratory Number:	16
Field Sample Reference	TP 13	Depth (m):	1.2 - 1.4

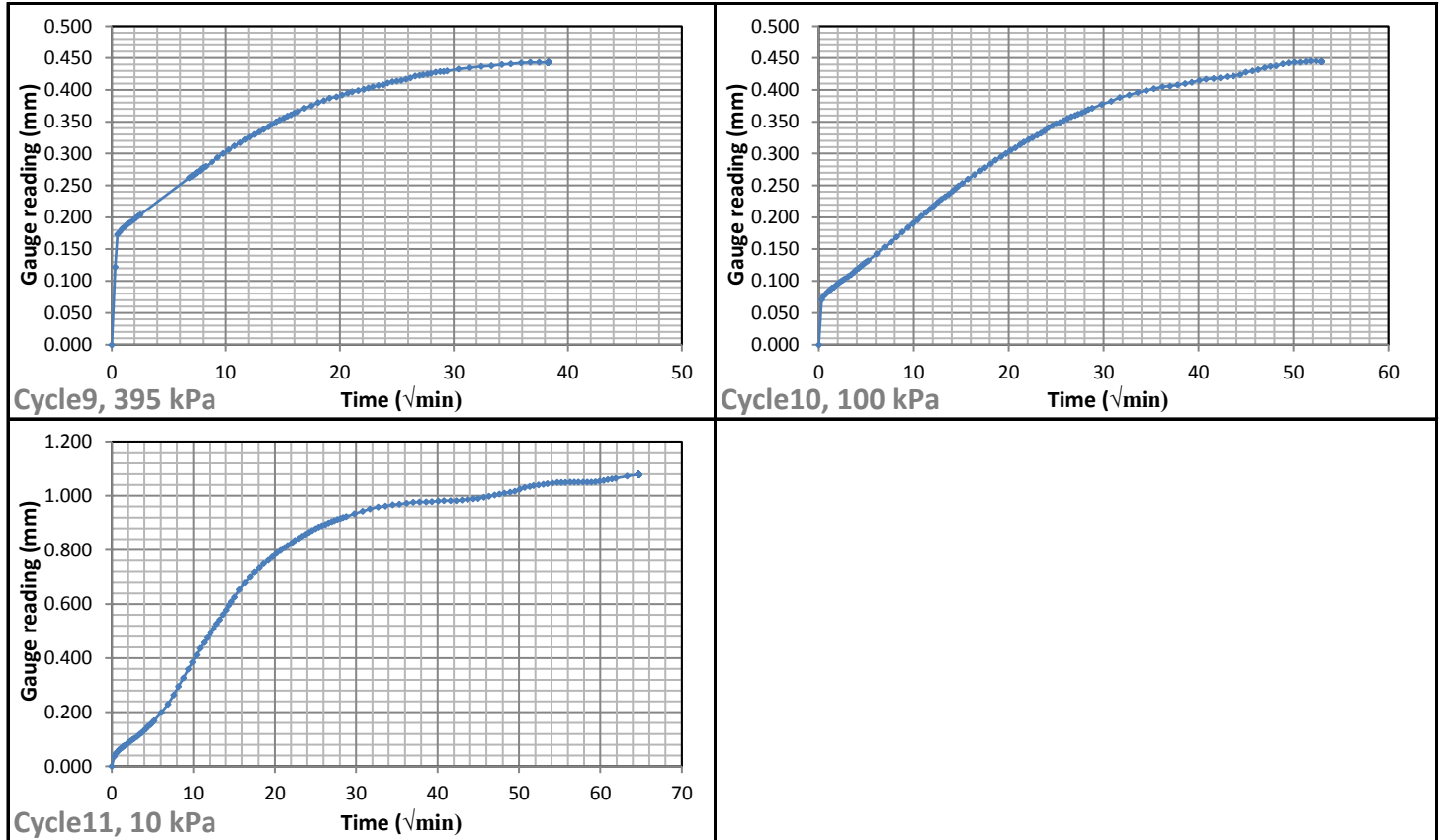
Test 1 - Consolidation vs Square Root Time



CONSOLIDATION TEST RESULTS - BS 1377: Part 5

Project	VEREENIGING PUMP STATION	Date Tested:	30/11/2018
Project No.	2018-B-2286	Laboratory Number:	16
Field Sample Reference	TP 13	Depth (m):	1.2 - 1.4

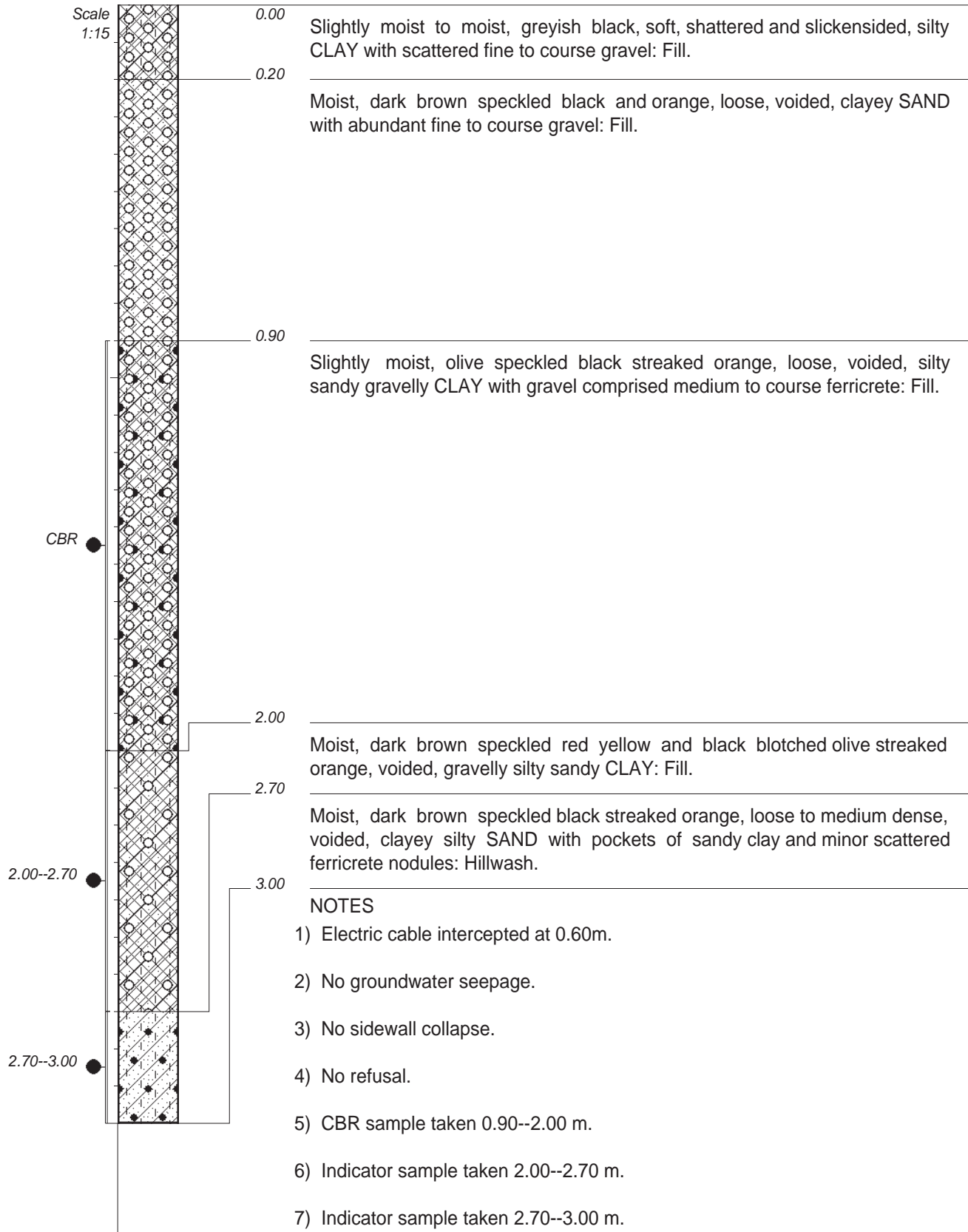
Test 1 - Consolidation vs Square Root Time



RAND WATER
VEREENIGING PUMPING STATION:
GEOTECHNICAL INVESTIGATION
225ML SEDIMENTATION TANK, FLOCCULATOR AND ASSOCIATED SYSTEM 1 PIPELINES

APPENDIX D

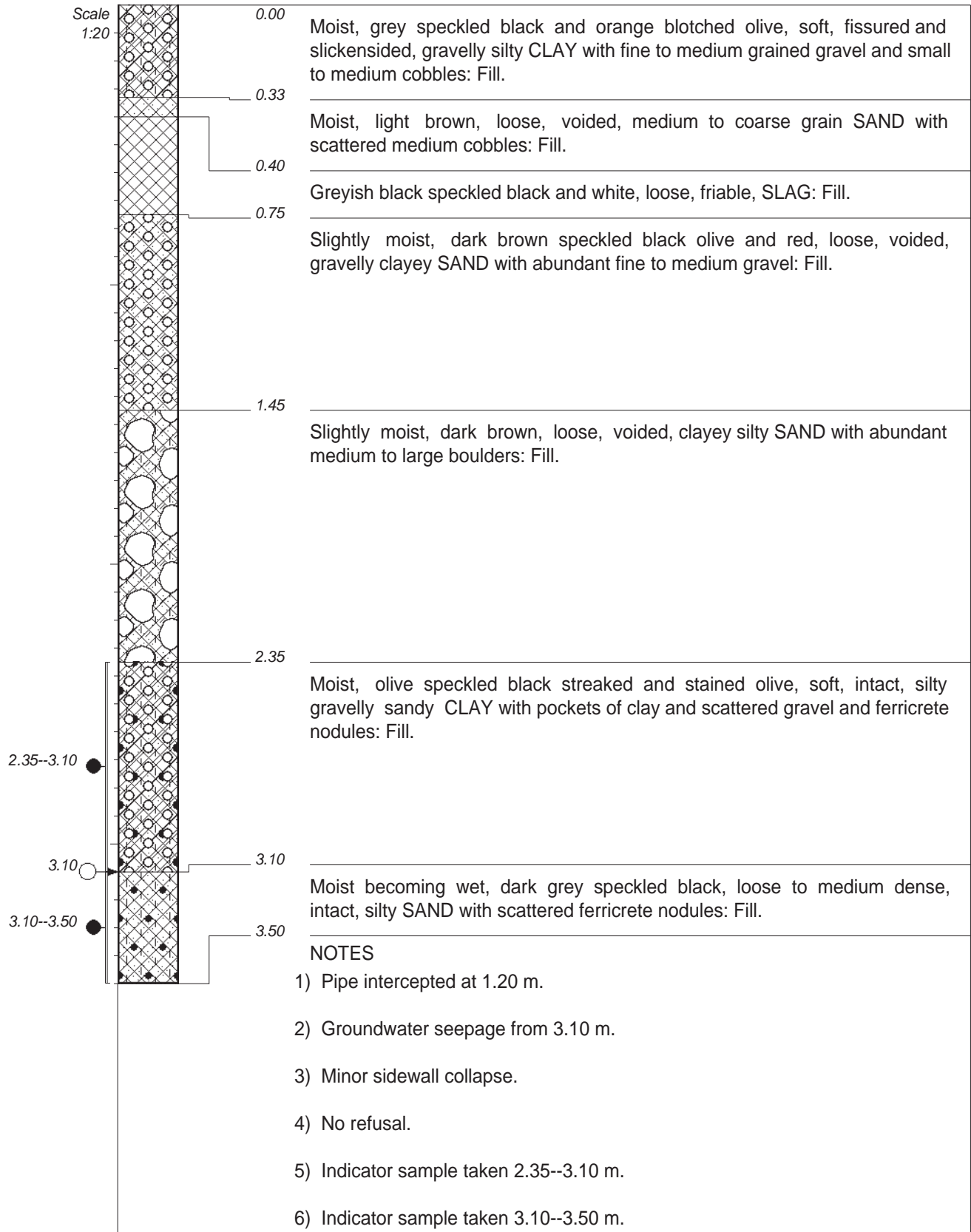
JG AFRIKA TEST PIT AND BOREHOLE LOGS



CONTRACTOR :
MACHINE : BELL
DRILLED BY :
PROFILED BY : S. KULLEN
TYPE SET BY : S. KULLEN
SETUP FILE : TP-JGA-A4.SET

INCLINATION :
DIAM :
DATE :
DATE : 14/07/2016
DATE : 17/11/2016 15:43
TEXT : ..256VEREENIGINGTPLOGS.TXT

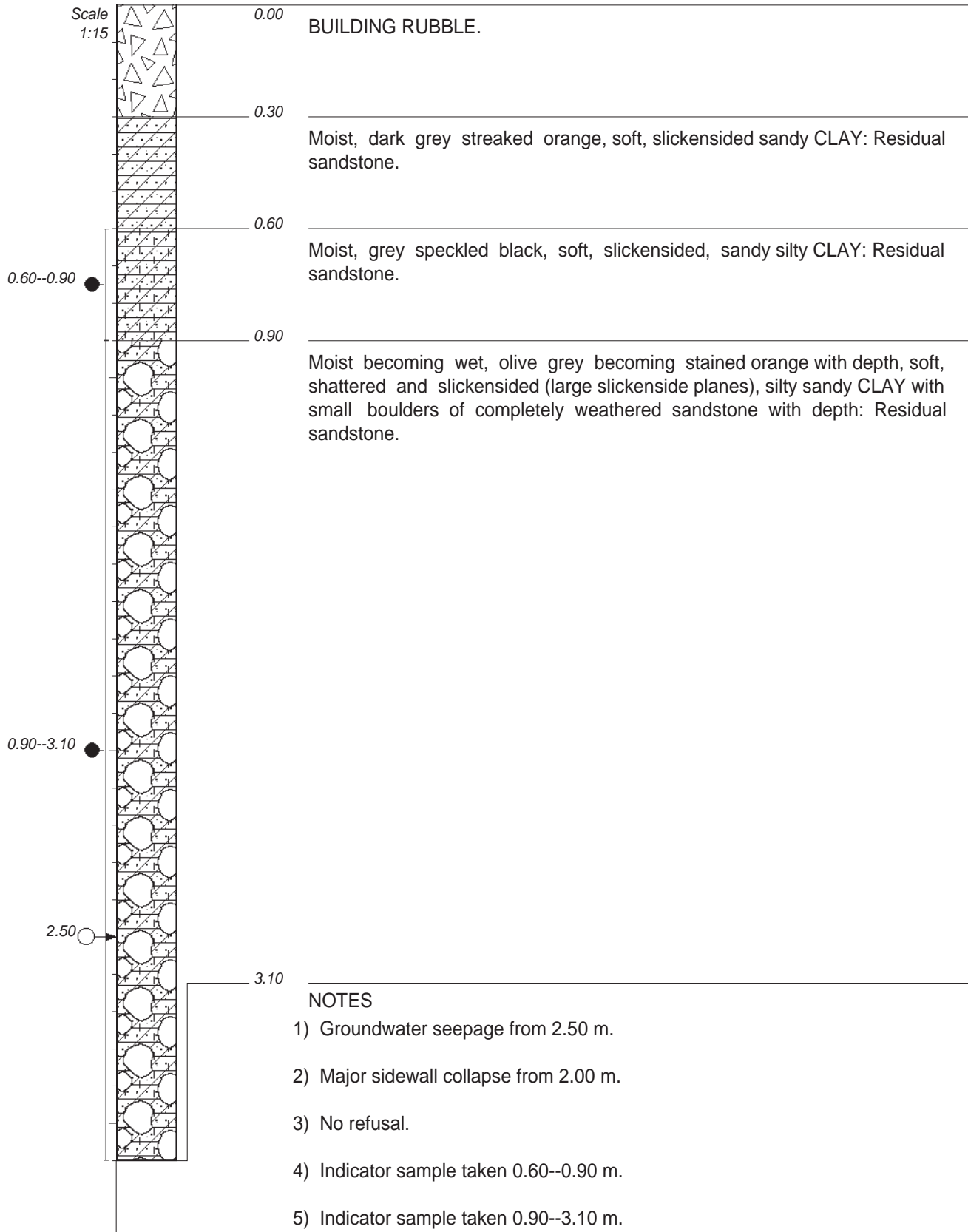
ELEVATION :
X-COORD : 27 55 12.0 E
Y-COORD : 26 41 13.1 S



CONTRACTOR :
MACHINE : BELL
DRILLED BY :
PROFILED BY : S. KULLEN
TYPE SET BY : S. KULLEN
SETUP FILE : TP-JGA-A4.SET

INCLINATION :
DIAM :
DATE :
DATE : 14/07/2016
DATE : 17/11/2016 15:43
TEXT : ..256VEREENIGINGTPLOGS.TXT

ELEVATION :
X-COORD : 27 55 07.1 E
Y-COORD : 26 41 13.9 S



CONTRACTOR :
MACHINE : BELL
DRILLED BY :
PROFILED BY : S. KULLEN
TYPE SET BY : S. KULLEN
SETUP FILE : TP-JGA-A4.SET

INCLINATION :
DIAM :
DATE :
DATE : 14/07/2016
DATE : 17/11/2016 15:43
TEXT : ..256VEREENIGINGTPLOGS.TXT

ELEVATION :
X-COORD : 29 35 27.6 E
Y-COORD : 26 03 34.0 S

HOLE No: BH1
Sheet 2 of 2

JOB NUMBER: 4256

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock



RAND WATER
VEREENIGING SEDIMENTATION & FLOCCULATION PLANT

HOLE No: BH1
Sheet 2 of 2

JOB NUMBER: 4256

%Mater recov	%Core recov	%RQD	SPT	Drilling Method	Frac Frequency	DEPTH Scale 1:50	DESCRIPTION
103	97	21		NWD4		12	"Grey speckled light brown and streaked blackish grey, with occasional light orange brown zones, highly to moderately weathered, fine grained, closely fractured, soft to medium hard rock SILTSTONE. Vryheid Formation. Fractures mostly bedding separation with occasional sub horizontal joints, wide, orange staining and clay infill, smooth planar dipping at 0-10 deg and 45 deg. Highly weathered, very closely fractured, clay zones at 11.41 to 11.5"
67	67	11		NWD4		13	"Slightly pinkish light brown and grey, highly to moderately weathered, fine grained, close to very closely fractured, soft to medium hard rock SILTSTONE. Vryheid Formation. Fractures mostly bedding separation with occasional sub horizontal joints, wide, orange staining and clay infill, smooth planar dipping at 0-10 deg and 55 deg."
37	27			NWD4		14	"Slightly pinkish light brown and grey, highly weathered, fine grained, very closely fractured, soft to medium hard rock SANDSTONE. Vryheid Formation. Fractures mostly bedding separation with occasional sub horizontal joints, wide, orange staining and clay infill, smooth planar dipping at 0-10 deg and 55 deg."
				NWD4		15	"Light orange brown with white and pinkish blotches with dark grey, highly to completely weathered, coarse grained, very closely fractured soft rock TILLITE. Dwyka Group. Fractures, narrow with orange staining, rough planar dipping at 0-10 and 65 deg"
95	91	25		NWD4		16	"Black with occasional light brown and shiny black streaks, moderately weathered, very closely to closely fractured, very soft to soft rock COAL. Vryheid Formation. Fractures, narrow, minor staining, smooth planar, dipping at 0-10 and 45 deg."
100	100	63		NWD4		16.09	"Black moderately weathered, very fine grained with occasional very coarse grains, closely fractured, soft to medium hard rock CARBONACEOUS MUDSTONE. Vryheid Formation. Fractures, narrow, minor staining, smooth planar, dipping at 0-10 and 45 deg."
				NWD4		17	"Dark grey with white and pinkish blotches with dark grey, highly to moderately weathered, coarse grained, very closely fractured soft rock TILLITE. Dwyka Group. Fractures, narrow with orange staining, rough planar dipping at 0-10 and 65 deg."
88	88	54		NWD4		16.65	"Black moderately weathered, very fine grained with occasional very coarse grains, closely fractured, soft to medium hard rock CARBONACEOUS MUDSTONE. Vryheid Formation. Fractures, narrow, minor staining, smooth planar, dipping at 0-10 and 45 deg."
				NWD4		18	"Dark grey, moderately weathered, fine grained, medium fractured, medium hard rock SANDSTONE. Vryheid Formation."
				NWD4		17.60	"Slightly light pinkish grey, slightly weathered, medium grained, medium to widely fractured, medium hard rock SANDSTONE/TILLITE with occasional well rounded inclusion Vryheid Formation. Fractures, narrow, clean, smooth planar, dipping at 0-10 deg"
101	101	90		NWD4		19.04	"Khaki Beige, light greyish brown, slightly to moderately weathered, VERY fine grained, medium fractured, medium hard rock SILTSTONE. Vryheid Formation."
				NWD4		19.20	"Khaki Beige, light greyish brown, slightly to moderately weathered, fine grained, medium fractured, medium hard to hard rock SANDSTONE. Vryheid Formation."
				NWD4		19.50	

- NOTES
- 1) Water table encountered at (pending measurement)
 - 2) Shelby samples retrieved at 1.50--1.90 and 7.5--7.8

CONTRACTOR : GEOMECHANICS	INCLINATION : Vertical	ELEVATION :
MACHINE : YWE - D8	DIAM :	X-COORD : 26deg41'12.9"S
DRILLED BY :	DATE : 16-17/08/2016	Y-COORD : 27deg55'11.20"E
PROFILED BY : KDI	DATE : 15/09/2016	
TYPE SET BY : KDI	DATE : 17/11/2016 15:21	HOLE No: BH1
SETUP FILE : BH-JGA-A3.SET	TEXT : ..56BH4256VPSBH001LOG.TXT	

HOLE No: BH2
Sheet 1 of 2

JOB NUMBER: 4256

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

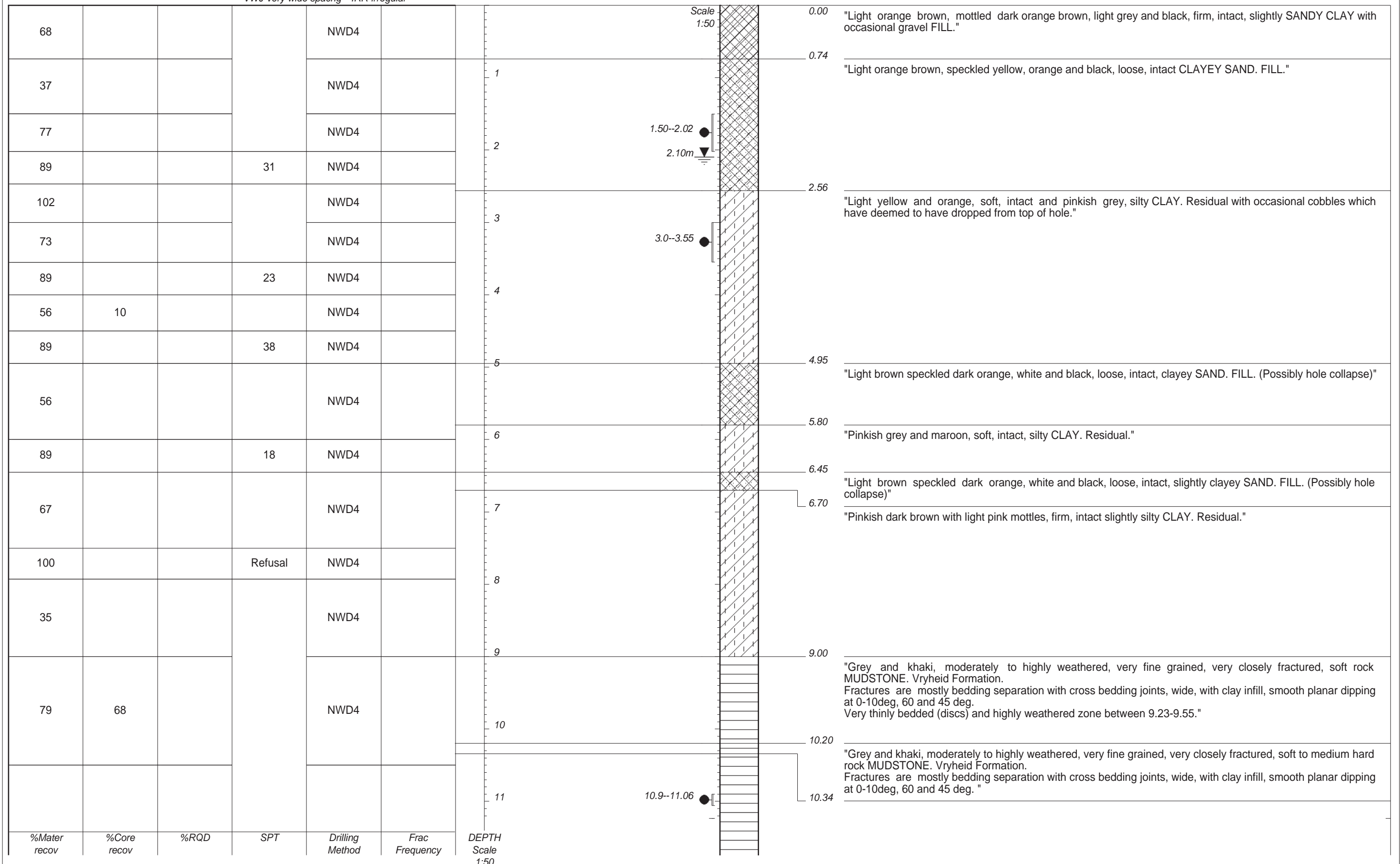
ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock



RAND WATER
VEREENIGING SEDIMENTATION & FLOCCULATION PLANT

HOLE No: BH2
Sheet 1 of 2

JOB NUMBER: 4256



HOLE No: BH2
Sheet 2 of 2

JOB NUMBER: 4256

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacing
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacing

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

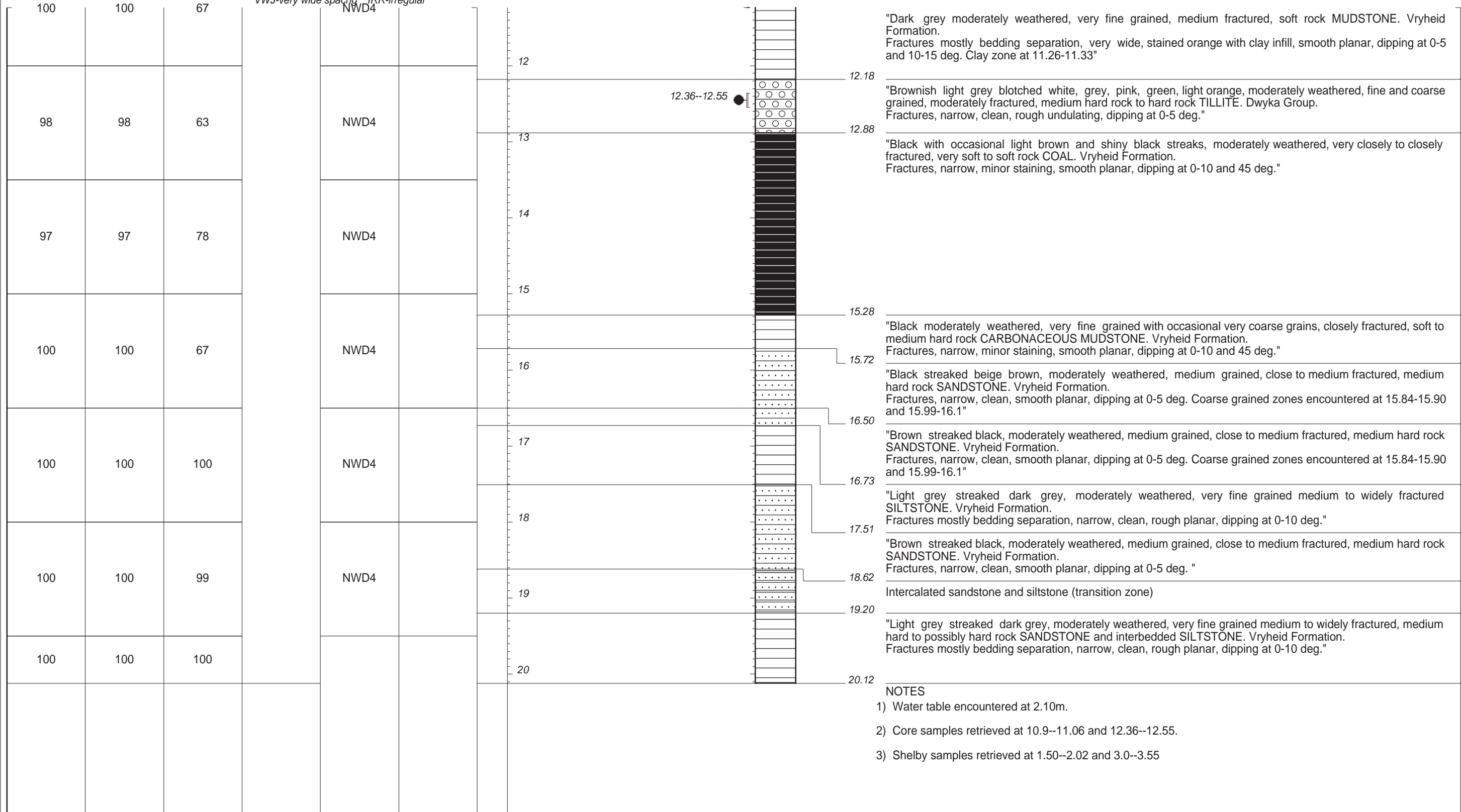
ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock



RAND WATER
VEREENIGING SEDIMENTATION & FLOCCULATION PLANT

HOLE No: BH2
Sheet 2 of 2

JOB NUMBER: 4256



- NOTES
- 1) Water table encountered at 2.10m.
 - 2) Core samples retrieved at 10.9--11.06 and 12.36--12.55.
 - 3) Shelby samples retrieved at 1.50--2.02 and 3.0--3.55

%Mater recov	%Core recov	%RQD	SPT	Drilling Method	Frac Frequency	DEPTH Scale 1:50	CONTRACTOR : GEOMECHANICS MACHINE : YWE - D8 DRILLED BY : PROFILED BY : KDI TYPE SET BY : KDI SETUP FILE : BH-JGA-A3.SET	INCLINATION : Vertical DIAM : DATE : 20-21/07/2016 DATE : 15/09/2016 DATE : 17/11/2016 15:22 TEXT : ..56BH4256VPSBH002LOG.TXT	ELEVATION : X-COORD : 26deg 41'14.50"S Y-COORD : 27deg 55'12.20"E
--------------	-------------	------	-----	-----------------	----------------	------------------	---	--	---

HOLE No: BH2

HOLE No: BH3
Sheet 1 of 2

JOB NUMBER: 4256

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

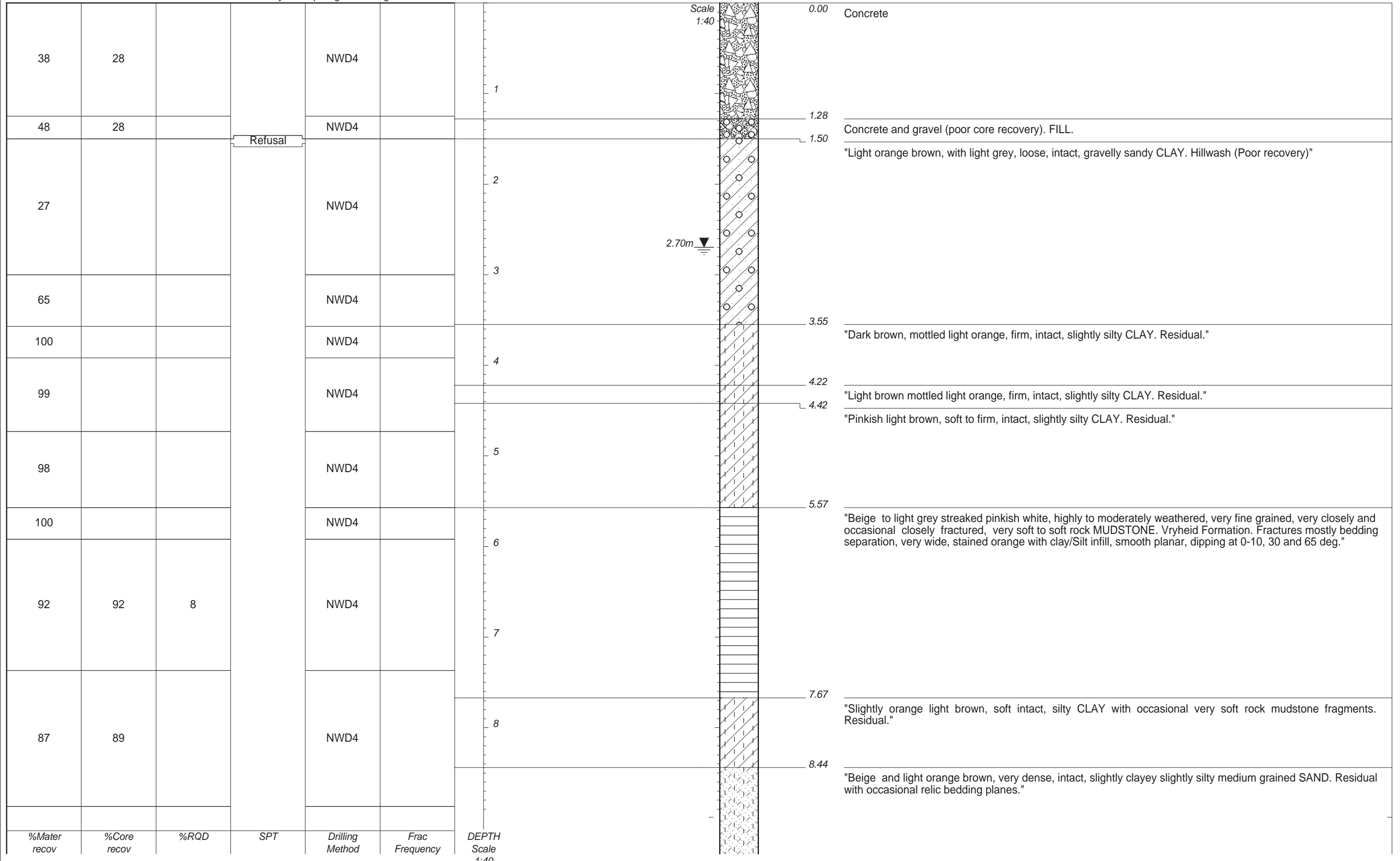
ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock



RAND WATER
VEREENIGING SEDIMENTATION & FLOCCULATION PLANT

HOLE No: BH3
Sheet 1 of 2

JOB NUMBER: 4256



HOLE No: BH3
Sheet 2 of 2

JOB NUMBER: 4256

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock



RAND WATER
VEREENIGING SEDIMENTATION & FLOCCULATION PLANT

HOLE No: BH3
Sheet 2 of 2

JOB NUMBER: 4256

%Mater recov	%Core recov	%RQD	SPT	Drilling Method	Frac Frequency	DEPTH Scale 1:40	DESCRIPTION
29	5			NWD4		9	
92	92	69		NWD4		10.35 - 10.60	"Black, soft, intact, CLAY. Residual."
						10.60 - 10.81	"Black, moderately weathered, very fine to fine grained, closely fractured, soft rock CARBONACEOUS MUDSTONE. Vryheid Formation. Fractures, narrow, minor silt infill, rough undulating, dipping at 30deg."
						10.81 - 11.19	"Light beige grey matrix with light grey, dark grey, pink and orange and whitish clast, medium grained, moderately to highly weathered, soft to medium hard rock TILLITE. Dwyka Group. Fractures, narrow, slightly stained, smooth planar dipping at 15 deg."
						11.19 - 11.26	"Black, soft, intact, CLAY. Residual."
100	100	100		NWD4		11.26 - 11.46	"Black, moderately weathered, very firm to fine grained, closely fractured, soft rock CARBONACEOUS MUDSTONE. Vryheid Formation. Fractures, narrow, minor silt infill, rough undulating, dipping at 30deg."
						11.46 - 12.16	"Beige streaked dark brown and dark brown streaked beige, moderately to highly weathered, medium grained to coarse grained, medium fractured, soft to medium hard rock SANDSTONE. Vryheid Formation. Fractures mostly bedding separation, narrow, minor staining, rough planar, dipping at 10 deg."
						12.16 - 12.63	"Beige and greyish brown with occasional black streaks, moderately weathered, very fine grained, medium fractured, medium hard to hard rock intercalated SILTSTONE/ MUDSTONE. Vryheid Formation. Fractures mostly bedding separation, narrow, minor staining, rough planar, dipping at 10 deg."
100	100	95		NWD4		12.63 - 13.41	"Beige streaked black, moderately weathered, fine grained, medium fractured, soft to medium hard rock SANDSTONE. Vryheid Formation. Fractures mostly bedding separation, narrow, minor staining, rough planar, dipping at 10 deg."
						13.41 - 15.12	"Beige streaked black, moderately weathered, very fine grained, medium fractured, soft to medium hard rock SILTSTONE with intercalated fine grained SANDSTONE. Vryheid Formation. Fractures mostly bedding separation, narrow, minor staining, rough planar, dipping at 10 deg. A highly weathered, very closely fractured zone at 14.93-15.12"
100	78	63		NWD4		15.12 - 15.22	"grey, moderately weathered, very fine grained, medium fractured, soft rock MUDSTONE. Vryheid Formation. Fractures mostly bedding separation, narrow, minor staining, rough planar, dipping at 10 deg. "
92	85	57		NWD4		15.22 - 16.42	"Light grey matrix with green, pink, dark grey white and khaki clasts, moderately weathered, coarse grained, medium fractured, medium hard rock to hard rock TILLITE. Fractures, narrow, minor staining, rough planar, dipping at 10 deg. "
							NOTES 1) water table encountered at 2.70m. 2) No Shelby samples retrieved. 3) No core samples retrieved.

CONTRACTOR : GEOMECHANICS		INCLINATION : Vertical		ELEVATION :	
MACHINE : YWE - D8		DIAM :		X-COORD : 26deg 41'14.02"S	
DRILLED BY :		DATE : 22-26/07/2016		Y-COORD : 27deg 55'09.8"E	
PROFILED BY : KDI		DATE : 15/09/2016			
TYPE SET BY : KDI		DATE : 17/11/2016 15:23			
SETUP FILE : BH-JGA-A3.SET		TEXT : ..56BH4256VPSBH003LOG.TXT			

HOLE No: BH3

HOLE No: BH4
Sheet 1 of 2

JOB NUMBER: 4256

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock



RAND WATER
VEREENIGING SEDIMENTATION & FLOCCULATION PLANT

HOLE No: BH4
Sheet 1 of 2

JOB NUMBER: 4256

%Mater recov	%Core recov	%RQD	SPT	Drilling Method	Frac Frequency	DEPTH Scale 1:50	DESCRIPTION
						0.00	"Dark brown,firm, intact, slightly gravelly sandy SILT. Fill/Colluvium."
						0.08	CONCRETE. (Small aggregate) FILL.
						0.32	"Mottled orange black and dark orange, dense, intact, slightly clayey slightly gravelly SAND. FILL."
42				NWD4		1.28	
32				NWD4		1.50	"Dark grey, loose, intact, GRAVEL. (Aggregate) FILL."
26				NWD4		1.85	"Mottled orange black and dark orange, dense, intact, slightly clayey slightly gravelly SAND. FILL."
62				NWD4		2.28	"Dark grey, loose, intact, GRAVEL. (Aggregate) FILL."
23				NWD4		3.67	
33	29			NWD4		5.00	"Light pink, highly weathered, medium fractured, medium to coarse grained, very soft rock SANDSTONE. Vryheid Formation. Fractures, narrow to wide, stained orange with clay infill, rough planar, dipping at 5-10deg and 15-20deg."
97	97	8		NWD4		5.58	"Light pink and light orange brown, highly weathered, medium fractured, medium to coarse grained, soft rock SANDSTONE. Vryheid Formation. Fractures, narrow, stained orange with clay infill, rough planar, dipping at 5-10deg and 15-20deg."
91				NWD4		6.57-6.90	"Dark brown mottled orange with maroon zones, very stiff, slickensided CLAY. Residual."
100			54	NWD4			
36	36			NWD4			
100	54	39		NWD4		8.86	"Light beige grey stained black and orange, highly to moderately weathered, very fine grained, close to moderately fractured, very soft to soft rock MUDSTONE. Vryheid Formation. Fractures mostly bedding separation, narrow to wide, stained black and orange with clay infill, smooth planar, dipping at 20 deg and 0-10 deg."
97	95	41		NWD4		9.81	"Light beige with pinkish grey , moderately to highly weathered, very fine grained, closely fractured very soft rock MUDSTONE. Vryheid Formation. Fractures mostly bedding separation, wide, clay infill with orange staining, smooth planar dipping at 0-10 and 20 deg."
						11.10	

HOLE No: BH4
Sheet 2 of 2

JOB NUMBER: 4256

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock



RAND WATER
VEREENIGING SEDIMENTATION & FLOCCULATION PLANT

HOLE No: BH4
Sheet 2 of 2

JOB NUMBER: 4256

%Mater recov	%Core recov	%RQD	SPT	Drilling Method	Frac Frequency	DEPTH Scale 1:50	DESCRIPTION
87	87	55		NWD4		11.71	"Grey, highly weathered, closely fractured, very fine grained, very soft rock MUDSTONE. Vryheid Formation. Fractures, narrow to wide, clay infill, rough undulating, dipping at 20deg and 0-10deg."
						12.00	"Light orange brown blotched grey and dark orange white, beige, moderately weathered, moderately fractured, hard rock TILLITE.Dwyka Group. Fractures, narrow, stained orange with minor silt infill, rough undulating dipping at 0-10 deg. Highly weathered mudstone at 11.88-11.96"
100	63	7		NWD4		12.20	"Dark marron and dark red, closely fractured, very fine grained, very soft rock CARBONACOUES MUDSTONE. Vryheid Formation."
						13.87	"Black, highly weathered, very fine grained, close to very closely fractured, very soft rock COAL. Vryheid Formation. Fractures are mostly bedding separation, narrow, clean, smoot planar, dipping at 0-10deg, occasional vertical joints."
100	91	51		NWD4		14.48	"Black, highly weathered, very fine grained, closely fractured, very soft rock CARBONACEOUS MUDSTONE. Vryheid Formation. Fractures are mostly bedding separation, narrow, clean, smooth planar, dipping at 0-10deg, occasional vertical joints."
						14.58	"Light orange brown blotched grey and dark orange white, beige, moderately weathered, moderately fractured, hard rock SANDSTONE. Vryheid Formation. Fractures, narrow, stained orange with minor silt infill, rough undulating dipping at 0-10 deg."
100	102	100		NWD4		14.72	"Black, highly weathered, very fine grained, closely fractured, very soft rock CARBONACEOUS MUDSTONE. Vryheid Formation. Fractures are mostly bedding separation, narrow, clean, smooth planar, dipping at 0-10deg, occasional vertical joints."
						15.14	"Dark grey and light beige grey, moderately weathered, coarse grained, medium fractured, medium hard to hard rock SANDSTONE/CONGLOMERATE. Vryheid Formation. "
						15.62	"Dark grey to black, moderately to slightly weathered, very fine to fine grained, widely fractured, soft rock SILTSTONE. Vryheid Formation. Fractures, narrow, clean, smooth planar, dipping at 80 and 0-10deg."
100	100	100		NWD4		15.92	"Khaki streaked black moderately weathered, medium grained, widely fractured, soft rock SANDSTONE. Vryheid Formation. Fractures, narrow, clean, smooth planar, dipping at 80 and 0-10deg."
						15.92	"Khaki grey, moderately weathered, medium grained, widely fractured, medium hard rock SANDSTONE. Vryheid Formation. Fractures, narrow, clean, rough undulating, dipping at 80 and 0-10deg."
						18.31	"Cream to light grey, moderately to highly weathered, very fine grained, very closely fractured, medium hard rock with minor soft rock zones SILTSTONE. Vryheid Formation. Fractures, narrow, clean, rough undulating, dipping at 80 and 0-10deg."
100	100	90		NWD4		18.82	"Light grey streaked black and dark grey, blotched and speckled khaki and light pink, coarse and fine grained, widely fractured, medium hard rock to hard rock TILLITE. Dwyka Formation. Fractures, narrow, clean, rough undulating, dipping at 80 and 0-10deg."
						19.74	NOTES 1) water table encountered at 0.90m. 2) Core samples retrieved at 15.91--16.41. 3) Shelby samples retrieved at 6.57-6.90

CONTRACTOR : GEOMECHANICS		INCLINATION : Vertical		ELEVATION :	
MACHINE : YWE - D8		DIAM :		X-COORD : 26deg 41'15.00"S	
DRILLED BY :		DATE : 27-28/07/2016		Y-COORD : 27deg 55'10.10"E	
PROFILED BY : KDI		DATE : 15/09/2016		HOLE No: BH4	
TYPE SET BY : KDI		DATE : 17/11/2016 15:24			
SETUP FILE : BH-JGA-A3.SET		TEXT : ..56BH4256VPSBH004LOG.TXT			

HOLE No: BH5
Sheet 1 of 1

JOB NUMBER: 4256

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock

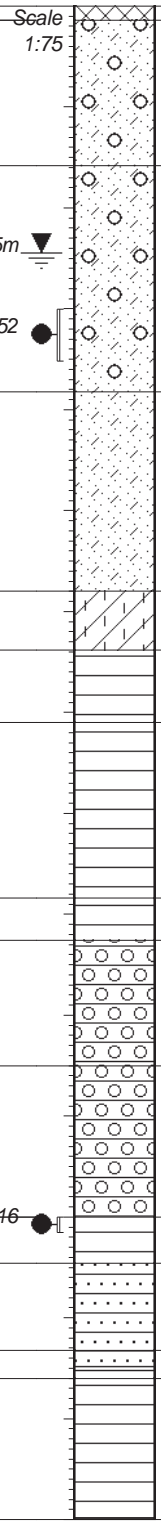


RAND WATER
VEREENIGING SEDIMENTATION & FLOCCULATION PLANT

HOLE No: BH5
Sheet 1 of 1

JOB NUMBER: 4256

DEPTH (m)	ROCK FABRIC	GRAIN SIZE	JOINT SPACING	JOINT ROUGHNESS	JOINT SHAPE	ROCK HARDNESS	DESCRIPTION
0.00 - 0.14							Grey gravel and Boulders. FILL.
0.14 - 1.58							"Dark brown, loose, intact, GRAVELLY CLAYEY SAND. Colluvium/Fill."
1.58 - 3.82							"Mottled dark grey, light orange, light grey, dark orange and black, very dense, intact, slightly clayey gravelly fine SAND. Fill."
3.82 - 5.80							"Orangish brown, mottled occasionally black and dark grey, loose to medium dense, intact, slightly clayey SAND. Residual."
5.80 - 6.38							"Mottled light pink, light orange beige and dark grey, soft, intact, SILTY CLAY. Residual."
6.38 - 7.10							"Cream and light pink, highly weathered, very fine grained, closely fractured, very soft rock MUDSTONE. Vryheid Formation. Fractures mostly bedding separation, wide to very wide, stained orange with clay infill, smooth planar, dipping at 0-10 deg."
7.10 - 8.84							"Grey streaked light pink, moderately to highly weathered, very fine grained, closely fractured, soft rock MUDSTONE. Vryheid Formation. Fractures mostly bedding separation, wide, stained orange with clay infill, smooth planar, dipping at 0-10 deg with occasional 80 deg."
8.84 - 9.26							"Cream and light pink, highly weathered, very fine grained, closely fractured, very soft rock MUDSTONE. Vryheid Formation. Fractures mostly bedding separation, wide to very wide, stained orange with clay infill, smooth planar, dipping at 0-10 deg."
9.26 - 10.50							"Pink and light orange brown, blotched cream, light grey and orange, highly weathered, widely fractured, soft rock TILLITE. Vryheid Formation. Fractures, narrow, with silt infill, rough undulating, dipping at 0-10 deg."
10.50 - 12.00							"Light grey and beige, highly weathered, fine grained, widely fractured, very soft rock to soft hard rock TILLITE. Vryheid Formation. Fractures, wide, clay infill, dipping at 70 and 0-10deg."
12.00 - 12.46							"Light khaki grey streaked black and dark grey, medium to slightly weathered, very fine grained, widely fractured, soft to medium hard rock SILTSTONE. Vryheid Formation. Fractures occur as bedding separations, narrow, clay infill stained orange, rough planar, dipping at 0-10 deg."
12.46 - 13.32							"Light khaki grey streaked black and dark grey, medium to slightly weathered, fine grained, widely fractured, medium hard rock SANDSTONE. Vryheid Formation. Fractures occur as bedding separations, narrow, clean, rough planar, dipping at 0-10 deg."
13.32 - 13.60							Transition zone between sandstone and siltstone -INTERCALATED SANDSTONE and SILTSTONE.
13.60 - 15.00							"Light grey with occasional dark grey streaks, moderately weathered, fine grained, widely fractured, soft to medium hard rock SILTSTONE. Vryheid Formation. Fractures occur as bedding separations, narrow, clean, rough planar, dipping at 0-10 deg."



%Mater recov	%Core recov	%RQD	SPT	Drilling Method	Frac Frequency
				NWD4	
				NWD4	
				NWD4	
			31	NWD4	
				NWD4	
			37	NWD4	
				NWD4	
			Refusal	NWD4	
	53			NWD4	
	100	43		NWD4	
				NWD4	
	82	55		NWD4	
				NWD4	
				NWD4	
	102	102		NWD4	
				NWD4	
	96	95		NWD4	

DEPTH Scale 1:75

CONTRACTOR : GEOMECHANICS
MACHINE : YWE - D8
DRILLED BY :
PROFILED BY : KDI
TYPE SET BY : KDI
SETUP FILE : BH-JGA-A3.SET

INCLINATION : Vertical
DIAM :
DATE : 28-29/07/2016
DATE : 15/09/2016
DATE : 17/11/2016 15:24
TEXT : ..56BH4256VPSBH005LOG.TXT

ELEVATION :
X-COORD : 26deg 41'15.2"S
Y-COORD : 27deg 55'07.5"E

HOLE No: BH5

HOLE No: BH6
Sheet 1 of 1

JOB NUMBER: 4256

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

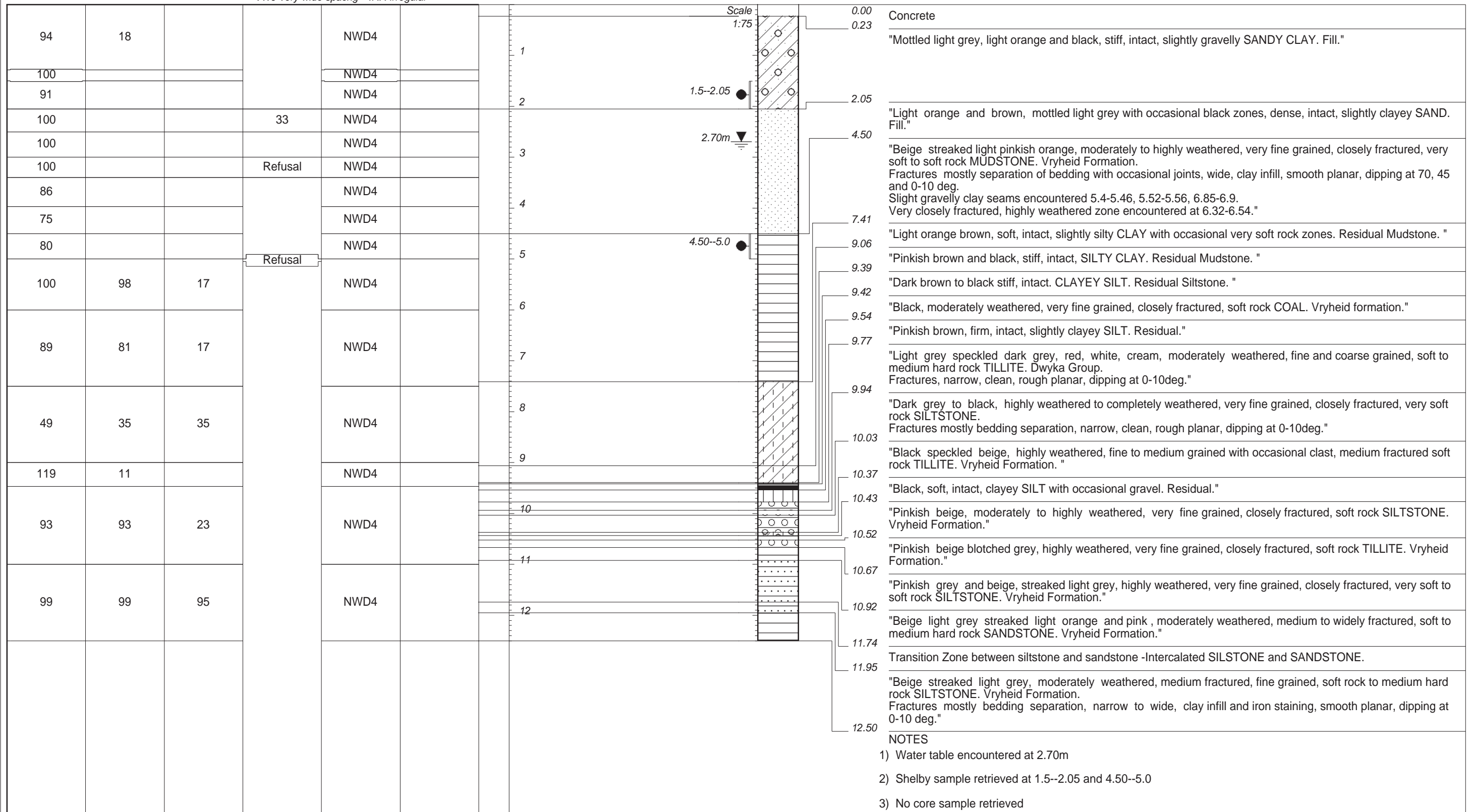
ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock



RAND WATER
VEREENIGING SEDIMENTATION & FLOCCULATION PLANT

HOLE No: BH6
Sheet 1 of 1

JOB NUMBER: 4256



%Mater recov	%Core recov	%RQD	SPT	Drilling Method	Frac Frequency	DEPTH Scale 1:75	CONTRACTOR : GEOMECHANICS MACHINE : YWE - D8 DRILLED BY : PROFILED BY : KDI TYPE SET BY : KDI SETUP FILE : BH-JGA-A3.SET	INCLINATION : Vertical DIAM : DATE : 8-10/08/2016 DATE : 15/09/2016 DATE : 17/11/2016 15:25 TEXT : ..56BH4256VPSBH006LOG.TXT	ELEVATION : X-COORD : 26deg 41'15.4"S Y-COORD : 27deg 55'5.8"E
									HOLE No: BH6

HOLE No: BH7
Sheet 1 of 2

JOB NUMBER: 4256

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

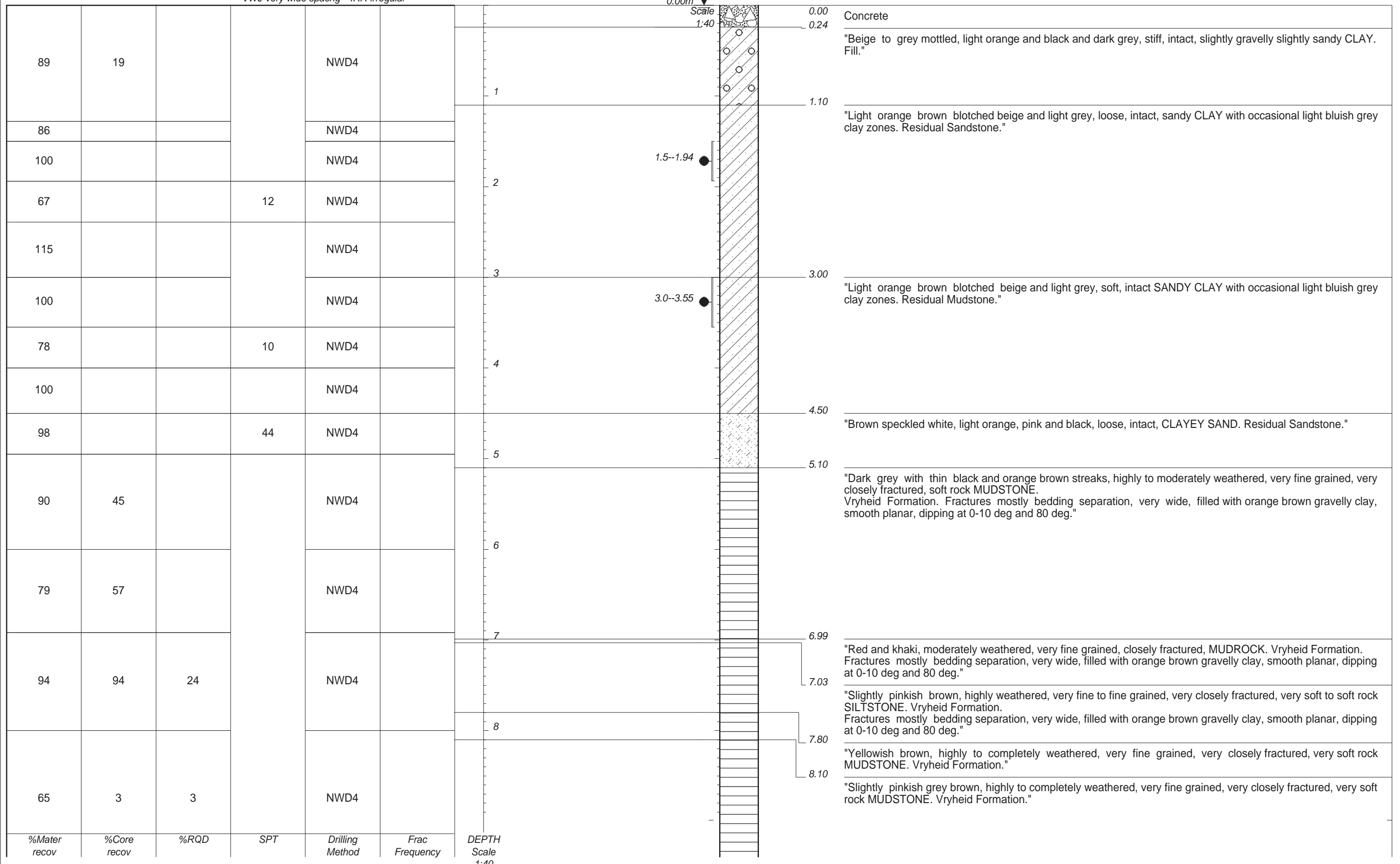
ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock



RAND WATER
VEREENIGING SEDIMENTATION AND FLOCCULATION PLANT

HOLE No: BH7
Sheet 1 of 2

JOB NUMBER: 4256



%Mater recov	%Core recov	%RQD	SPT	Drilling Method	Frac Frequency	DEPTH Scale 1:40
89	19			NWD4		1
86				NWD4		
100				NWD4		2
67			12	NWD4		
115				NWD4		3
100				NWD4		
78			10	NWD4		4
100				NWD4		
98			44	NWD4		5
90	45			NWD4		6
79	57			NWD4		
94	94	24		NWD4		7
65	3	3		NWD4		8

HOLE No: BH7
Sheet 2 of 2

JOB NUMBER: 4256

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock



RAND WATER
VEREENIGING SEDIMENTATION AND FLOCCULATION PLANT

HOLE No: BH7
Sheet 2 of 2

JOB NUMBER: 4256

%Mater recov	%Core recov	%RQD	SPT	Drilling Method	Frac Frequency	DEPTH Scale 1:40	DESCRIPTION
113	113	23		NWD4		9.37 - 9.60	"Yellowish beige, highly weathered fine to medium grained, closely fractured, soft rock SANDSTONE. Vryheid Formation."
						9.60 - 9.86	"Blackish dark brown with occasional light pinkish specks, soft, intact, slightly silty CLAY . Residual."
						9.86 - 10.05	"Blackish dark brown with occasional light pinkish specks, soft, intact, silty CLAY with occasional rock fragments. Residual."
99	99	64		NWD4		10.05 - 10.39	"Black, moderately to highly weathered, fine grained, closely fractured, very soft to soft rock CARBONACEOUS MUDSTONE. Vryheid Formation. Fractures mostly bedding separation, narrow, no infill, smooth planar, dipping at 0-10 deg."
						10.39 - 10.50	"Black streaked dark grey, highly to moderately weathered, fine grained, medium fractured, fine grained, soft rock SILTSTONE. Vryheid Formation."
						10.50 - 10.96	"Light grey blotched dark grey, highly to moderately weathered, medium grained, close to moderately fractured, soft to medium hard rock TILLITE. Vryheid Formation."
						10.96 - 11.23	"Black, moderately to highly weathered, fine grained, closely fractured, very soft to soft rock CARBONACEOUS MUDSTONE. Vryheid Formation. Fractures mostly bedding separation, narrow, no infill, smooth planar, dipping at 0-10 deg."
98	98	91		NWD4		11.23 - 11.55	"Black streaked dark grey, highly to moderately weathered, fine grained, medium fractured, fine grained, soft rock SILTSTONE. Vryheid Formation."
						11.55 - 11.63	"Black, moderately to highly weathered, fine grained, closely fractured, very soft to soft rock CARBONACEOUS MUDSTONE. Vryheid Formation. Fractures mostly bedding separation, narrow, no infill, smooth planar, dipping at 0-10 deg."
						11.63 - 11.74	"Black streaked dark grey, highly to moderately weathered, fine grained, medium fractured, fine grained, soft rock SILTSTONE. Vryheid Formation."
						11.74 - 12.41	"Light khaki grey, moderately weathered, fine grained, moderately to widely fractured, soft rock SANDSTONE. Vryheid Formation, Fractures mostly bedding separation, very narrow, clean, smooth planar, dipping at 0-10deg."
						12.41 - 13.50	"Light khaki grey, moderately weathered, very fine to fine grained, moderately to widely fractured, soft rock to medium hard rock SILTSTONE with intercalated sandstone. Vryheid Formation, Fractures mostly bedding separation, very narrow, clean, smooth planar, dipping at 0-10deg."

- NOTES
- 1) Water table encountered at 0.00m
 - 2) Shelby sample retrieved at 1.5--1.94 and 3.0--3.55
 - 3) No Core sample retrieved.

CONTRACTOR : GEOMECHANICS	INCLINATION : Vertical	ELEVATION :
MACHINE : YWE - D8	DIAM :	X-COORD : 26deg 41'15.3"S
DRILLED BY :	DATE : 10-11/08/2016	Y-COORD : 27deg 55'04.9"E
PROFILED BY : KDI	DATE : 15/09/2016	
TYPE SET BY : KDI	DATE : 17/11/2016 15:26	HOLE No: BH7
SETUP FILE : BH-JGA-A3.SET	TEXT : ..56BH4256VPSBH007LOG.TXT	

HOLE No: BH8
Sheet 1 of 2

JOB NUMBER: 4256

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

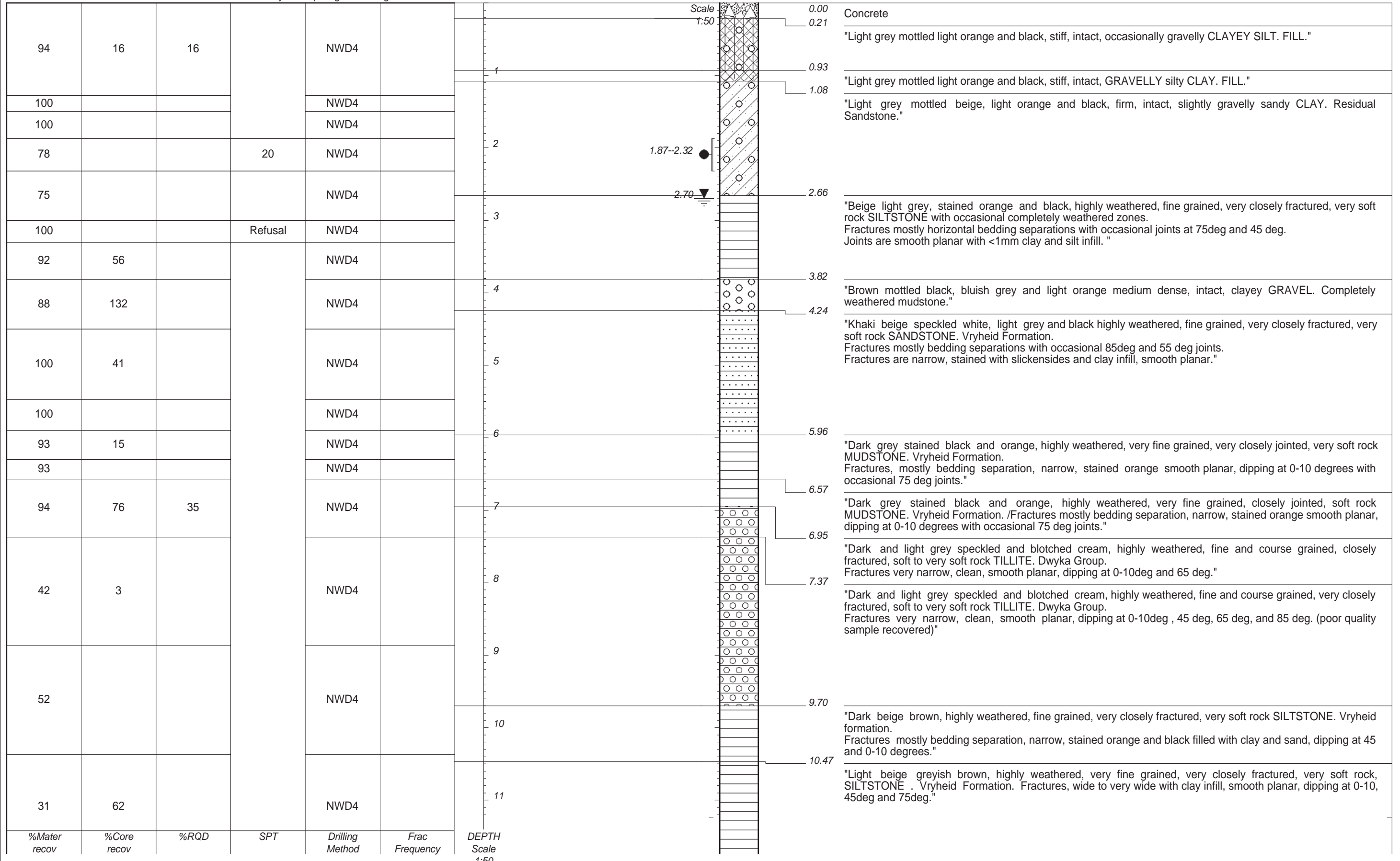
ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock



RAND WATER
VEREENIGING SEDIMENTATION & FLOCCULATION PLANT

HOLE No: BH8
Sheet 1 of 2

JOB NUMBER: 4256



%Mater recov %Core recov %RQD SPT Drilling Method Frac Frequency DEPTH Scale 1:50

HOLE No: BH8
Sheet 2 of 2

JOB NUMBER: 4256

ROCK FABRIC
MF -massive
BF -bedded
FF -foliated
CF -cleaved
SF -schistose
GF -gneissose
LF -laminated

GRAIN SIZE
FG -fine grained
MG -medium grain
CG -coarse grain

JOINT SPACING
VCJ-very close spacg
CJ -close spacing
MJ -medium spacing
WJ -wide spacing
VWJ-very wide spacng

JOINT ROUGHNESS
SLJ-slickensided
SJ -smooth
RJ -rough

JOINT SHAPE
CUR-curvilinear
PLA-planar
UND-undulating
STE-stepped
IRR-irregular

ROCK HARDNESS
EHR-extremely hard rock
VHR-very hard rock
HR -hard rock
MHR-medium hard rock
SR -soft rock
VSR-very soft rock



RAND WATER
VEREENIGING SEDIMENTATION & FLOCCULATION PLANT

HOLE No: BH8
Sheet 2 of 2

JOB NUMBER: 4256

%Mater recov	%Core recov	%RQD	SPT	Drilling Method	Frac Frequency	DEPTH Scale 1:50	DESCRIPTION
76	44			NWD4		12	"Light grey, with black and light orange mottles, loose, intact, slightly clayey fine grained SAND. Completely weathered sandstone."
						12.10	
						12.34	"Light grey with occasional orange streaks and black magnesium dendrites, highly weathered, fine grained, very closely to closely fractured SILTSTONE. Vryheid formation. Fractures mostly bedding separation, narrow, stained orange and black with minor clay infill, smooth planar, dipping at 0-10 deg and 35 deg."
32	32			NWD4		13	
						14	
32	27			NWD4		14.85	"Beige light orange brown, highly weathered, fine grained, closely fractured, soft rock SILTSTONE. Vryheid Formation. Fractures mostly bedding separations, narrow, stained orange and black (magnesium dendrites), smooth undulating, dipping at 0-10deg, 45 deg."
96	96	29		NWD4		15	
						15.94	"Light grey, highly weathered, very fine grained, very closely fractured, soft rock SILTSTONE. Vryheid Formation. Fractures, narrow, with clay infill, smooth planar, dipping at 45 and 0-10 deg."
217	117			NWD4		16	
						16.37	"Beige, highly to moderately weathered, very fine grained, very closely fractured, soft rock MUDSTONE. Vryheid Formation. Fractures, narrow stained orange, smooth planar, dipping at 0-10 and 80 deg."
						16.60	Weathered Contact
						16.67	
58	58	58				17	"Dark grey speckled and blotched red, green, pink, white, light grey, moderately weathered, fine grained (matrix) and very coarse grained (clasts) medium to widely fractured, medium hard rock TILLITE with highly weathered zones at 16.77 -16.8 and 18.42 to 18.45. Dwyka Group. Fractures, narrow, clean, rough undulating, dipping at 0-10 degrees."
						18	
						18.69	"Light green speckled and blotched red, pink, white, light grey, moderately weathered, fine grained (matrix) and very coarse grained (clasts) medium to widely fractured, medium hard rock to possibly hard rock TILLITE. Dwyka Group. Fractures, narrow, clean, rough undulating, dipping at 0-10 degrees."
						19	
						19.24	"Dark grey speckled and blotched red, green, pink, white, light grey, moderately weathered, fine grained (matrix) and very coarse grained (clasts) medium to widely fractured, soft to medium hard rock TILLITE. Dwyka Group. Fractures, narrow, clean, rough undulating, dipping at 0-10 degrees."
104	104	62				19.70	"Light grey, medium weathered, very fine grained, very closely fractured, medium hard rock to possibly hard rock SILTSTONE. Vryheid Formation. Fractures, narrow, with clay infill, smooth planar, dipping at 45 and 0-10 deg."
						19.84	
						20	"Dark grey to black, moderately to highly weathered, very fine grained, moderately fractured, medium hard rock to possibly hard rock MUDSTONE with highly to completely weathered zones. Fractures mostly bedding separation, wide, clay infill, smooth planar dipping at 0-10 deg."
						20.42	

- NOTES
- 1) Water table encountered at 2.70 m
 - 2) Shelby sample retrieved at 1.87--2.32
 - 3) No Core samples retrieved.

CONTRACTOR : GEOMECHANICS	INCLINATION : Vertical	ELEVATION :
MACHINE : YWE - D8	DIAM :	X-COORD : 26deg 41'16.70"S
DRILLED BY :	DATE : 11-15/08/2016	Y-COORD : 27deg 55'4.1"E
PROFILED BY : KDI	DATE : 15/09/2016	
TYPE SET BY : KDI	DATE : 17/11/2016 15:27	HOLE No: BH8
SETUP FILE : BH-JGA-A3.SET	TEXT : ..56BH4256VPSBH008LOG.TXT	